



Achany Wind Farm Extension Grid Connection

Appendix 7.2: Peat Management Plan

SSEN Transmission

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Basis of Report

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1.0 Introduction

1.1 General

SLR Consulting Ltd (SLR) was commissioned by ASH design+assessment on behalf of Scottish and Southern Electricity Networks (SSEN) Transmission to prepare a Peat Management Plan (PMP) for the proposed Achany Wind Farm Extension Grid Connection (the "Proposed Development").

The Proposed Development is situated in a predominantly rural setting, approximately 2.3 km north of Invershin and 300 m west of Inveran, see **Figure 7.2.1**. The Proposed Development comprises approximately 16 km of overhead line (OHL) and approximately 1.2 km of underground cables (UGC), from its northern extent located at the Achany Wind Farm Extension on-site substation at National Grid Reference (NGR) NC 46355 08761 to the existing Shin Power Station located at approximately NGR NH 57220 97484.

The work has been undertaken by a team of Geotechnical Engineers and Geologists, with over 10 years' experience in undertaking peat assessments. The team was led by a Fellow of the Chartered Institution of Water and Environmental Management (CIWEM) and Chartered Water and Environment Manager, with more than 30 years' consultancy experience and specialising in the assessment of soils, geology and water for renewable power projects in Scotland.

1.2 Proposed Development

It is anticipated that the Proposed Development would comprise approximately 16 km of OHL supported by trident H-wood pole, shown on **Figure 7.2.2**. There would be a requirement to install a short section of underground cable (UGC), of approximately 1.2 km into to the consented Achany Wind Farm Extension on-site substation. This is due to the proximity of the proposed Achany Wind Farm Extension wind turbines and the engineering requirement to maintain a minimum separation from OHL infrastructure within their vicinity.

Full details of the Proposed Development are provided in the **EA**, **Chapter 3: The Proposed Development**.

1.3 Objectives

The PMP outlines the overall approach of minimising disruption to peatland, and it aims to ensure that all further opportunities to minimise peat disturbance and extraction would be taken during detailed design and construction of the development.

The PMP has been developed to demonstrate that peat has been afforded significant consideration during the routeing, alignment, design and construction phase of the Proposed Development, should consent be granted. Specifically it shows, with the benefit of site specific peat probing data, how areas of deeper peat have been avoided where technically feasible and how shallow deposits of peat and soils can be safeguard and used to support the long-term habitat restoration and management proposals.

1.4 Role of the Peat Management Plan

The PMP is intended to be a working document to be used throughout the key stages of the design, construction, operation, decommissioning and re-instatement phases of the Proposed Development as part of an overall Construction Environmental Management Plan (CEMP). These stages are outlined below.



Stage 1: Environmental Assessment (EA)

This report forms the Outline Peat Management Plan and is submitted as part of the EA Report. From this initial report the Peat Management Plan will be developed further into a Stage 2 Pre-Construction PMP.

Stage 2: Post Consent / Pre-Construction

The peat mass balance calculations may be further developed prior to the works commencing, following detailed ground investigation or further survey works required to inform detailed design, or that may be required under planning consent conditions.

Stage 3: Construction Stage

Actual peat volumes excavated during construction will be recorded against the overall predicted volumes. Within micrositing allowances, the alignment and design of tracks, pole foundations and associated construction methods will be reviewed to avoid / minimise peat disturbance as much as possible considering the more detailed information available once construction commences. A regular review and update of the peat mass balance will be undertaken by the appointed Contractor and monitored by the Ecological Clerk of Works (ECoW) on-site and made available to regulators as required.

1.5 Legislation and Guidance

The PMP has been compiled in accordance with the following legislation and best practice guidance:

- National Planning Framework for Scotland 4 (NPF4) (Scottish Government, February 2023)¹;
- Scottish Government, Scottish Natural Heritage, SEPA (2014) 'Peat Survey Guidance; Developments on Peatland: Site Surveys²;
- SEPA Regulatory Position Statement Developments on Peat (Scottish Environment Protection Agency, 2010)³;
- Good Practice During Wind Farm Construction, NatureScot (July 2024)
- Guidance on the Assessment of Peat Volumes, Reuse of Excavated Peat and the Minimisation of Waste (Scottish Renewables and SEPA, 2012) 5:
- The Waste Management Licensing (Scotland) Regulations 2011⁶;
- Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments (Scottish Government, January 2017)
- Floating Roads on Peat Report into Good Practice in Design, Construction and Use
 of Floating Roads on Peat with reference to Wind Farm Developments in Scotland
 (Forestry Commission Scotland & Scottish Natural Heritage, 2010) 8.



 $^{1 \,} Scottish \, Government \, (2023). \, https://www.gov.scot/binaries/content/documents/govscot/publications/advice-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-framework-4-revised-and-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-guidance/2022/11/national-planning-gu$

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² Scottish Natural Heritage (SNH), SEPA, Scottish Government & James Hutton Institute. (2014)' Peat Survey Guidance; Developments on Peatland: Site Surveys'.

 $^{{\}tt 3\ Scottish\ Environment\ Protection\ Agency.\ 2010.\ Regulatory\ Position\ Statement-Developments\ on\ Peat}$

 $^{4\} NatureScot (July\ 2024), Good\ Practice\ During\ Wind\ Farm\ Construction,\ available\ online\ at: https://www.nature.scot/doc/good\ -practice\ -during\ -wind\ -farm\ -construction$

⁵ Scottish Renewables, Scottish Environment Protection Agency. 2012. Guidance on the Assessment of Peat Volumes, Reuse of Excavated Peat and the Minimisation of Waste

⁶ Scottish Government 2011. The Waste Management Licensing (Scotland) Regulations 2011. https://www.legislation.gov.uk/sdsi/2011/9780111012147/contents

⁷ Peat Landslide Hazard and Risk Assessments (Scottish Government, April 2017)

⁸ Scottish Natural Heritage, Forestry Commission (August 2010). Floating Roads on Peat

Requirements of National Planning Policy 4

The intent of Policy 5 (Soils) of National Planning Policy 4 (NPF4)¹ is "to protect carbon rich soils, restore peatlands and minimise the disturbance of soils from development".

The Policy states [5(a)] that development proposals should only be supported if they are designed and constructed:

- in accordance with the mitigation hierarchy by first avoiding and then minimising the amount of disturbance to soils on undeveloped land; and
- in a manner that protects soils from damage including from compaction and erosion, and that minimises soils sealing.

Further [5(c)] confirms that development proposals on peatland, carbon rich soils, and priority peatland will only be supported if they are:

- essential infrastructure and there is a specific locational need and no other suitable site;
- the generation of energy from renewable sources that optimises the contribution of the area to greenhouse gas emissions reductions targets;
- small-scale development directly linked to a rural business, farm or croft;
- supporting a fragile community in a rural or island area; or
- restoration of peatland habitats.

And [5(d)] confirms that where development on peatland, carbon-rich soils or priority peatland habitat is proposed, a detailed site specific assessment will be required to identify:

- the baseline depth, habitat condition quality and stability of carbon rich soils;
- the likely effects of the development on peatland, including on soil disturbance; and
- the likely net effects of the development on climate emissions and loss of carbon.

Policy 5 also confirms that the site specific (above) assessment [5(d)] "should inform careful project design and ensure, in accordance with relevant guidance and the mitigation hierarchy, that adverse impacts are first avoided and then minimised through best practice. A peat management plan will be required to demonstrate that this approach has been followed, alongside other appropriate plans required for restoring and/ or enhancing the site into a functioning peatland system capable of achieving carbon seguestration".

This Stage 1 PMP considers the protection and safeguarding of peat and seeks to fulfil the requirements of Policy 5(d) with further detail on peatland habitat and peatland restoration proposals provided in EA Chapter 5 Ecology which would be included in a future Outline Habitat Management Plan for the Proposed Development.

Mitigation Hierarchy

SEPA³ has published guidance regarding the mitigation hierarchy for developments on peat which is summarised below:

- Prevention avoiding generating excess peat during construction (e.g. by avoiding peat areas or by using construction methods that do not require excavation such as floating tracks);
- Re-use use of peat produced on-site in restoration, provided that its use is fully justified and suitable;



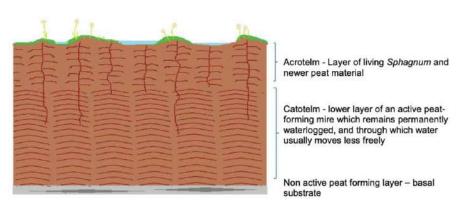
- Recycling / Recovery / Treatment modify peat produced on-site for use as fuel, or as a compost / soil conditioner, or dewater peat to improve its mechanical properties in support to re-use; and
- Storage applying the SEPA guidance, storage of peat up to a depth of 2 m is not classified as a waste and, however clarification should be sought from the waste regulator prior to re-use and care must be taken to ensure that it does not cause environmental pollution.

Definition of Peat

Peat is defined as a material consisting of the partially decomposed remains of plant material and organic matter preserved over a period in a waterlogged environment resulting in anaerobic conditions and is of depths >0.5 m.

Peat can be classed as two principal types, the acrotelm layer and the catotelm layer as shown on **Plate 1-1**.

Plate 1-1: Drawing of two layered Structure of Active Bog Peatlands above Non-Active Peat⁹



The acrotelm layer is found in the upper layer of peat where conditions are relatively dry and comprises living vegetation and partially decomposed plant material. Hydraulic conductivity in this layer tends to be higher in relation to distance from the water table. The thickness of the acrotelm layer varies depending on topography such as steepness of slope, peat hags, and hummocks. In particular, the acrotelm layer can be affected during periods of drought or as a consequence of drainage. Fibrous in texture, the acrotelm layer has some tensile strength and is generally considered to be stable for storage and re-use.

The catotelm layer is found under the acrotelm layer and comprises decayed plant material and organisms and is denser and with a very low hydraulic conductivity. The catotelm layer sits below the water table resulting in permanent anaerobic conditions. The catotelm layer is amorphous and has very low tensile strength making it less suitable for storage and re-use.

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⁹ Bruneau, P.M.C & Johnson, S.M. 2014. Scotland's peatland - definitions & information resources. Scottish Natural Heritage Commissioned Report No 701.

2.0 Baseline Conditions

2.1 Topography

Ground elevations across the Proposed Development range from approximately 400 m Above Ordnance Datum (AOD) within the northern extent, near Carn nam Bo Maola, to approximately 2 m AOD at the southern extent of the Proposed Development near the Kyle of Sutherland and River Shin confluence. The approximate ground levels of the connection point at Shin Substation are 10 m AOD.

2.2 Geology

2.2.1 Artificial Ground

Published BGS online data¹⁰ indicates that made ground deposits are not present within the Proposed Development.

2.2.2 Superficial Geology

Based on the available BGS online data¹⁰ the superficial geology mapping shows that the northern extent of the Proposed Development is generally underlain by glacial till deposits whilst the southern extent of the Proposed Development is generally underlain by glacial till and morainic deposits.

Areas of peat are mapped within the Proposed Development, particularly within the northeastern extents near the slopes of Cnoc nan Imrichean and within the southern extents of the Proposed Development near Braemore Wood.

In the southern extents of the Proposed Development, near to Kyle of Sutherland, alluvium, river terrace and alluvial fan deposits are noted. Alluvial deposits are also recorded within the extents of the larger watercourses within the Proposed Development.

EA Chapter 7 Figure 7.3 shows the superficial geology BGS mapping across the Proposed Development.

2.2.3 Bedrock Geology

Based on the available BGS online data¹⁰, the majority of the Proposed Development is underlain by psammites of the Altnaharra Psammite Formation. A strip across the centre of the Proposed Development, near Doir' a Chatha, is shown to be underlain by the Lewisianoid Gneiss Complex comprising orthogneisses.

There are several amphibolite and phyllonite intrusions noted across the southern extents of the Proposed Development.

There are no inferred faults recorded within the Proposed Development.

EA Chapter 7 Figure 7.5a and b shows the bedrock geology BGS mapping across the Proposed Development.

2.3 Peatland Classification

The Carbon and Peatland Map 2016¹¹ indicates that the majority of the northern extent of the Proposed Development is underlain by Class 2 peatland with areas of Class 1 peatland

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¹⁰ British Geological Survey, GeoIndex Onshore, available online at: https://mapapps2.bgs.ac.uk/geoindex/home.html?_ga=2.133433804.376188765.1646739904-1030004651.1646739904

¹¹ NatureScot, Carbon and Peatland Map 2016, Available online at: map.environment.gov.scot/soil_maps/

confined to the eastern edges of the Proposed Development. Class 1 and Class 2 peatlands are considered nationally important carbon-rich soils, deep peat and priority peatland which are considered to have high conservation value.

Much of the southern extent of the Proposed Development is located within Class 5 peatland (habitats which may contain carbon rich soils and deep peat but are not considered to be of high conservation value) with localised areas of Class 1, Class 2 and Class 3 peatland also recorded. The southern extent of the Proposed Development area around Linsidemore is shown to be underlain by mineral soils (Class 0) whereby peatland habitats are not typically found.

EA Chapter 7 Figure 7.4 provides the Peatland Classification.

2.4 Hydrology

The Proposed Development is located entirely within the Kyle of Sutherland surface water catchment, in particularly the following three sub catchments:

- The northern extents of the Proposed Development is largely located within the surface water catchment of the River Cassley. The River Cassley flows in a generally northwest to south east direction from Fionn Loch Mor to the Dornoch Firth, approximately 1.8 km west of the Proposed Development. A number of smaller watercourses drain into the River Cassley, notably the Allt Bad an t-Segairt and Allt an Rasail which cross the Proposed Development.
- The central part of the Proposed Development is located within the surface water management catchment of the Allt Mor. Allt Mor flows from Loch Doire a' Chatha generally south-westerly towards its discharge into the Kyle of Sutherland.
- The south-eastern extent of the Proposed Development lies within the River Shin surface water catchment. A small area north of the Proposed Development, near to Loch Sgeireach, also falls into this catchment. The River Shin flows from Loch Shin to Dornoch Firth with many smaller burns draining towards it. The river is approximately 200 m east of the Proposed Development near to the existing tower at Shin Substation.

2.5 Peat Deposits

There are deep peat deposits situated within areas of the Proposed Development. However, these deposits are generally situated across flatter expanses and in minor topographic lows. **Photo 1** shows typical ground conditions.

There are areas of blanket bog situated north of Coire Bog, these blanket bogs are further described in the NVC survey detailed in **EA Chapter 5** with peat depths over 3 m recorded across this area. The distribution and extents of peat recorded during the peat depth surveys are detailed in **Section 3.2** below.



Photo 1: Blanket bog at NC 46574 06363 northwest of Coire Bog



2.5.1 Peat Erosional Features

From review of aerial photography, there are peat haggs observed across the Proposed Development. This was confirmed by site visits where erosional features were recorded especially in the northern extents of the Proposed Development. The following photo provides a visual example of peat hagging at the Proposed Development.

Photo 2: Peat haggs at NC 46123 07098 southeast of Loch Shiela



2.5.2 Artificial Drainage

Artificial drainage was frequently observed on review of aerial photography and during site visits. Artificial drainage across the Proposed Development is generally associated with the



existing road and the forestry in the southern area of the Proposed Development. There are frequent artificial drains associated with the forestry with drainage furrows generally trending north to south. There are extensive drainage channels in the northern extent of the Proposed Development as shown in **Photo 3**.

Photo 3: Drainage channels at NC 46191 06947 trending east to west





3.0 Fieldwork

3.1 Methodology

The surveys carried out followed best practice guidance for developments on peatland ^{12,13}. Phase 1 peat probing resulted in probing on an approximate 50 - 100 m grid on initial assessment areas of the OHL route which was used in preliminary site layout designs. Phase 2 probing saw detailed probing undertaken across the Proposed Development layout, focusing on access tracks, cable routes, pole locations and other site infrastructure. The Phase 1 survey informed the site design such that areas of recorded peat could be avoided where technically feasible.

Phase 2 probing was typically undertaken on linear infrastructure (permanent / temporary tracks) at 25 m to 50 m spacings with offset probing locations either side (approximately 10 m to 25 m). Infrastructure (poles) was typically probed at 10 m grid spacings within the working area as defined in **EA Chapter 3**.

The thickness of the peat was assessed using a graduated peat probe, approximately 6 mm diameter and capable of probing depths of up to 10 m. This was pushed vertically into the peat to refusal and the depth recorded, together with a unique location number and the coordinates from a handheld Global Positioning System instrument (GPS). The accuracy of the GPS was quoted as ±2 m, which was considered sufficiently accurate for this survey. All data was uploaded into a GIS database for incorporation into various drawings and analysis assessments.

Where the peat probing met refusal on a hard substrate, the 'feel' of the refusal can provide an insight into the nature of the substrate. An assessment of the substrate was made and recorded at each probe hole. The following criteria were used to assess material:

- solid and abrupt refusal rock;
- solid but less abrupt refusal with grinding or crunching sound sand or gravel or weathered rock;
- rapid and firm refusal clay; or
- gradual refusal dense peat or soft clay.

The relative stiffness of the peat was also assessed from the resistance to penetration of the probe and to the effort required to extract the probes (retrieval of the probe was often impossible for one person). In all instances refusal was met on obstructions allowing identification of subsurface geology.

3.2 Peat Depth

Peat is generally defined as a soil with a surface organic layer more than 0.5 m¹³. Where the probing recorded a thickness of less than 0.5m thick, it is considered to be a peaty soil (or organo-mineral soil). Soils with a peaty organic horizon over mineral soil are often referred to as 'peaty soils'. These organo-mineral soils are extensive across the UK uplands, but do not meet recognised definitions of peat as they are either shallower than true peat or have a lower carbon density.

Peat >0.5 m was recorded within the area of the UGC and temporary access track routes in the northern area of the Proposed Development. Localised areas of deep peat >1.0 m were

¹³ Scottish Natural Heritage (SNH), SEPA, Scottish Government & James Hutton Institute. (2014)' Peat Survey Guidance; Developments on Peatland: Site Surveys'.



¹² Scottish Renewables & SEPA (2012) 'Developments on Peatland Guidance on the Assessment of Peat Volumes, Reuse of Excavated Peat and the Minimisation of Waste'.

recorded in localised topographic lows predominantly within the northern section of the UGC and temporary access track route.

To the south of the UGC route within the Proposed Development areas of peat are present >0.5 m with deep peat >1.0 m recorded in the flatter topographic areas and gentler slopes to the east of Loch Shiela, the Allt an Rasail, Glen Rossal Burn and Cnoc nah Gamhna.

Peat is also present in the central area of the Proposed Development on the flatter expanses to the north-west of the Allt Doir a' Chatha. To the east of the Allt Doir a' Chatha within the area of the Proposed Development up to the Allt Loch an Fheoir, peat is typically absent due to the steeper topography.

To the south of the Allt Loch an Fheoir and to the north of Middle Hill deep peat >1 m is present in the flatter expanses of the Proposed Development. An area of deep peat >1 m is present within the Proposed Development within the flatter topographic area between Middle Hill Wood and Cnoc Eadar-mi. Peat >0.5m is typically absent within the Proposed Development between the Allt a' Ghlugheran and Inveran at the Shin Substation.

A total of 14,800 peat probes were undertaken across all survey phases, with the results summarised in **Table A** and within the peat depth interpolation figure **(Figure 7.2.4)**. The interpolation of peat depths shown on the figures was undertaken using the Inverse Distance Weighting (IDW) methodology. All probing data is provided in **Annex B**.

Table A: Peat Probing Results

Peat Thickness (m)	No. of Probes	Percentage (of total probes undertaken on-site)
0 (no peat)	233	1.6
0.01 - 0.49 (peaty soil)	10663	72
0.50 - 0.99	2186	14.8
1.00 – 1.49	827	5.6
1.50 – 1.99	449	3
2.00 - 2.49	210	1.4
2.50 - 2.99	126	0.9
3.00 - 3.49	69	0.5
3.50 - 3.99	28	0.2
> 4.00	9	0.1

3.3 Peat Condition

Peat is described using BS5930¹⁴ and the Von Post classification¹⁵. Five peat cores were undertaken by SLR using a peat auger and were used to inform interpretations of the peat condition and underlying substrate. The locations for the cores were selected based on their vicinity to infrastructure that were situated within areas of peat deposits.

Based on interpretations from probing and peat core samples, the peat within the Proposed Development is predominantly fibrous to pseudo fibrous. Shallow peat deposits across the



¹⁴ BS 5930:2015+A1:2020, Code of practice for ground investigations

¹⁵ Von Post, L. and Grunland, E., (1926), 'Sodra Sveriges torvillganger 1' Sverges Geol. Unders. Avh., C335, 1-127.

Proposed Development are generally fibrous. Deeper peat deposits are generally characterised as pseudo-fibrous. The peat was classified using the Von Post classification as between H2 and H5, showing insignificant to moderate decomposition.

Peat core logs and photographs are presented within **Annex B**.



4.0 Potential Impacts on Peat During Construction

The initial construction phase for the Proposed Development will include soil and peat stripping and excavation activities associated with construction of the Proposed Development.

There are four main types of impact on peat which can occur during construction. These are:

- Loss of structural integrity and peat strength, due to stripping off or damaging the surface vegetation turf, excavation, handling and transporting peat (particularly wet, subsurface peat);
- Erosion and gullying, caused by exposure and desiccation of bare peat surfaces primarily caused by water erosion, due to surface runoff after rainfall;
- Contamination, caused by leaks, spillages or inappropriate laydown of materials; and
- Peat slide, caused by laying wet peat on top of wet peat, laying other heavy materials (including excavated mineral soil or other construction materials) on top of wet peat or by inappropriate stockpiling, such as attempting to create stockpiles of peat that are too high, without bunding, engineering or geotechnical support.

A range of methods and control measures are described below which are designed to prevent these impacts from occurring.



5.0 Management and Mitigation

The Proposed Development design took account of a number of environmental and technical constraints. The design sought to avoid areas of thick peat where technically feasible, whilst taking into account other environmental and technical factors such as ecology, ornithology, hydrology, topography and existing infrastructure. The Proposed Development has largely avoided extensive areas where peat is >1 m and efforts have been made by iterative design to minimise the footprint of site infrastructure on peat >0.5 m as far as practicable. Where peat and peaty soils are to be excavated, re-used or reinstated, the following good practice applies.

5.1 Excavation

Excavated peat should be excavated as turves, including the acrotelm (surface vegetation) and a layer of adjoining catotelm (more humified peat) typically up to 0.5 m thick in total, or as blocks of catotelm; the acrotelm should not be separated from its underlying peat, furthermore:

- the turves should be as large as possible to minimise desiccation during storage, though the practicalities of handling should be considered:
- the mixing of excavated peat with substrate materials is to be avoided at all times;
 and
- consider timing of excavation activities to avoid very wet weather and avoid multiple handling to minimise the likelihood of excavated peat losing structural integrity.

If possible, extract intact full depth acrotelm layers from the top surface of the peat deposit. This technique will maintain connectivity between the surface vegetation and the partially decomposed upper layers of the catotelm.

5.2 Re-use

All excavated material (including peat and non-peat soils) from the installation of the poles will be re-used for reinstatement of the working area immediately surrounding the poles.

It is anticipated that the volume of material excavated for the new permanent access track can be entirely reused for a variety of restoration purposes, including verge restoration to taper into the existing peatland by infilling depressions and levelling-out gradients as part of the cut and fill track construction process.

5.3 Storage

The following good practice applies to the storage of peaty soils / peat:

- stripped materials should be carefully separated to keep peat and other type of soils apart;
- to minimised handling and haulage distances, excavated material should be stored local to the site of excavation or end point of restoration;
- peat turves should be stored in wet conditions or irrigated in order to prevent desiccation (once dried, peat will not rewet);
- stockpiling of peat should be in large volumes to minimise exposure to wind and sun (and desiccation), but with due consideration for slope stability and should not exceed 1 m in height to maintain stability of stockpile;
- stockpiles should be isolated from watercourses or drains with appropriate bunding to minimise pollution risks;



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- stockpiles to be stored a minimum of 10 m from any watercourse;
- stores of non-turf (catotelm) peat should be bladed off to reduce the surface area and desiccation of the stored peat; and
- peat storage areas should be monitored during periods of very wet weather, or during snowmelt, to identify early signs of peat instability.

Any peaty soils / peat to be removed during construction would require a temporary storage area near to the construction works / area of re-use. Where peat cannot be transferred immediately to an appropriate restoration area, short term storage will be required. In this case, the following good practice applies:

- peat should be stored around the excavation perimeter at sufficient distance from the cut face to prevent overburden induced failure;
- local gullies, diffuse drainage lines (or very wet ground) and locally steep slopes should be avoided for peat storage;
- drying of stored peat should be avoided by irrigation or by seeding (although this is unlikely to be significant for peat materials stored less than 2 months);
- peat generated from permanent excavations should be transported directly to its allocated restoration location, to minimise the volume being stockpiled with the possibility of drying out;
- stores of catotelm peat should be bladed off to reduce their surface area and minimise desiccation;
- where transport cannot be undertaken immediately, stored peat should be irrigated to limit drying and stored on a geotextile mat to promote stability; and
- monitoring of large areas of peat storage during wet weather or snowmelt should be undertaken to identify any early signs of peat instability.

5.4 Transport

The following good practice applies to transport:

- movement of turves should be kept to a minimum once excavated, and therefore it is preferable to transport peat planned for translocation and reinstatement to its destination at the time of excavation; and
- if HGVs / dump trucks that are used for transporting non-peat material are also to be used for peat materials, measures should be taken to minimise cross-contamination of peat soils with other materials.

5.5 Handling

Following refinement of the peat model, a detailed storage and handling plan should be prepared forming part of the detailed CEMP, including:

- best estimate excavation volume at each infrastructure location (including peat volumes split into area / volume of 'acrotelm' or 'turf', and volume of catotelm) which would be achieved by undertaking additional probing in line with current guidance;
- volume to be stored locally and volume to be transferred directly on excavation to restoration areas elsewhere (e.g. peat storage areas) in order to minimise handling;
- location and size of storage area relative to pole foundations and natural peat morphology / drainage features; and



• irrigation requirements and methods to minimise desiccation of excavated peat during short term storage.

These parameters are best determined post-consent, informed by detailed ground investigation with the micro-siting areas for each element of infrastructure.

5.6 Restoration

During restoration, the following best practice should be followed:

- carefully evaluate potential restoration sites, such as peat storage areas for their suitability, and agree that these sites are appropriate with the ECoW, landowners and relevant consultees;
- undertake restoration and revegetation or reseeding work as soon as practically possible;
- where required, consider exclusion of livestock from areas of the Proposed Development undergoing restoration, to minimise impacts on revegetation; and
- as far as reasonably practicable, restoration will be carried out concurrently with construction rather than at its conclusion.

5.7 Access Tracks

There is guidance^{4,8} available to support access track design in peatlands. Guidance is generally focused on floating tracks and excavated tracks and is summarised below.

Temporary tracks are likely to comprise trackway which would not require excavation. If trackway was not deployed then temporary excavated access tracks would be required and would be fully re-instated following completion of the construction phase.

Based on the avoidance of significant areas of deep peat, permanent track design is typically present on peat <1 m, with only limited sections of track on localised areas of peat >1 m, therefore the use of excavated tracks is proposed.

Excavated tracks require complete excavation of soil / peat to a competent substrate. Excavated tracks will generally be undertaken where peat depths are less than 1 m. This peat / soil would require storage ahead of re-use elsewhere within Proposed Development. Good practice guidance relates mainly to drainage in association with excavated tracks:

- trackside ditches should capture surface water (within the acrotelm) before it reaches the road;
- interceptor drains should be shallow and flat bottomed (and preferably entirely within the acrotelm to limit drawdown of the water table);
- any stripped peat turves should be placed back in the invert and sides of the ditch to assist regeneration and prevent erosion to the peat and wash out that could occur; and
- culverts and cross drains should be installed under excavated tracks to maintain subsurface drainage pathways (such as natural soil pipes or flushes). Discharge from constructed drainage should allow for as much diffuse dispersion of clean (silt free) water as possible while minimising disturbance to existing peatland as far as possible. Silt mitigation measures will be incorporated into all constructed drainage as per the requirements of the CEMP.

Although excavation is normally undertaken in peat of minor thickness (< 1 m), there is a possibility of minor slippage from the cut face of the peat mass. Accordingly:



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- free faces should be inspected for evidence of instability (cracking, bulging, excessive discharge of water or sudden cessation in discharge); and
- where significant depths of peat are to be stored adjacent to an excavation, stability analysis should be conducted to determine Factor of Safety (FoS) and an acceptable FoS adopted for loaded areas.

Regular routine monitoring should be scheduled post-construction to ensure that hydrological pathways and track integrity have been suitably maintained.

5.8 Monitoring and Inspection

There would be frequent, routine and regular inspections of peat in all stockpiles and temporary storage areas as part of the PMP audit process. Inspections would assess in situ peat physical conditions, integrity of containment and temporary drainage conditions, and they would seek to confirm that stockpile design and management was adequate to prevent erosion and peat slide. These inspections would take place weekly during stockpile creation and storage.

Should any problems be observed during regular visual inspections of peat stockpiles, this would invoke implementation of an appropriate corrective action which would be recorded and monitored for effectiveness. Types of corrective actions would include, but would not necessarily be limited to; modification of temporary drainage, additional or modified bunding, incorporating of sediment fencing if required, light re-grading to correct any areas of surface erosion, etc.

Regular, frequent inspections of peat conditions during construction and restoration phases of work would be carried out by the Engineer and ECoW as follows:

- peat surface, peat profile and peat consistency conditions would be carried out as part of ground investigations prior to the start of construction. This information would provide detailed information on the baseline conditions for each part of the infrastructure footprint;
- restored peat conditions would be inspected immediately after restoration to ensure that the methods detailed in the PMP had been correctly implemented and to inform any corrective actions should they be required;
- further monitoring to be undertaken where required to ensure restoration works have been correctly implemented; and
- the physical condition of peat would be retained as carefully as possible both at the peat storage and the peat restoration stages. This is particularly important for vegetation establishment.



6.0 Peat Balance Assessment

Table B below provides an estimate of peat and peaty soil volumes to be excavated and reused during the construction of the Proposed Development. The peat and peaty soil excavation and re-use volumes are detailed for each infrastructure element in **Annex A**.

6.1 Excavated Volumes

Peat excavation volumes associated with the construction of the Proposed Development have been calculated using the results from the peat depth surveys and interpolation using the GIS package ArcGIS. Peat excavation volumes are detailed in **Table B** and **Annex A** and based on the following assumptions:

- Interpolation of peat depth was undertaken using the Inverse Distance Weighting (IDW) interpolation method.
- An acrotelm depth of 0.5 m across all infrastructure based on peat depth survey results.
- The peat volumes have been calculated based on the average peat depth across each item of infrastructure using the peat depth survey results.
- The peat balance calculations also include a worst case estimate for excavated
 materials assuming the temporary track is excavated and re-instated following
 completion of the construction phase. At this stage it is envisaged that the temporary
 track will likely comprise trackway which will not require further excavations but the
 use of excavated tracks cannot be discounted.

The excavated volumes will comprise primarily acrotelmic peat and soils.

6.2 Reuse Volumes

The volume of peat to be reused at the Proposed Development is detailed in **Table B** and **Annex A** and based on the following assumptions:

- In appropriate locations around the edges of permanent track verges, a 2.5 m wide strip either side of the permanent track will be re-used at a thickness of about 0.5 m (turves and acrotelmic peat) to tie into the adjacent habitat.
- Reinstatement of pole working areas with the excavated soils and peat to ensure integration with the adjacent habitat areas some of which comprise blanket bog,.

6.3 Net Peat Balance

Table B provides an estimate of peat volumes to be excavated and reused during the construction of the infrastructure.

Table B: Peat Balance Assessment

Infrastructure	Volume of Peat Excavated (m³)	Volume of Peat Reused and Reinstated (m³)
Permanent Access Track	258	258
Temporary Access Track*	20,334	20,334
UGC	2,456	2,456
Wood Poles	17,327	17,327
Total	40,380	40,380



Infrastructure	Volume of Peat Excavated (m³)	Volume of Peat Reused and Reinstated (m³)	
Total**	20,046	20,046	

^{*}Assumes temporary track excavated. Likely to be using Trackway system and therefore no excavations will be required.

The total volume of peat predicted to be excavated of 40,380m³, does not exceed the intended total peat reuse volume, therefore no excess peat is required to be disposed offsite as a consequence of the Proposed Development.



 $^{{\}bf **} {\sf Total} \ when \ {\sf trackway} \ {\sf is} \ {\sf used} \ {\sf for} \ {\sf temporary} \ {\sf tracks} \ {\sf and} \ {\sf no} \ {\sf excavation} \ {\sf of} \ {\sf temporary} \ {\sf tracks} \ {\sf is} \ {\sf required}.$

7.0 Waste Classification

This section of the Stage 1 Outline PMP includes the method for dealing with peat which could potentially be classified as waste (only if the above volumes estimate significant quantities of catotelm peat, which cannot be re-used).

Table C outlines where those materials that are likely to be generated on-site fall within the Waste Management Licensing (Scotland) Regulations 2011.

Based on the results presented in this document, it has been concluded that all of the materials to be excavated on-site would fall within the non-waste classification and would be re-used on-site. Based on a detailed probing exercise and visual inspection of the peat, it is predominantly fibrous peat which would be suitable to be re-used on-site. Typically, the peat was found to be fibrous and fairly dry within the top metre before becoming slightly more pseudo-fibrous with depth.



Table C: Excavated Materials – Assessment of Suitability

Excavated Material	Indicative Volume % of total excavated soils	Is there a suitable use for material	Is the material required for use on Site	Material Classified as Waste	Re-use Potential	Re-use on Site
Turf and Acrotelmic Peat An estimated acrotelm depth of 0.5 m based on peat survey results	82	Yes	Yes	Not classified as waste	Yes	Will be re-used in reinstatement of pole excavation working areas including cut and fill verges, road verges, side slopes and check drains.
Catotelmic peat	18	Yes	Yes	Not classified as waste	Yes	Will be re-used in reinstatement of pole excavation working areas including cut and fill verges, road verges, side slopes and check drains.
Amorphous Catotelm Peat (amorphous material unable to stand unsupported when stockpiled >1 m)	0	Potentially	Potentially*	Potentially if not required as justifiable restoration of habitat management works	Limited	If peat does not require treatment prior to re-use it can be used on-site providing adequate justification and method statements are provided and approved by SEPA. If it is unsuitable for use without treatment then it may be regarded as a waste. However every attempt to avoid this type of peat has been incorporated into the design.

^{*}Such uses for this type of material are limited, however there may be justification for use in the base of peat restoration areas to maintain waterlogged conditions and prevent desiccation of restored area and in some habitat management works such as gully or ditch blocking where saturated peat is required to mimic mire type habitats and encourage establishment of sphagnum.



8.0 Conclusion

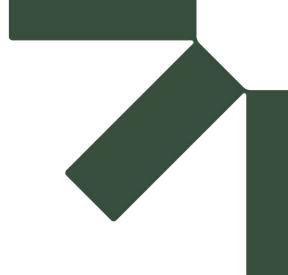
This Stage 1 Outline PMP presents a pre-construction assessment of the expected peat extraction and reuse volumes associated with the works phase of the construction of the Proposed Development. The PMP also provides the guiding principles which would be applied during the construction of the Proposed Development. Peat depth surveys have shown that there are localised peat deposits across the Proposed Development.

Through a process of continued design refinement (focused on minimising peat excavation volumes) and adoption of best practice working methods, the Proposed Development has been shown to achieve an overall peat balance. Thus, all excavated material will be required for reuse as part of the works and no surplus peat would be generated.

The figures detailed within this report are to be considered indicative at this stage. The total peat volumes are based on a series of assumptions for the layout of the Proposed Development and the results of several phases of peat probing. Such parameters can still vary over small scale areas and therefore topographic changes in the bedrock profile could impact the total accuracy of the volume calculations.

The calculations presented here would be updated and expanded upon as part of detailed design works, taking account of pre-construction site investigations and micro-siting, to confirm actual quantities of arising peat. A detailed, construction phase PMP would be developed (by the Contractor) and maintained by updating this plan in conjunction with a Geotechnical Risk Register. The implementation of the detailed PMP would ensure a robust commitment to excavating, storing and reinstating peat in a manner that follows best practice and ensures the protection of peat throughout the construction and post-construction phases.





Figures

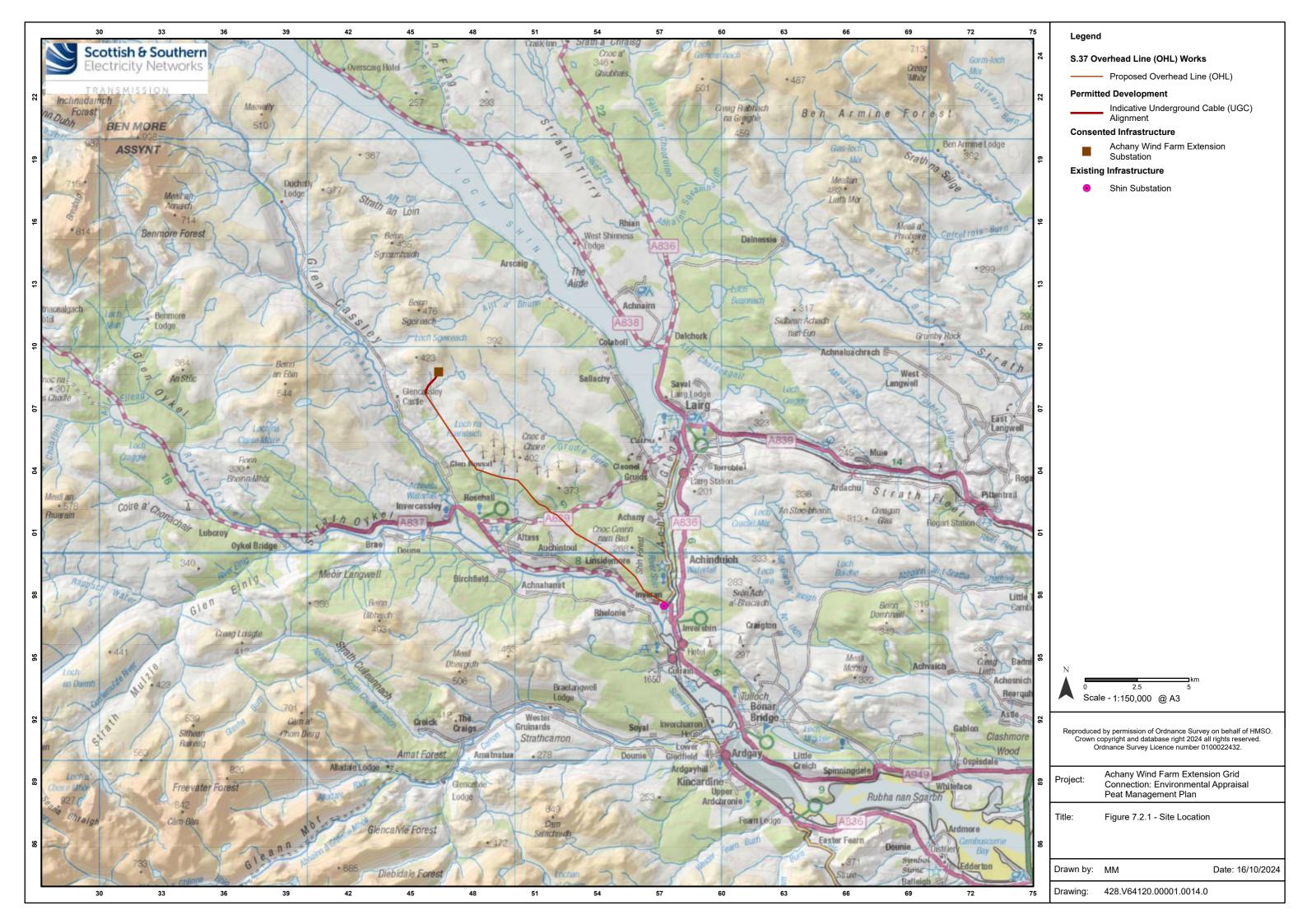
Achany Wind Farm Extension Grid Connection

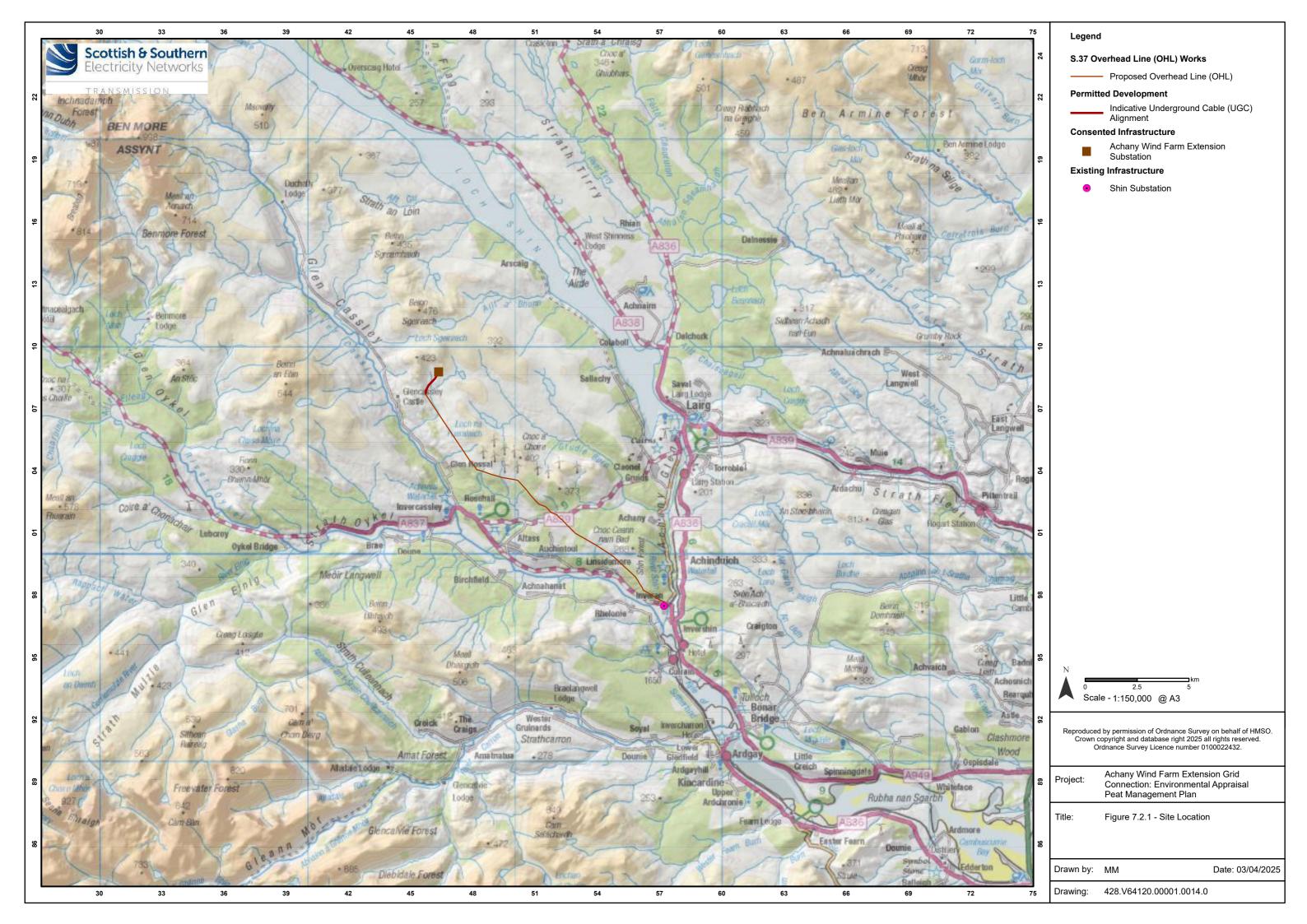
Appendix 7.2: Peat Management Plan

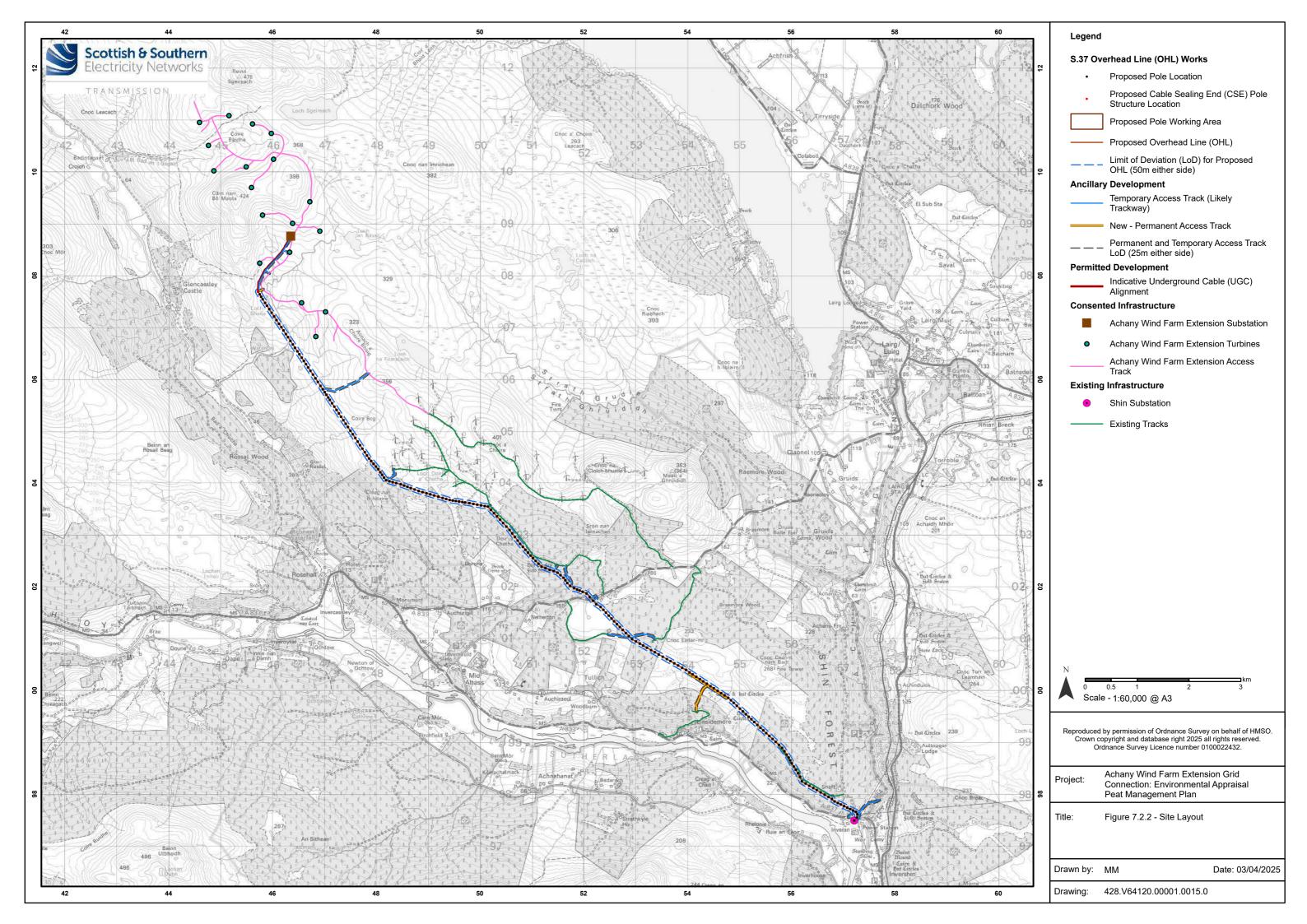
SSEN Transmission

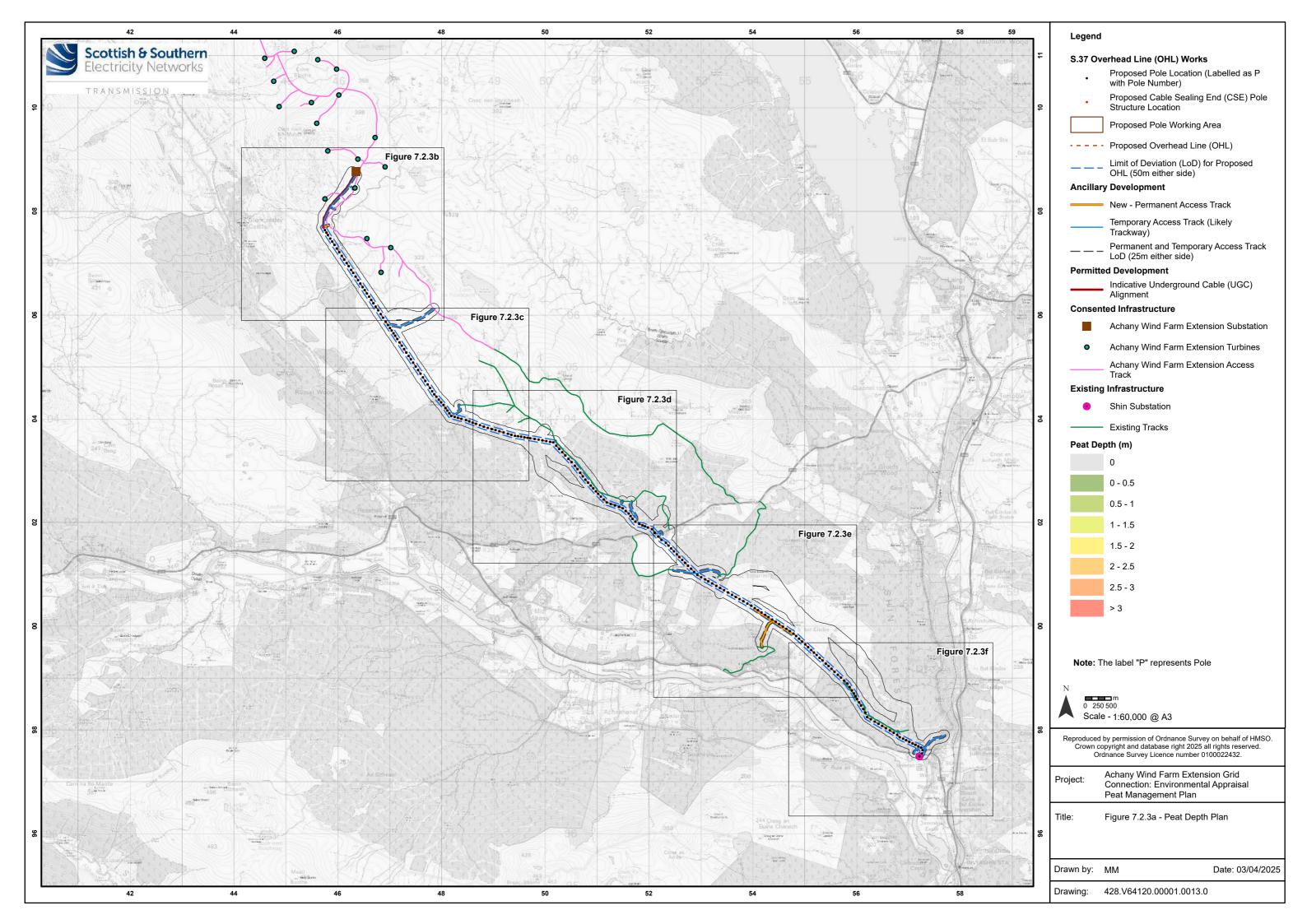
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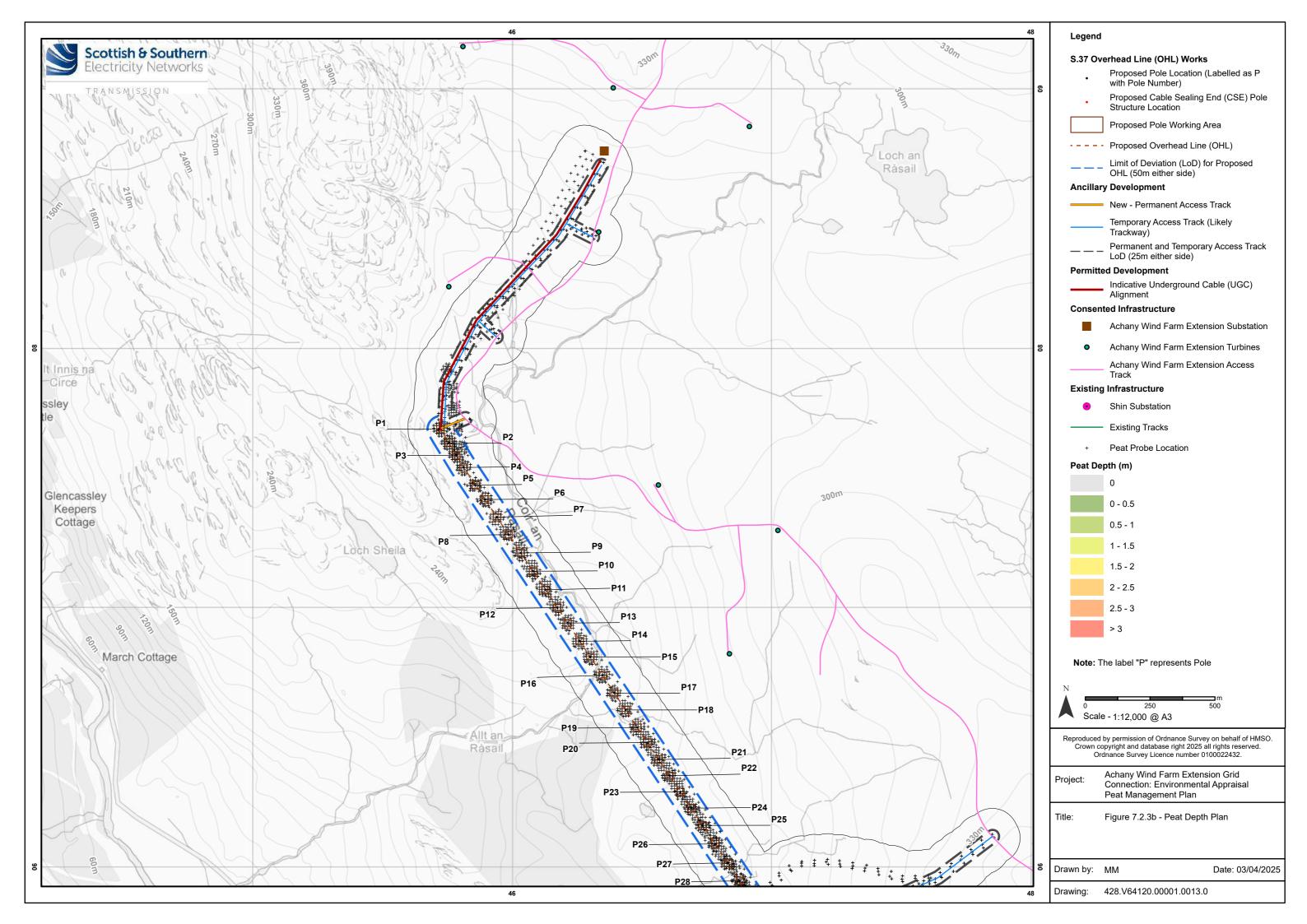


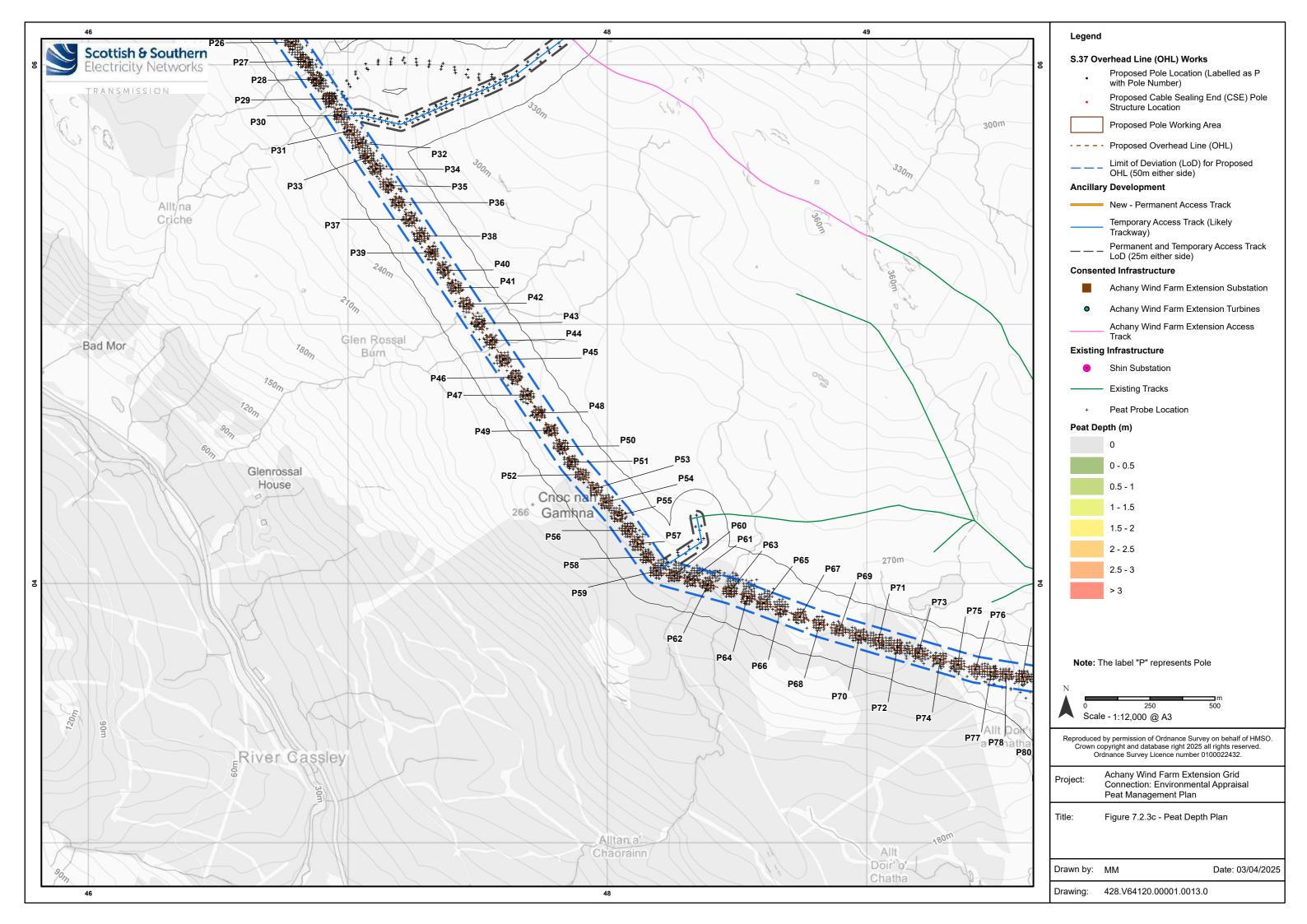


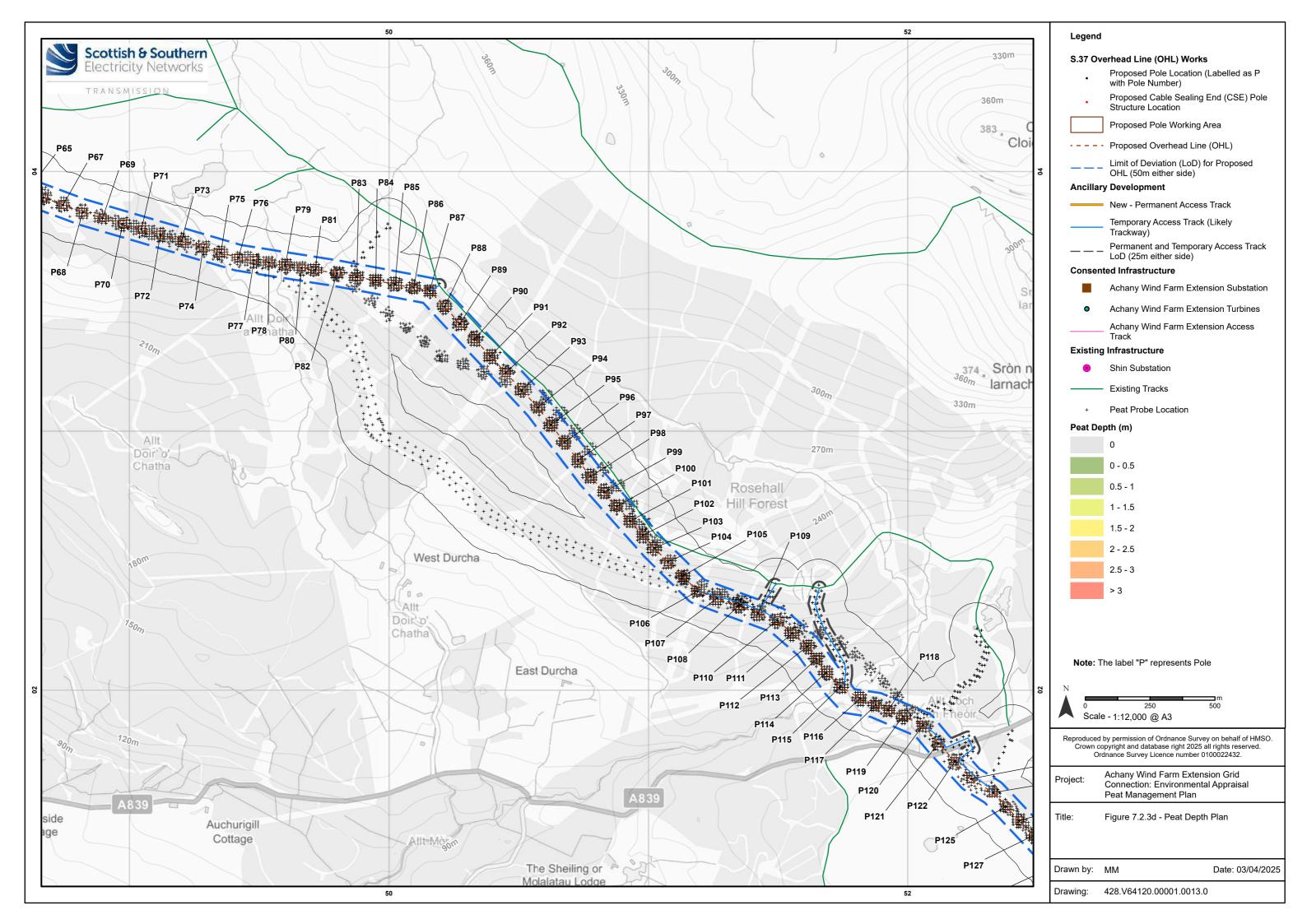


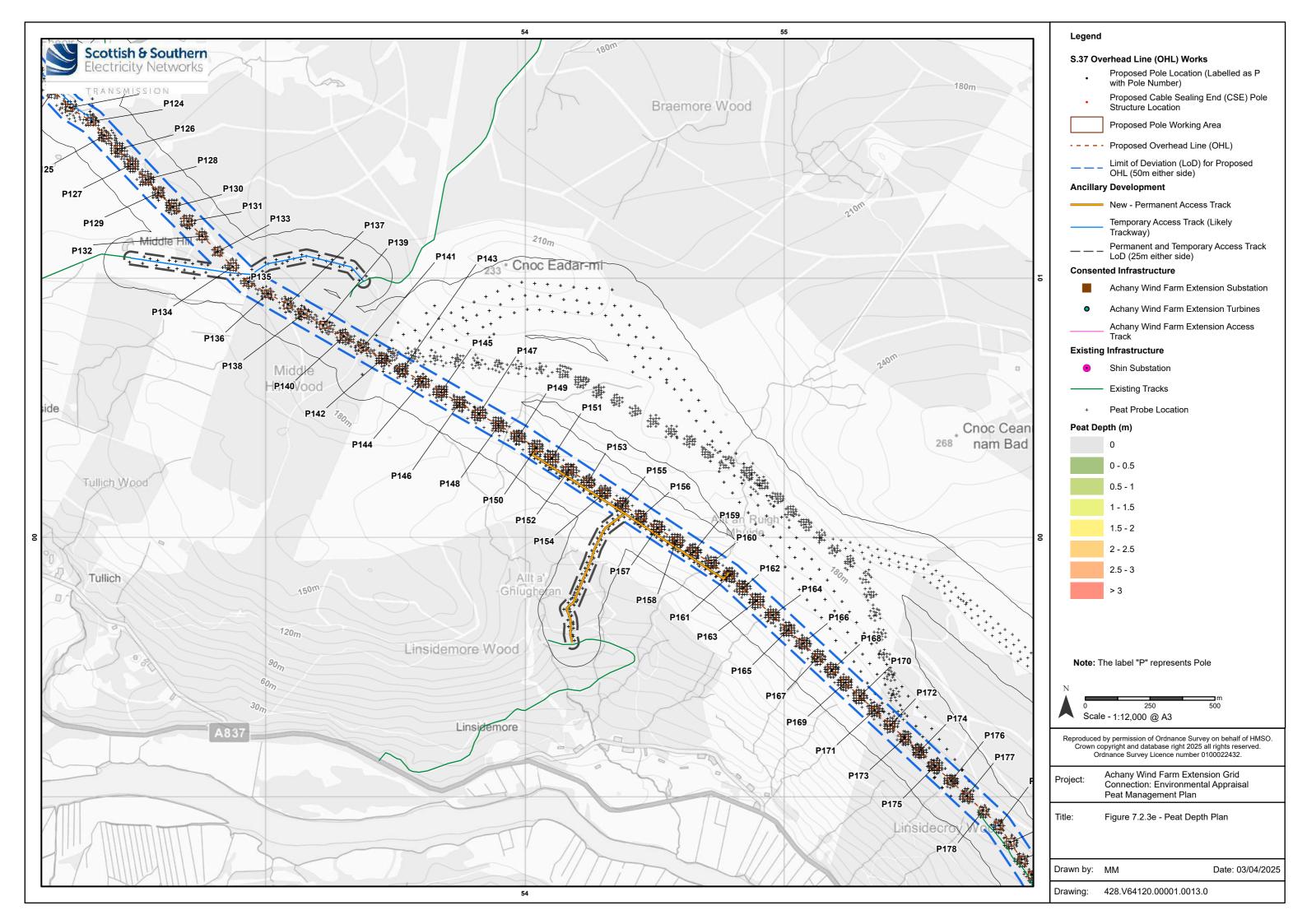


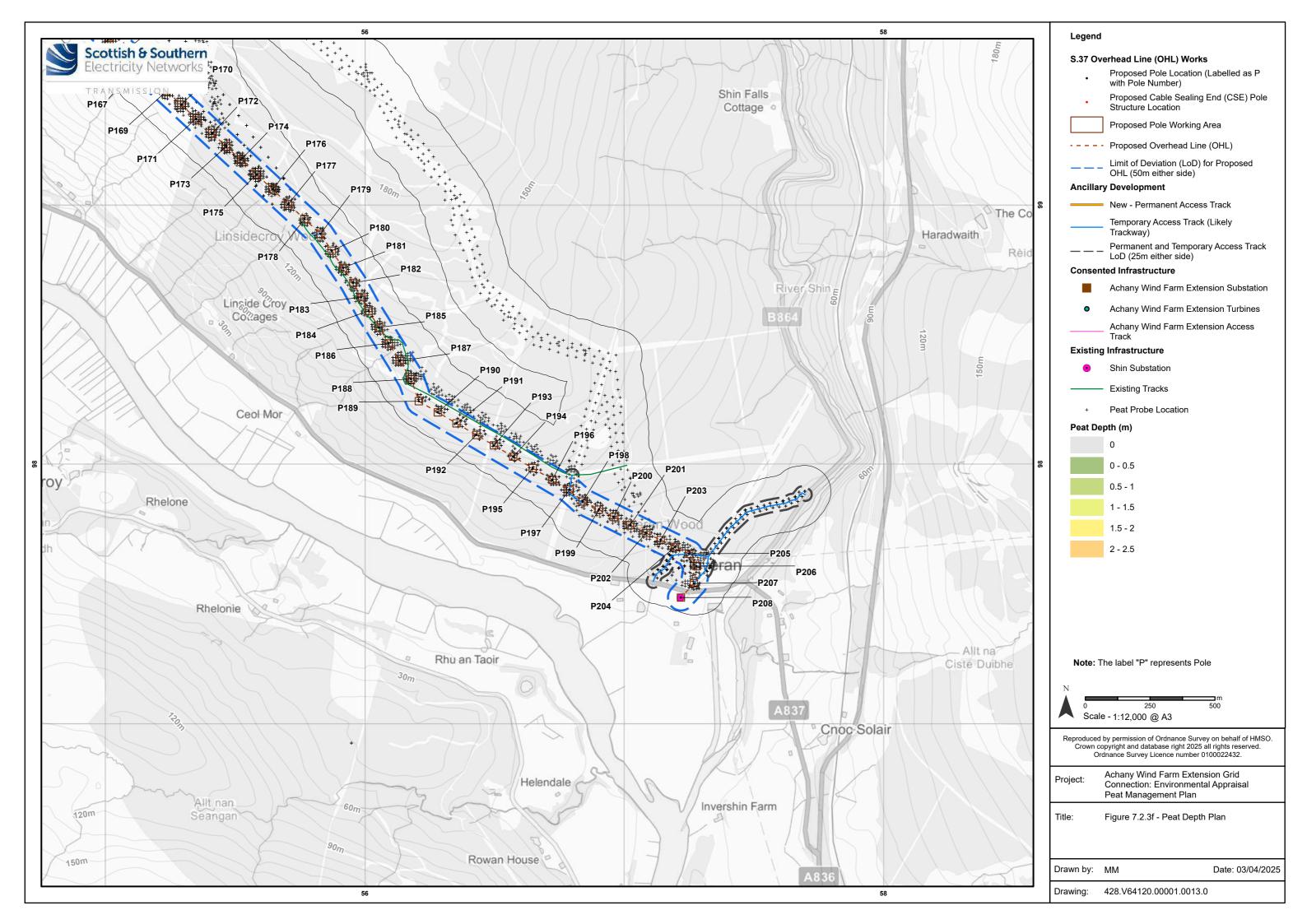


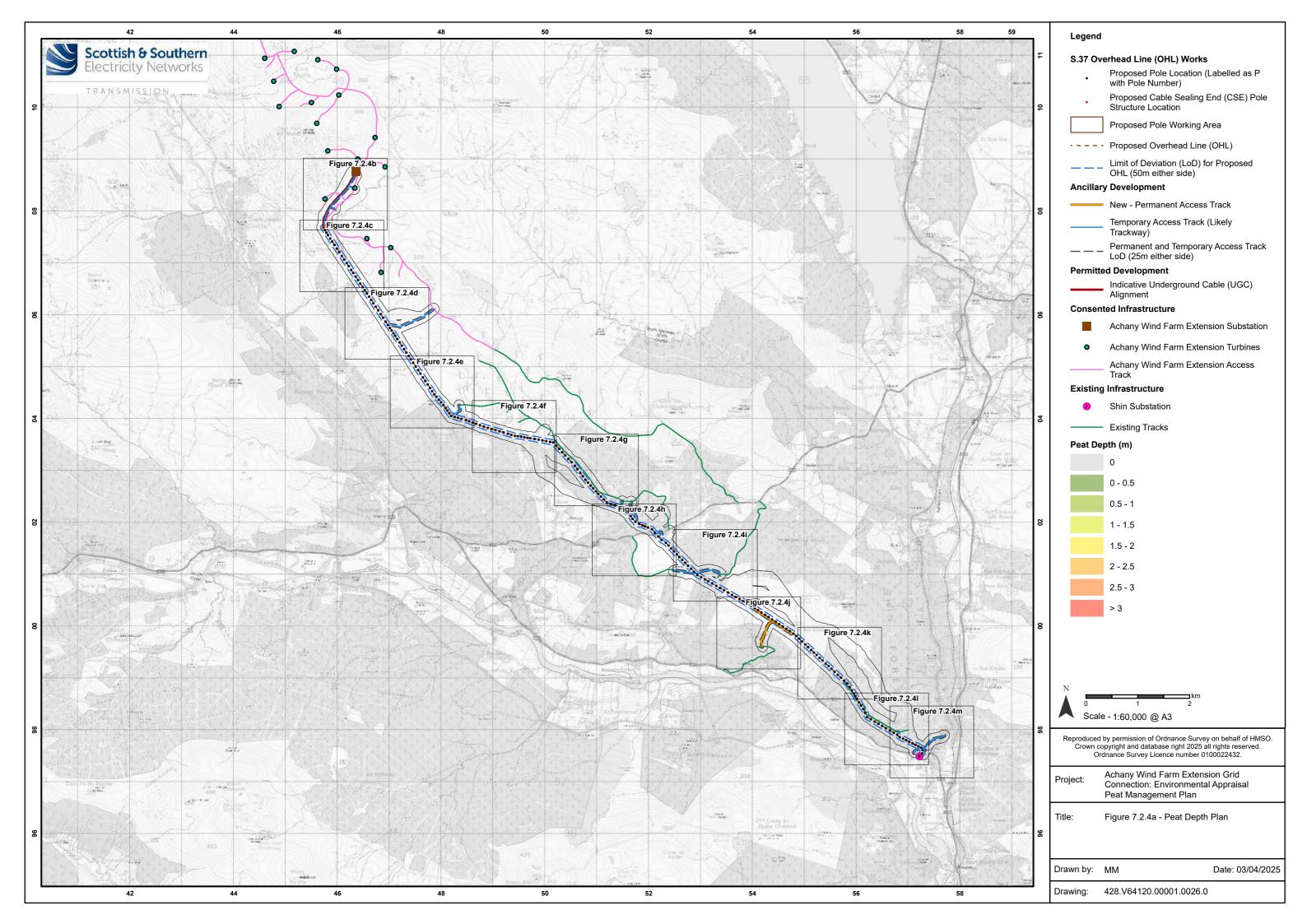


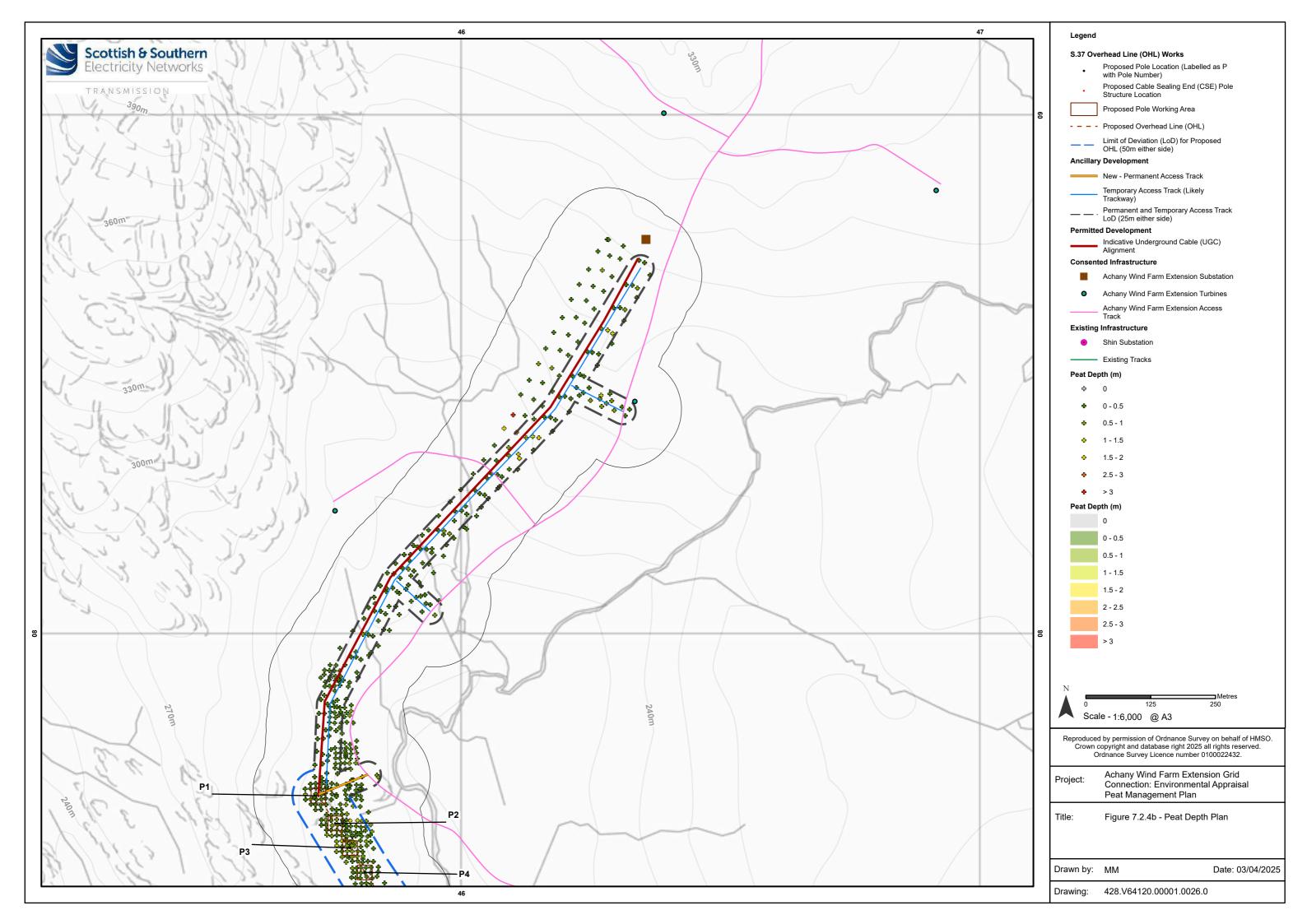


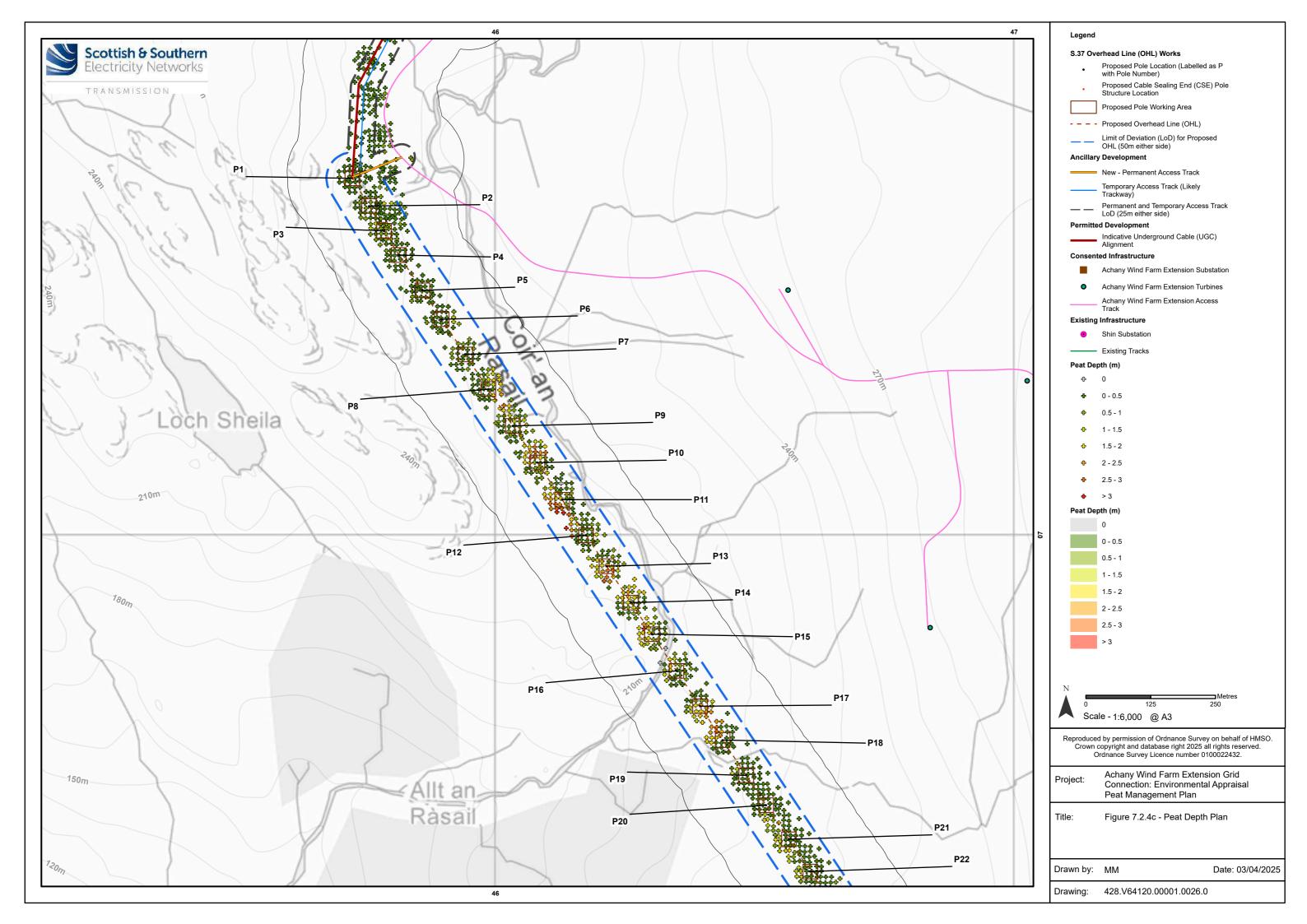


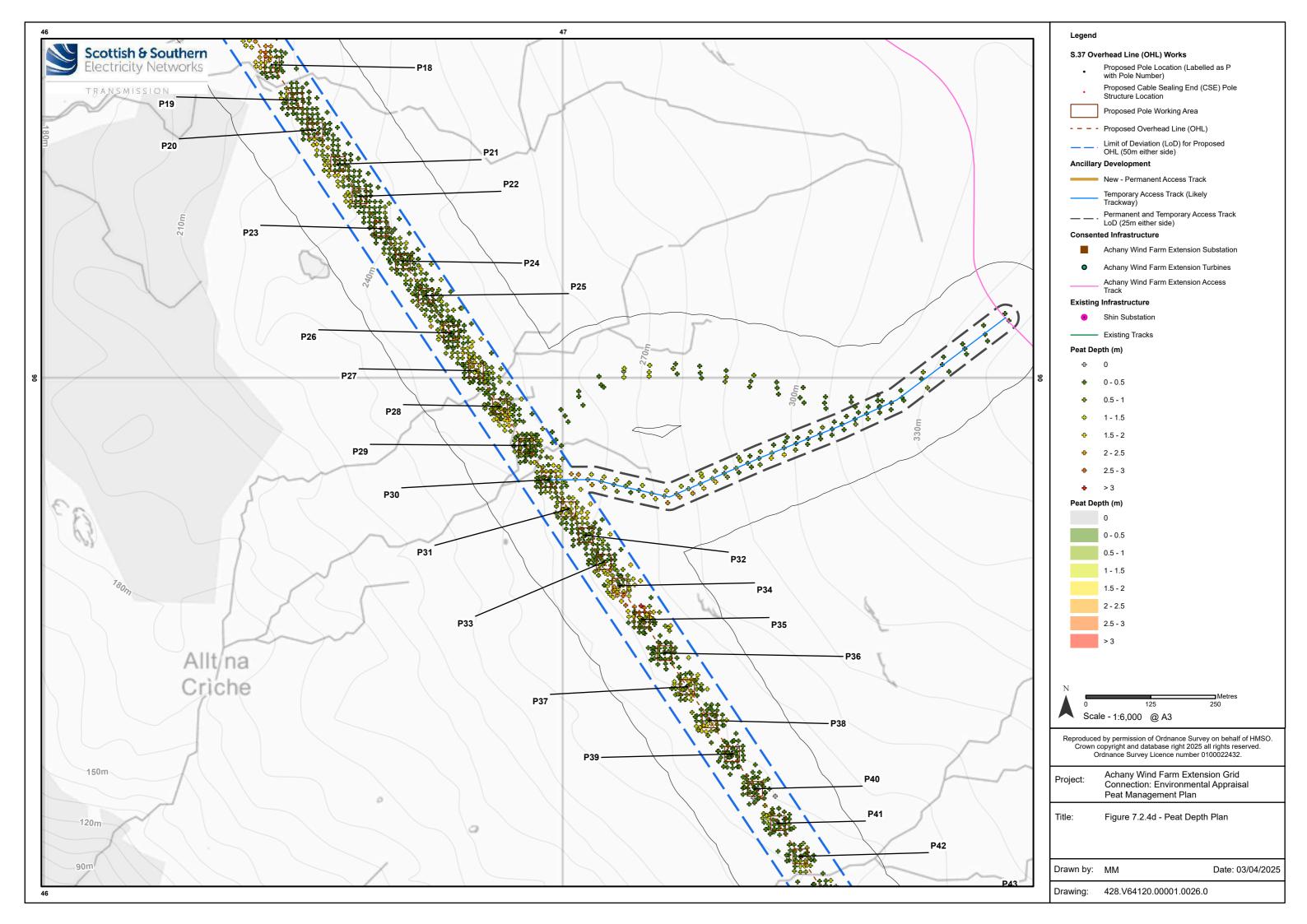


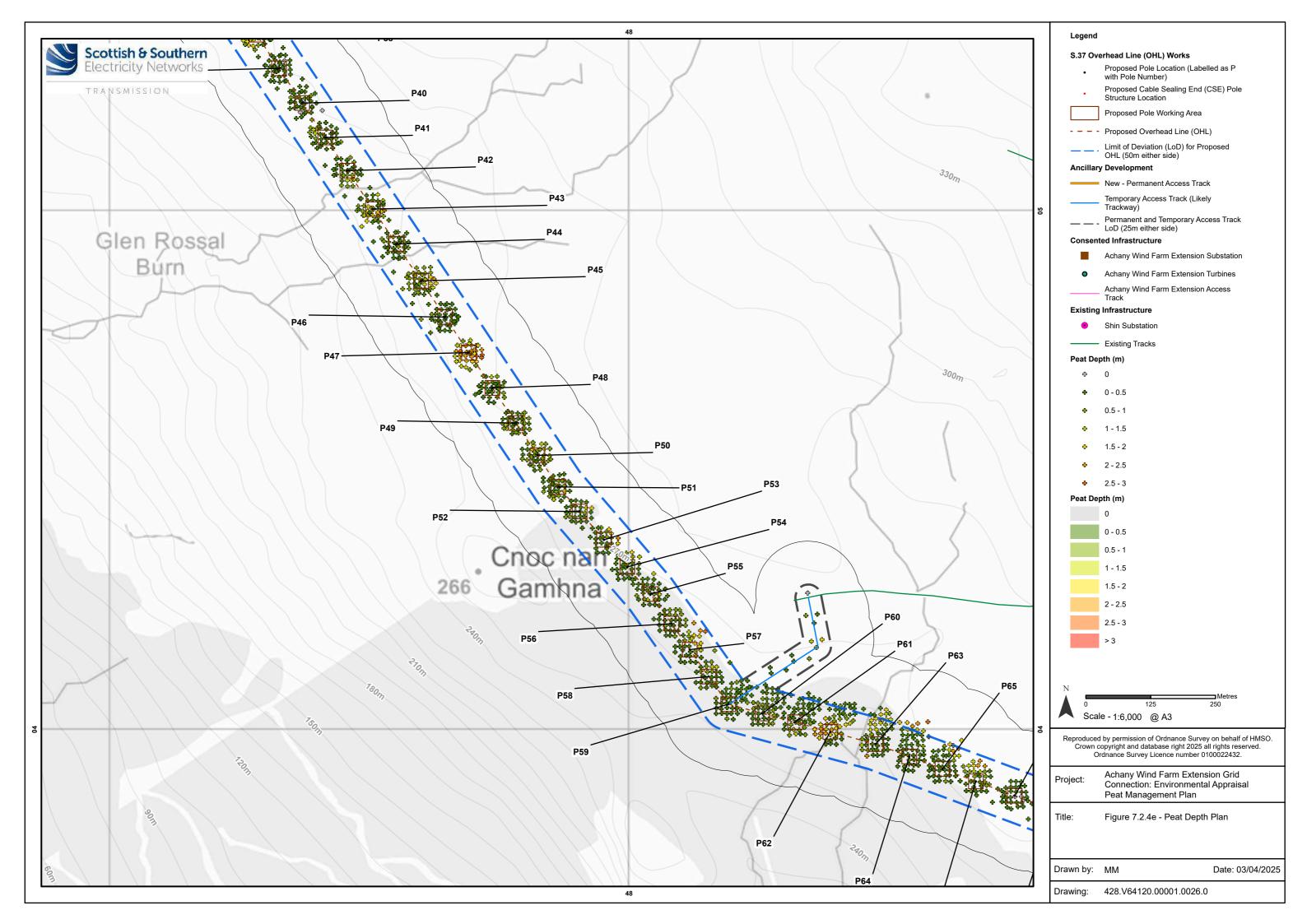


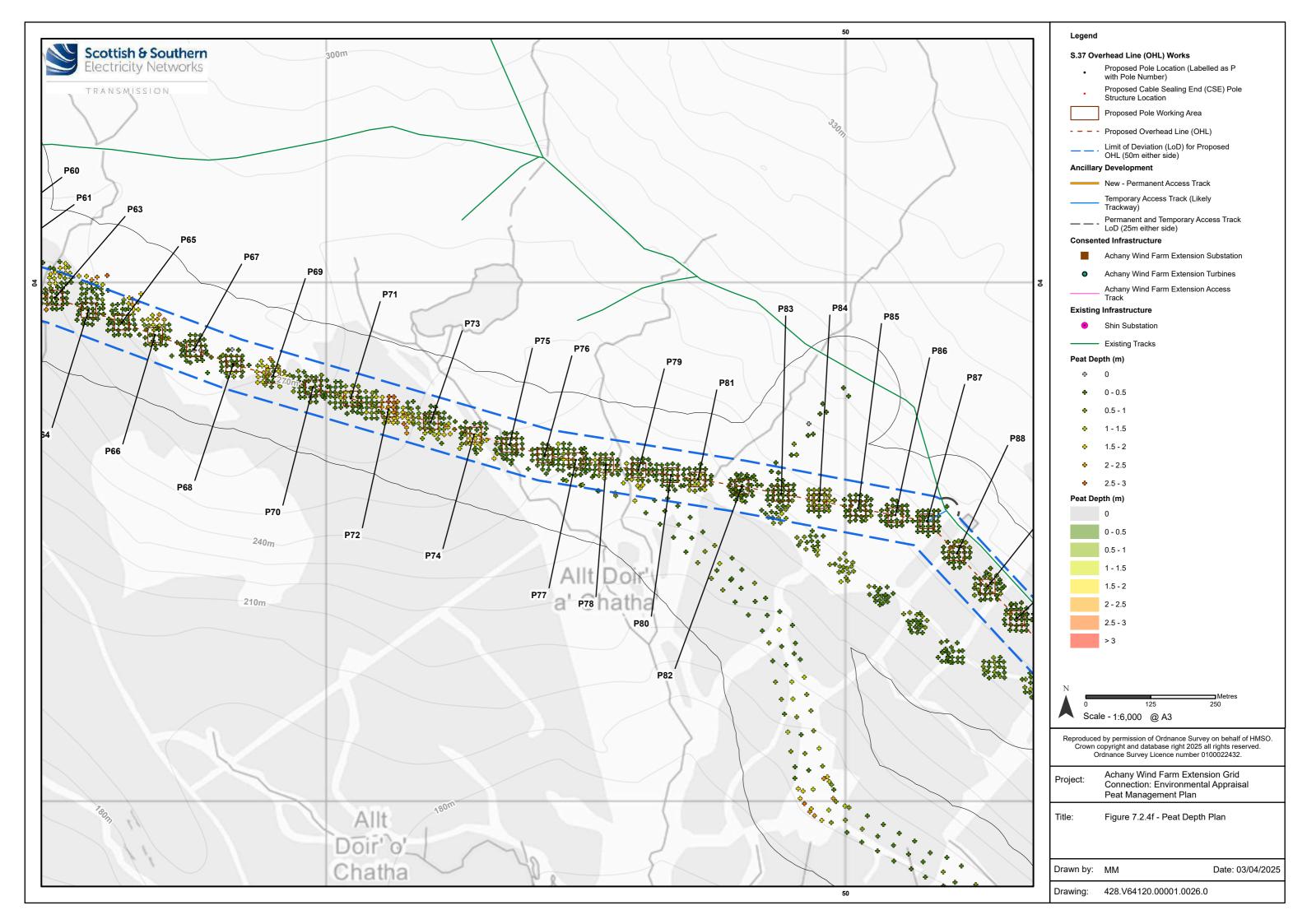


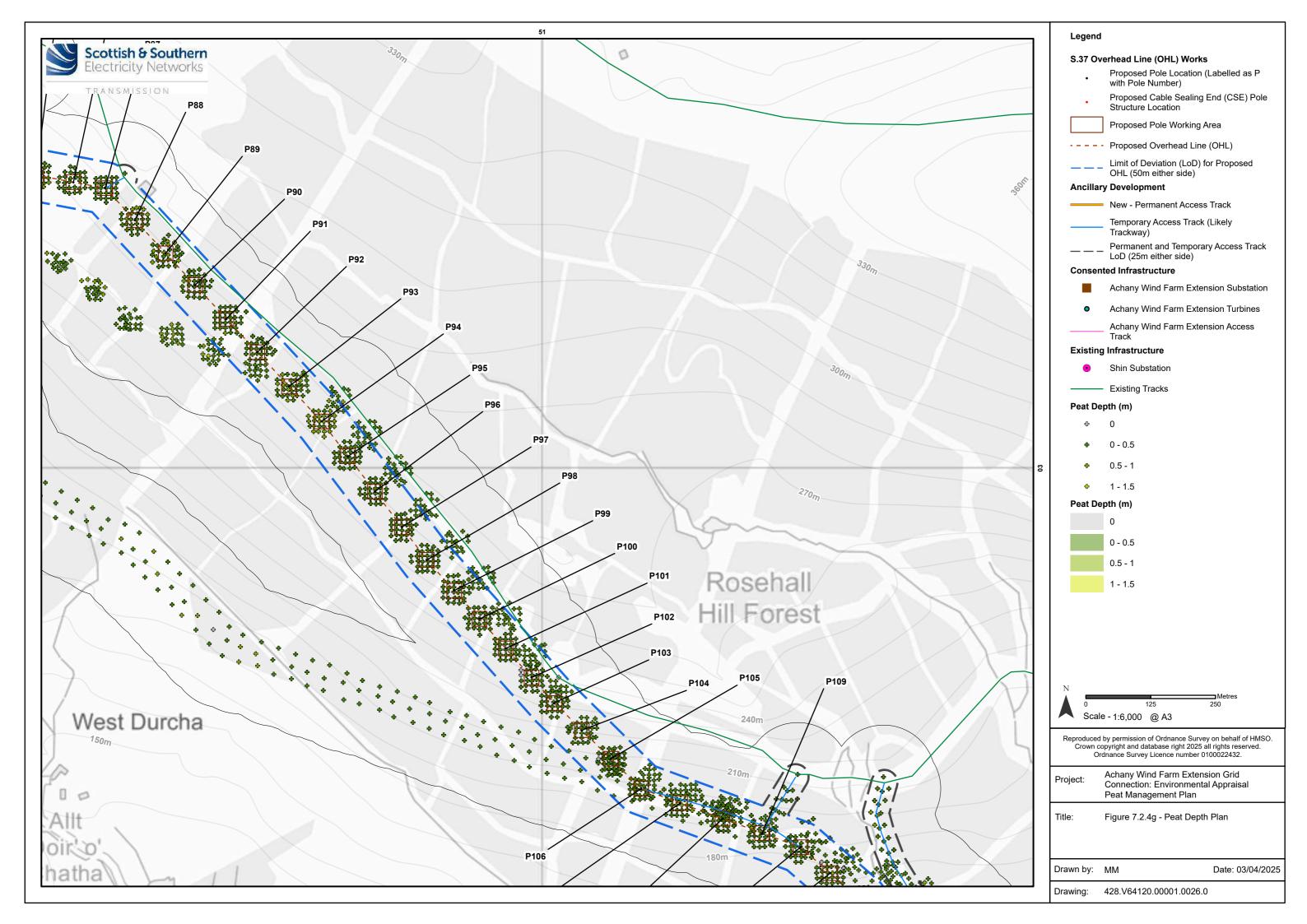


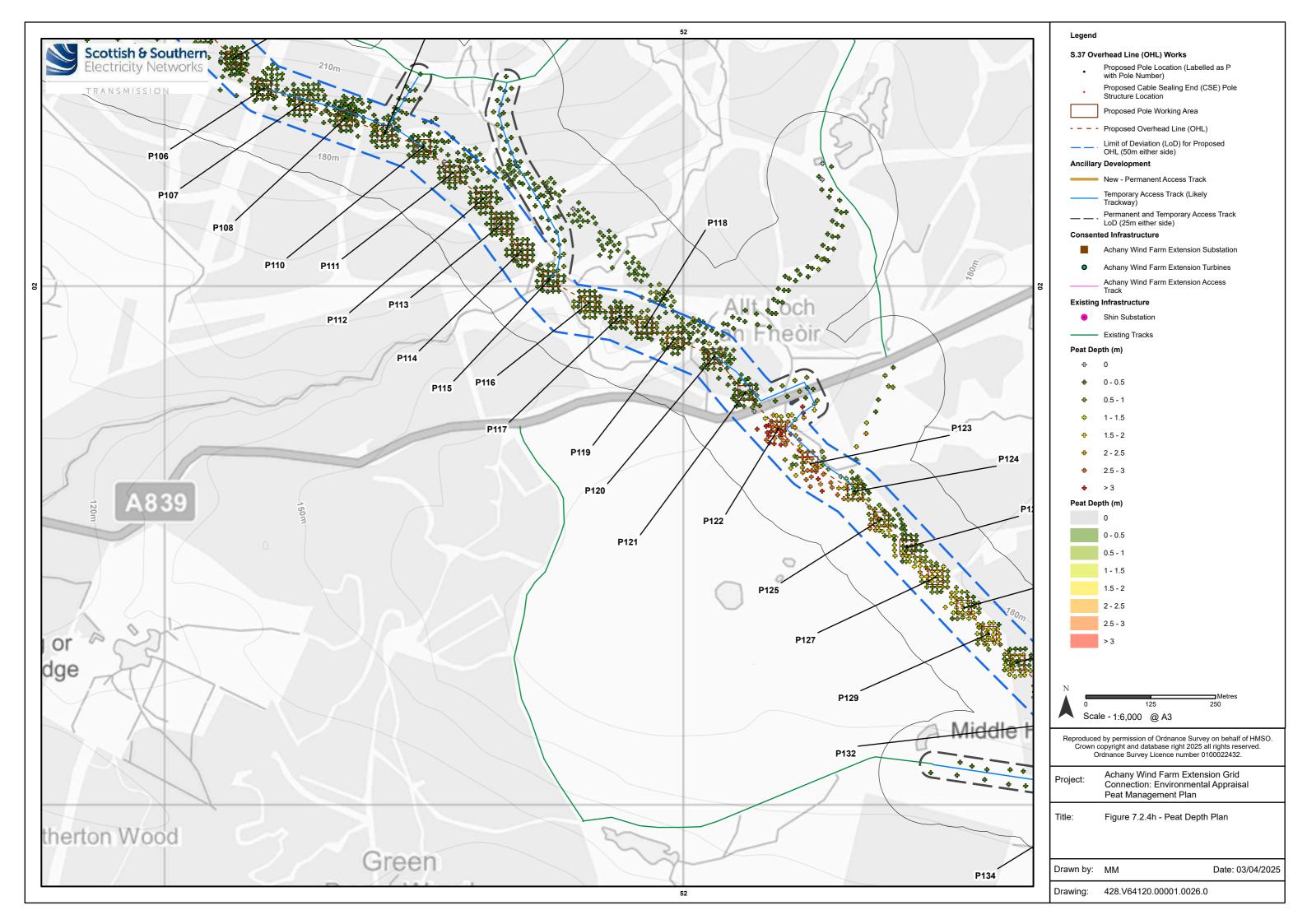


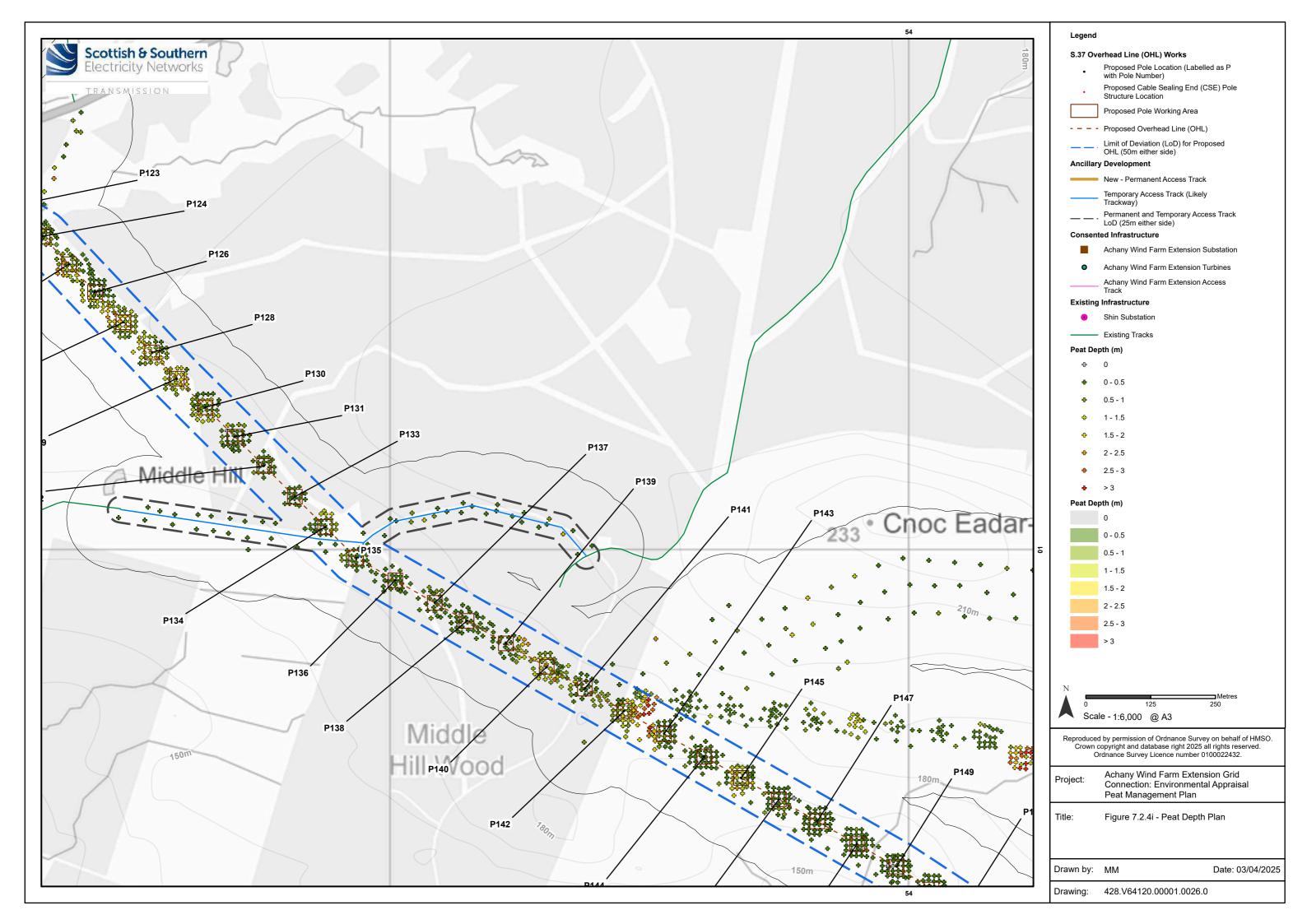


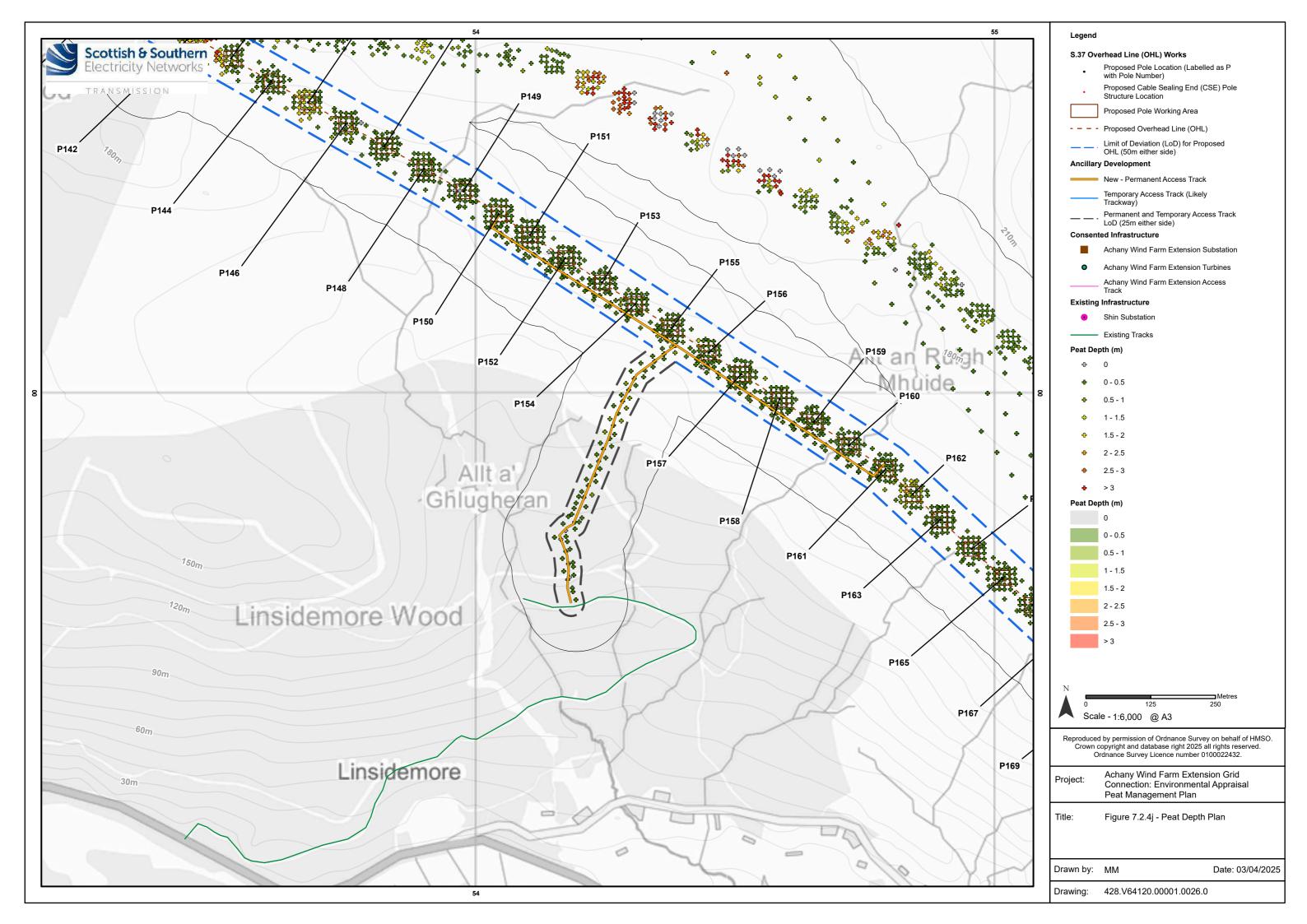


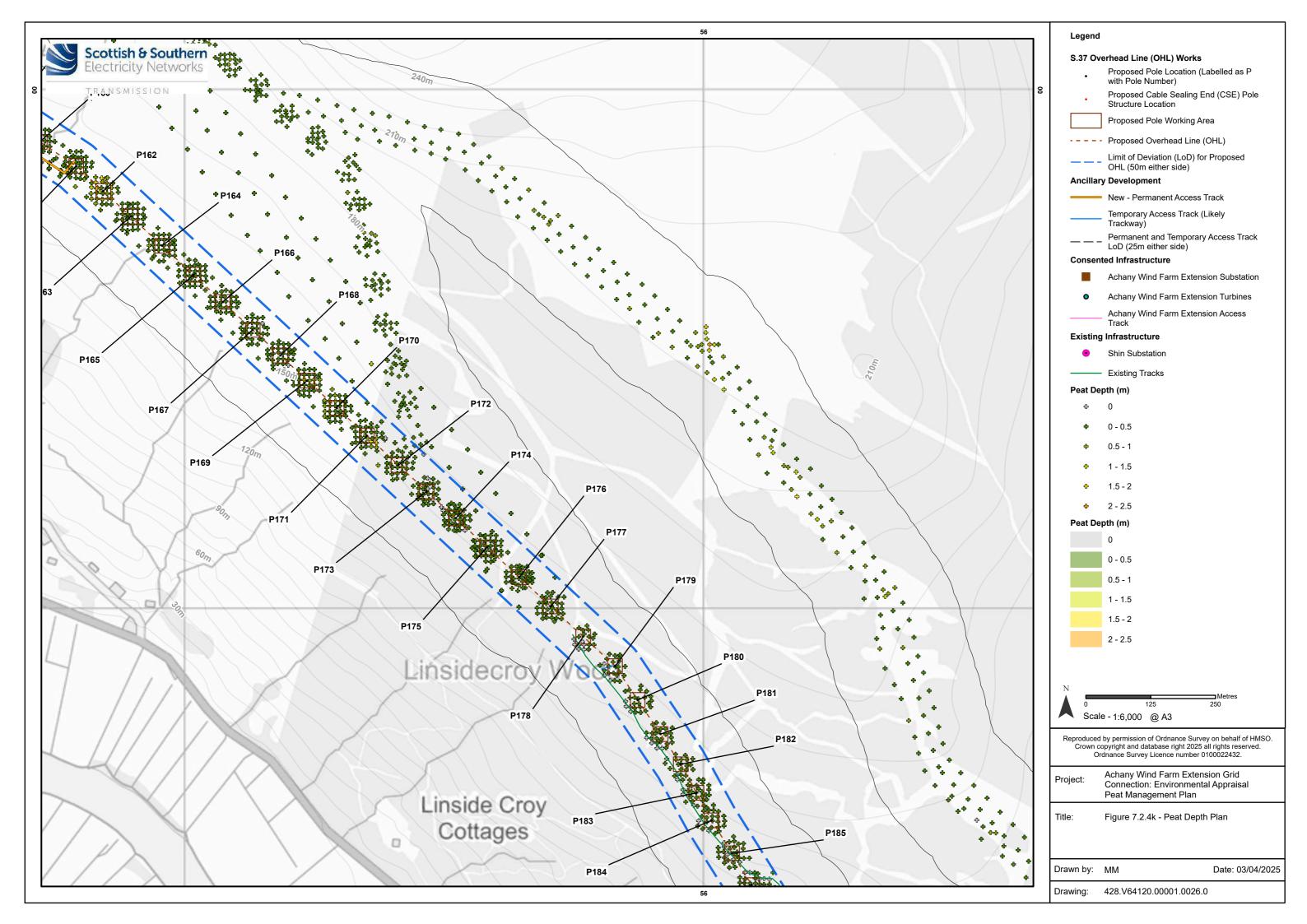


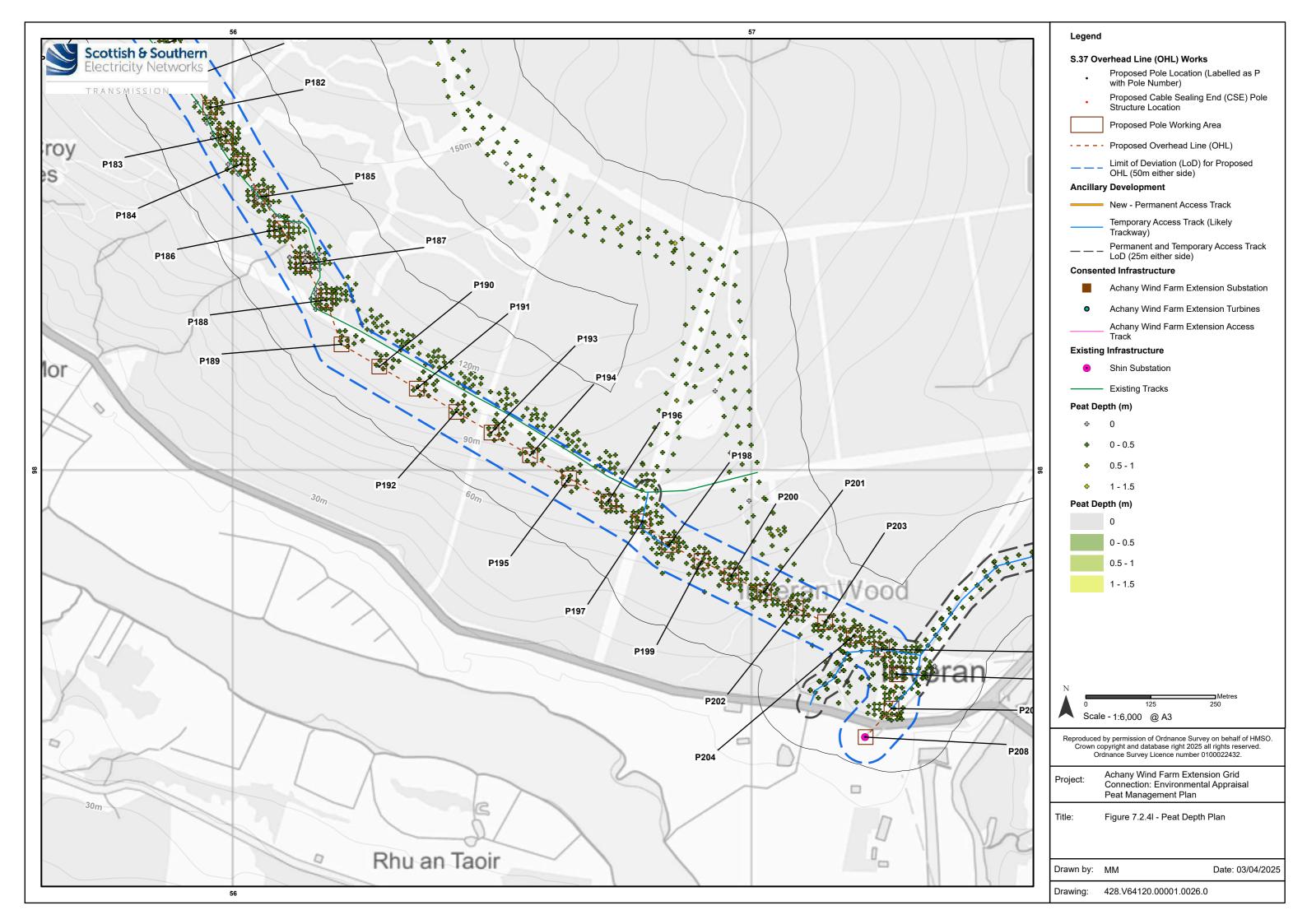


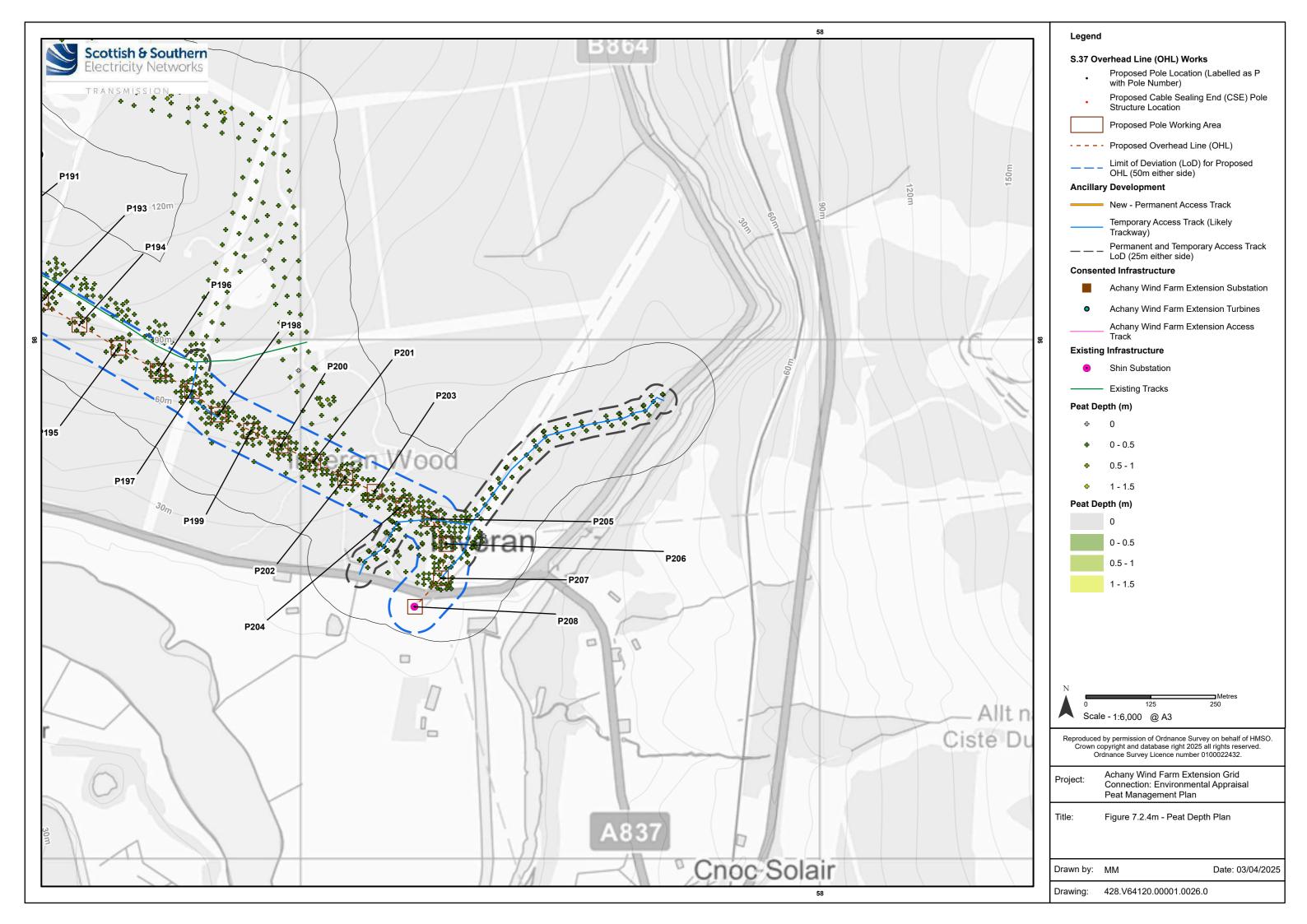


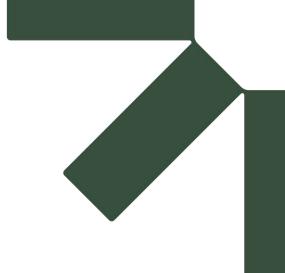












Annex A Excavated Materials Calculations

Achany Wind Farm Extension Grid Connection

Appendix 7.2: Peat Management Plan

SSEN Transmission

SLR Project No.: 428.064120.00001



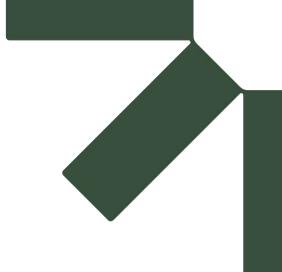
Infrastructure														Total Re-use	Total Re-use		
iiiidstructure	Length (m)	Width (m)	Area (m²)	Average Depth	Number	Volume Acrotelm Peat	Volume Catotelm Peat	Total Excavated	Length (m)	Width (m)	Area (m²)	Average Depth	Number	Volume Acrotelm Peat	Volume Catotelm Peat	Total Re-use	. Notes
				(m)		(m ³)	(m ³)	Volume (m³)				(m)		(m³)	(m ³)	Volume (m ³	
Permanent Access Track	103	5	515	0.51	1	258	5	263	103	2.5	258	0.51	2	258	5	263	Assumes re-use of 2.5m width either side of the track for verge restoration to tie into adjacent peatland habitats.
Temporary Access Track UGC	9919 1235	1.3	49595 1606	0.41 1.53	1	20334 803	1654	20334 2456	9919 1235	1.3	49595 1606	0.41 1.53	1	20334 803	1654	20334 2456	Likely to be trackway and therefore no excavations, included for reference only. Fully reinstated
Pole Number 1 Pole Number 2	-	-	200 200	0.40	1	81 75	-	81 75	-	-	200 200	0.40 0.38	1	81 75	-	81 75	Fully reinstated Fully reinstated
Pole Number 3	-	-	200	0.38 0.68	1	100	36	136	-	-	200	0.68	1	100	36	136	Fully reinstated
Pole Number 4 Pole Number 5	-	-	200 200	0.12 0.15	1	24	-	24	-	-	200 200	0.12 0.15	1	24 30	-	24 30	Fully reinstated Fully reinstated
Pole Number 6	-	-	200	0.14	1	27	<u>-</u>	27	-	-	200	0.13	1	27	-	27	Fully reinstated
Pole Number 7	-	-	200	0.09	1	18 90	-	18	-	-	200	0.09	1	18 90	-	18	Fully reinstated
Pole Number 8 Pole Number 9	-	-	200 200	0.45 0.36	1	72	-	72	-	-	200 200	0.45 0.36	1	72	-	90 72	Fully reinstated Fully reinstated
Pole Number 10	-	-	200	1.26	1	100	151	251 290	-	-	200	1.26	1	100	151	251	Fully reinstated
Pole Number 11 Pole Number 12	-	-	200 200	1.45 0.13	1	100 27	190 -	27	-	-	200 200	1.45 0.13	1	100 27	190	290 27	Fully reinstated Fully reinstated
Pole Number 13 Pole Number 14	-	-	200 200	1.72	1	100 100	243	343 261	-	-	200 200	1.72	1	100 100	243	343 261	Fully reinstated Fully reinstated
Pole Number 15	-	-	200	1.30 1.22	1	100	161 143	243	-	-	200	1.30 1.22	1	100	161 143	243	Fully reinstated
Pole Number 16	-	-	200	0.75	1	100	50	150	-	-	200	0.75	1	100	50	150	Fully reinstated
Pole Number 17 Pole Number 18	-	-	200 200	1.63 0.64	1	100 100	226 28	326 128	-	-	200 200	1.63 0.64	1	100 100	226 28	326 128	Fully reinstated Fully reinstated
Pole Number 19	-	-	200	0.15	1	31	-	31	-	-	200	0.15	1	31	-	31	Fully reinstated
Pole Number 20 Pole Number 21	-	-	200 200	0.23 0.24	1	47 48	-	47 48	-	-	200 200	0.23	1	47 48	-	47	Fully reinstated Fully reinstated
Pole Number 22	-	-	200	0.20	1	40	-	40	-	-	200	0.20	1	40	-	40	Fully reinstated Fully reinstated
Pole Number 23 Pole Number 24			200 200	0.14 0.15	<u> </u>	30	-	30	<u>-</u> -	-	200 200	0.14 0.15	<u> </u>	30		30	Fully reinstated Fully reinstated
Pole Number 25			200	0.25	1	50	-	50	-	-	200	0.25	1	50	-	50	Fully reinstated
Pole Number 26 Pole Number 27			200 200	0.36 0.87	<u> </u>	72 100	73	72 173	-	-	200 200	0.36 0.87	<u> </u>	72 100	73	72 173	Fully reinstated Fully reinstated
Pole Number 28			200	0.97	1	100	93	193	-	-	200	0.97	1	100	93	193	Fully reinstated
Pole Number 29 Pole Number 30			200 200	0.33 0.26	<u> </u>	66 52	-	66 52	-	-	200 200	0.33 0.26	<u> </u>	66 52	-	66 52	Fully reinstated Fully reinstated
Pole Number 31			200	0.94	1	100	88	188	-	-	200	0.94	1	100	88	188	Fully reinstated
Pole Number 32 Pole Number 33			200 200	0.27 0.68	1 1	54 100	35	54 135	-	-	200 200	0.27 0.68	1 1	54 100	35	54 135	Fully reinstated Fully reinstated
Pole Number 34			200	1.04	1	100	108	208	-	-	200	1.04	1	100	108	208	Fully reinstated
Pole Number 35 Pole Number 36	-		200 200	0.94 0.13	1 1	100 25	88 -	188 25	-	-	200 200	0.94 0.13	1 1	100 25	88	188 25	Fully reinstated Fully reinstated
Pole Number 37			200	0.93	1	100	87	187	-	-	200	0.93	1	100	87	187	Fully reinstated
Pole Number 38 Pole Number 39			200 200	0.94 0.11	<u>1</u> 1	100	89 -	189 22	-	-	200 200	0.94 0.11	1 1	100	89	189 22	Fully reinstated Fully reinstated
Pole Number 40			200	0.20	1	39	-	39	-	-	200	0.20	1	39	-	39	Fully reinstated
Pole Number 41 Pole Number 42			200 200	0.17 0.45	1	33 89	-	33 89	-	-	200 200	0.17 0.45	1	33 89	-	33 89	Fully reinstated Fully reinstated
Pole Number 43			200	1.31	1	100	162	262	-	-	200	1.31	1	100	162	262	Fully reinstated
Pole Number 44 Pole Number 45			200	0.43	1	87 100	<u>-</u> 84	87 184	-	-	200 200	0.43 0.92	1	87 100	84	87 184	Fully reinstated Fully reinstated
Pole Number 46			200	0.18	1	36		36	-	-	200	0.18	1	36	-	36	Fully reinstated
Pole Number 47 Pole Number 48			200	2.38 0.40	1	100	376	476 80	-	-	200 200	2.38 0.40	1	100 80	376	476 80	Fully reinstated Fully reinstated
Pole Number 49			200	0.40	1	100	13	113	-	-	200	0.57	1	100	13	113	Fully reinstated
Pole Number 50 Pole Number 51			200	0.77 0.62	1	100 100	54 25	154 125	-	-	200 200	0.77 0.62	1	100	54 25	154 125	Fully reinstated Fully reinstated
Pole Number 52			200	0.68	1	100	36	136	-	-	200	0.68	1	100	36	136	Fully reinstated
Pole Number 53 Pole Number 54			200	0.44	1	88	<u>-</u>	88 43	-	-	200 200	0.44	1	88	-	88 43	Fully reinstated Fully reinstated
Pole Number 55			200	0.64	1	100	29	129		-	200	0.64	1	100	29	129	Fully reinstated
Pole Number 56 Pole Number 57			200	0.35	1	69	- 21	69	-	-	200	0.35	1	69	- 21	69	Fully reinstated
Pole Number 58			200 200	0.61 0.53	1	100 100	21 6	121 106	-	-	200 200	0.61 0.53	1	100 100	6	121 106	Fully reinstated Fully reinstated
Pole Number 59 Pole Number 60			200 200	0.32 0.41	1	64 82	-	64 82	-	-	200 200	0.32 0.41	1	64 82	-	64 82	Fully reinstated Fully reinstated
Pole Number 61			200	0.41	1	100	37	137	-	-	200	0.69	1	100	37	137	Fully reinstated
Pole Number 62 Pole Number 63			200 200	1.74 0.27	1	100 54	248	348 54	-	-	200 200	1.74 0.27	1	100 54	248	348 54	Fully reinstated
Pole Number 64			200	0.27	1	62	<u>-</u> 	62	-	-	200	0.27	1	62		62	Fully reinstated Fully reinstated
Pole Number 65 Pole Number 66			200	0.23 0.26	1	46 51	-	46	-	-	200 200	0.23 0.26	1	46 51	-	46 51	Fully reinstated
Pole Number 67			200 200	0.26	1	51 23	<u>-</u>	51 23	-	-	200	0.26	1	23	-	23	Fully reinstated Fully reinstated
Pole Number 68			200	0.38	1	76 100	- -	76 105	-	-	200	0.38	1	76 100	-	76 105	Fully reinstated Fully reinstated
Pole Number 69 Pole Number 70			200 200	0.53 0.15	<u> </u>	100 30	<u>5</u>	105 30	-	-	200 200	0.53 0.15	1	100 30	-	105 30	Fully reinstated Fully reinstated
Pole Number 71			200	0.80	1	100	60	160	-	-	200	0.80	1	100	60	160	Fully reinstated
Pole Number 72 Pole Number 73			200 200	1.75 0.38	<u> </u>	100 76	250 -	350 76	-	-	200 200	1.75 0.38	<u> </u>	100 76	250	350 76	Fully reinstated Fully reinstated
Pole Number 74			200	1.01	1	100	102	202	-	-	200	1.01	1	100	102	202	Fully reinstated
Pole Number 75 Pole Number 76			200 200	0.12 0.11	1 1	25 21	-	25 21	-	-	200 200	0.12 0.11	1 1	25 21	-	25 21	Fully reinstated Fully reinstated
Pole Number 77			200	0.42	1	85	-	85	-	-	200	0.42	1	85	-	85	Fully reinstated
Pole Number 78 Pole Number 79			200 200	0.43 0.35	1 1	87 71	-	87 71	-	-	200 200	0.43 0.35	1 1	87 71	-	87 71	Fully reinstated Fully reinstated
Pole Number 80			200	0.15	1	30	-	30	-	-	200	0.15	1	30	-	30	Fully reinstated
Pole Number 81 Pole Number 82			200 200	1.00 0.17	1	100 34	101	201 34	-	-	200 200	1.00 0.17	1	100 34	101	201 34	Fully reinstated Fully reinstated
Pole Number 83			200	0.14	1	29	-	29	-	-	200	0.14	1	29	-	29	Fully reinstated
Pole Number 84 Pole Number 85			200 200	0.62 0.16	1	100 32	24	124 32	-	-	200 200	0.62 0.16	1	100 32	24	124 32	Fully reinstated Fully reinstated
Pole Number 86			200	0.14	1	27	-	27	-	-	200	0.14	1	27	-	27	Fully reinstated
Pole Number 87 Pole Number 88			200 200	0.23 0.31	1	47 62	-	47 62	-	-	200 200	0.23 0.31	1	47 62	-	47 62	Fully reinstated Fully reinstated
Pole Number 89			200	0.45	1	90	<u>-</u>	90	-	-	200	0.45	1	90	-	90	Fully reinstated
Pole Number 90			200	0.20	1	39	-	39	-	-	200	0.20	1	39	-	39	Fully reinstated

Infrastructure	Length (m)	Width (m) Area (m²)	Average Depth (m)	Number	Total Excavated Volume Acrotelm Peat	Total Excavated Volume Catotelm Peat	Total Excavated Volume (m³)	Length (m)	Width (m)	Area (m²)	Average Depth (m)	Number	Total Re-use Volume Acrotelm Peat	Total Re-use Volume Catotelm Peat	Total Re-use Volume (m³)	Notes
					(m³)	(m³)							(m³)	(m³)	` '	
Pole Number 91 Pole Number 92		200	0.26 0.17	1 1	52 34	-	52 34	-	-	200 200	0.26 0.17	1 1	52 34	-		Fully reinstated Fully reinstated
Pole Number 93		200	0.47	1	94	-	94	-	-	200	0.47	1	94	-		Fully reinstated
Pole Number 94		200	0.65	1	100	29	129	-	-	200	0.65	1	100	29		Fully reinstated
Pole Number 95 Pole Number 96		200	0.10 0.15	1	20	-	20 31	-	-	200 200	0.10 0.15	1	20	-		Fully reinstated Fully reinstated
Pole Number 97		200	0.13	1	27	-	27	-	-	200	0.13	1	27	-		Fully reinstated
Pole Number 98		200	0.16	1	32	-	32	-	-	200	0.16	1	32	-		Fully reinstated
Pole Number 99 Pole Number 100		200	0.18	1	35	-	35 43	-	-	200	0.18	1	35 43	-		Fully reinstated Fully reinstated
Pole Number 100		200	0.22 0.19	1	43	-	37	<u>-</u> -	-	200	0.19	<u>1</u> 1	37	-		Fully reinstated Fully reinstated
Pole Number 102		200	0.16	1	32	-	32	-	-	200	0.16	1	32	-		Fully reinstated
Pole Number 103		200	0.14	1	28	-	28	-	-	200	0.14	1	28	-		Fully reinstated
Pole Number 104 Pole Number 105		200	0.11 0.11	1	23	-	23	-	-	200 200	0.11	1	23	-		Fully reinstated Fully reinstated
Pole Number 106		200	0.17	1	33	-	33		-	200	0.17	1	33	-		Fully reinstated
Pole Number 107		200	0.42	1	83	-	83	-	-	200	0.42	1	83	-		Fully reinstated
Pole Number 108		200	0.27	1	55	-	55	-	-	200	0.27	1	55	-		Fully reinstated
Pole Number 109 Pole Number 110		200	0.29 0.24	1	58 48	-	58 48	-	-	200 200	0.29	1	58 48	-		Fully reinstated Fully reinstated
Pole Number 111		200	0.25	1	51	-	51	<u> </u>	-	200	0.25	1	51	-		Fully reinstated
Pole Number 112		200	0.16	1	33	-	33	-	-	200	0.16	1	33	-		Fully reinstated
Pole Number 113 Pole Number 114		200	0.27	1	53 56	-	53 56	-	-	200	0.27	1	53 56	-		Fully reinstated Fully reinstated
Pole Number 115		200	0.28 0.16	1	32	-	32	-	-	200 200	0.28 0.16	1	32	-		Fully reinstated Fully reinstated
Pole Number 116		200	0.49	1	99	-	99	-	-	200	0.49	1	99	-	99 F	Fully reinstated
Pole Number 117		200	0.13	1	26	-	26	-	-	200	0.13	1	26	-		Fully reinstated
Pole Number 118 Pole Number 119		200	0.44 0.56	1	89 100	- 12	89 112	-	-	200 200	0.44	1	89 100	12		Fully reinstated Fully reinstated
Pole Number 120		200	0.33	1	66	-	66	-	-	200	0.33	1	66	-		Fully reinstated
Pole Number 121		200	0.29	1	58	-	58	-	-	200	0.29	1	58	-		Fully reinstated
Pole Number 122		200	2.88	1	100	475	575	-	-	200	2.88	1	100	475		Fully reinstated
Pole Number 123 Pole Number 124		200	2.33 0.70	1	100	366 40	466 140	-	-	200 200	2.33 0.70	1	100	366 40		Fully reinstated Fully reinstated
Pole Number 125		200	1.22	1	100	145	245	-	-	200	1.22	1	100	145		Fully reinstated
Pole Number 126		200	0.47	1	94	_	94	-	-	200	0.47	1	94	-		Fully reinstated
Pole Number 127 Pole Number 128		200	1.15 1.33	1	100	129 167	229 267	-	-	200	1.15 1.33	1	100	129 167		Fully reinstated Fully reinstated
Pole Number 129		200	1.29	1	100	158	258		-	200	1.29	1	100	158		Fully reinstated
Pole Number 130		200	0.71	1	100	41	141	-	-	200	0.71	1	100	41		Fully reinstated
Pole Number 131		200	0.16	1	32	-	32	-	-	200	0.16	1	32	-		Fully reinstated
Pole Number 132 Pole Number 133		200	0.20 0.31	1	40 62	-	40 62	-	-	200 200	0.20	1	40 62	-		Fully reinstated Fully reinstated
Pole Number 134		200	0.32	1	63	-	63	-	-	200	0.32	1	63	-		Fully reinstated
Pole Number 135		200	0.25	1	51	-	51	-	-	200	0.25	1	51	-		Fully reinstated
Pole Number 137		200	0.16 0.19	1	32 38	-	32	-	-	200 200	0.16	1	32	-		Fully reinstated
Pole Number 137 Pole Number 138		200	0.19	1	38	-	38	<u>-</u> -	-	200	0.19 0.19	1	38	-		Fully reinstated Fully reinstated
Pole Number 139		200	0.19	1	39	-	39	-	-	200	0.19	1	39	-		Fully reinstated
Pole Number 140		200	1.20	1	100	139	239	-	-	200	1.20	1	100	139		Fully reinstated
Pole Number 141 Pole Number 142		200	0.30 1.15	1	60 100	131	60 231	<u>-</u>	-	200 200	0.30 1.15	1	100	131		Fully reinstated Fully reinstated
Pole Number 143		200	0.72	1	100	44	144	-	-	200	0.72	1	100	44		Fully reinstated Fully reinstated
Pole Number 144		200	0.24	1	48	1	48	-	-	200	0.24	1	48	-	48 F	Fully reinstated
Pole Number 145		200	1.00	1	100	100	200	-	-	200	1.00	1	100 57	100		Fully reinstated
Pole Number 146 Pole Number 147		200	0.29 0.19	1	38	-	38	-	-	200 200	0.29	1	38	-		Fully reinstated Fully reinstated
Pole Number 148		200	0.24	1	48	<u> </u>	48	-	-	200	0.24	1	48			Fully reinstated
Pole Number 149		200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20 F	Fully reinstated
Pole Number 150		200	0.15	1	29 43	-	29 43	-	-	200	0.15	1	29 43	-		Fully reinstated
Pole Number 151 Pole Number 152		200	0.21 0.10	1	20	<u>-</u>	20	-	-	200 200	0.21	1	20	-		Fully reinstated Fully reinstated
Pole Number 153		200	0.17	1	34	-	34	-	-	200	0.17	1	34	-		Fully reinstated
Pole Number 154		200	0.31	1	62	-	62	-	-	200	0.31	1	62	-		Fully reinstated
Pole Number 155 Pole Number 156		200	0.10	1	20 39	-	20 39	-	-	200	0.10	1	20 39	-		Fully reinstated Fully reinstated
Pole Number 157		200	0.24	1	49	-	49	<u>-</u>	-	200	0.24	1	49	-		Fully reinstated
Pole Number 158		200	0.24	1	48	1	48	-	-	200	0.24	1	48	-	48 F	Fully reinstated
Pole Number 159		200	0.21	1	41	-	41	-	-	200	0.21	1	41	-		Fully reinstated
Pole Number 160 Pole Number 161		200	0.20 0.10	1	40 19	-	40 19	-	-	200 200	0.20 0.10	1	40 19	-		Fully reinstated Fully reinstated
Pole Number 162		200	0.75	1	100	51	151	-	-	200	0.75	1	100	51		Fully reinstated
Pole Number 163		200	0.23	1	47	-	47	-	-	200	0.23	1	47	-	47 F	Fully reinstated
Pole Number 164		200	0.22 0.18	1	45 36	-	45 36	-	-	200	0.22 0.18	1	45 36	-		Fully reinstated
Pole Number 165 Pole Number 166		200	0.18	1	33	-	36	-	-	200 200	0.18	1	35	-		Fully reinstated Fully reinstated
Pole Number 167		200	0.10	1	20		20	-	-	200	0.10	1	20	-		Fully reinstated
Pole Number 168		200	0.10	1	20	-	20	-	-	200	0.10	1	20	-		Fully reinstated
Pole Number 169 Pole Number 170		200	0.36 0.36	1	72 73	-	72 73	-	-	200	0.36	1	72 73	-		Fully reinstated Fully reinstated
i die ivaniber 170		1 200	1 0.30	1	/3	<u>-</u>	73	-	<u> </u>	200	0.30	1	1 /3	<u>-</u>	/3	runy remotated

21/10/2024

						Total Excavated	Total Excavated							Total Re-use	Total Re-use		
				Average Depth		Volume	Volume	Total Excavated			,	Average Depth		Volume	Volume	Total Re-use	
Infrastructure	Length (m)	Width (m)	Area (m²)	(m)	Number	Acrotelm Peat	Catotelm Peat	Volume (m³)	Length (m)	Width (m)	Area (m²)	(m)	Number	Acrotelm Peat	Catotelm Peat	Volume (m³)	Notes
				(,		(m³)	(m³)	Tolume (iii)				(,		(m³)	(m³)	Tolume (m)	
e Number 171			200	0.42	1	84	-	84	-	-	200	0.42	1	84	-	84	Fully reinstated
Number 172			200	0.20	1	40	-	40	-	-	200	0.20	1	40	-	40	Fully reinstated
e Number 173			200	0.10	1	19	-	19	-	-	200	0.10	1	19	-	19	Fully reinstated
e Number 174			200	0.11	1	23	-	23	-	-	200	0.11	1	23	-	23	Fully reinstated
Number 175			200	0.24	1	48	-	48	-	-	200	0.24	1	48	-	48	Fully reinstated
Number 176			200	0.16	1	31	-	31	-	-	200	0.16	1	31	-	31	Fully reinstated
e Number 177			200	0.13	1	26	-	26	-	-	200	0.13	1	26	-	26	Fully reinstated
Number 178			200	0.07	1	15	-	15	-	-	200	0.07	1	15	-	15	Fully reinstated
Number 179			200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
e Number 180			200	0.09	1	19	-	19	-	-	200	0.09	1	19	-	19	Fully reinstated
e Number 181			200	0.14	1	28	-	28	-	-	200	0.14	1	28	-	28	Fully reinstated
e Number 182			200	0.13	1	26	-	26	-	-	200	0.13	1	26	-	26	Fully reinstated
Number 183			200	0.13	1	26	-	26	-	-	200	0.13	1	26	-	26	Fully reinstated
Number 184			200	0.16	1	32	-	32	-	-	200	0.16	1	32	-	32	Fully reinstated
Number 185			200	0.09	1	17	-	17	-	-	200	0.09	1	17	-	17	Fully reinstated
Number 186			200	0.12	1	25	-	25	-	-	200	0.12	1	25	-	25	Fully reinstated
Number 187			200	0.08	1	16	-	16	-	-	200	0.08	1	16	-	16	Fully reinstated
Number 188			200	0.15	1	30	-	30	-	-	200	0.15	1	30	-	30	Fully reinstated
e Number 189			200	0.20	1	40	-	40	-	-	200	0.20	1	40	-	40	Fully reinstated
Number 190			200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
Number 191			200	0.14	1	28	-	28	-	-	200	0.14	1	28	-	28	Fully reinstated
e Number 192			200	0.13	1	25	-	25	-	-	200	0.13	1	25	-	25	Fully reinstated
e Number 193	-	-	200	0.27	1	53	-	53	-	-	200	0.27	1	53	-	53	Fully reinstated
e Number 194	-	-	200	0.20	1	41	-	41	-	-	200	0.20	1	41	-	41	Fully reinstated
e Number 195	-	-	200	0.12	1	25	-	25	-	-	200	0.12	1	25	-	25	Fully reinstated
Number 196	-	-	200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
Number 197	-	-	200	0.20	1	41	-	41	-	-	200	0.20	1	41	-	41	Fully reinstated
Number 198	-	-	200	0.16	1	32	-	32	-	-	200	0.16	1	32	-	32	Fully reinstated
Number 199	-	-	200	0.11	1	22	-	22	-	-	200	0.11	1	22	-	22	Fully reinstated
Number 200	-	-	200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
Number 201	-	-	200	0.10	1	21	-	21	-	-	200	0.10	1	21	-		Fully reinstated
Number 202	-	-	200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
Number 203	-	-	200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
Number 204	-	-	200	0.12	1	24	-	24	-	-	200	0.12	1	24	-	24	Fully reinstated
Number 205	-	-	200	0.12	1	23	-	23	-	-	200	0.12	1	23	-	23	Fully reinstated
Number 206	-	-	200	0.12	1	23	-	23	-	-	200	0.12	1	23	-	23	Fully reinstated
Number 207	-	-	200	0.10	1	20	-	20	-	-	200	0.10	1	20	-	20	Fully reinstated
Number 208	-	-	200	0.08		16	_	16	-	_	200	0.08	1	16	-	16	Fully reinstated

Total Excavated Volume Acrotelm Peat (m ³)	33169
Total Excavated Volume Catotelm Peat (m ³)	721
Total Excavated Volume Peat (m ³)	4038
Total Re-use Volume Acrotelm Peat (m ³)	3316
Total Re-use Volume Catotelm Peat (m ³)	7212
Total Re-use Volume of Peat (m ³)	4038
Net Balance (m ³)	_



Annex B Peat Coring Data

Achany Wind Farm Extension Grid Connection

Appendix 7.2: Peat Management Plan

SSEN Transmission

SLR Project No.: 428.064120.00001





Hole No.

PC01

Project: Achany Wind Farm Grid Connection Client: Scottish & Southern Electricity Networks Dates: 25-08-2023

Project No: 428.V64120.00001 Logger: ET Approved By: AH Coordinates: E: 252159.00 N: 901704.00

Location: Achany, Lairg Hole Type: HA Level: Vertical Scale: 1:26

	, teriarry, Earry			Hole Type: Tirt		ı		vertical scare. 1.20
Water	Depth (m)	Sample Type	Depth	Recovery (%)	Depth (m) / Discontinuity Detail	Level (mAOD)	Legend	Stratum Description
	0.00 - 1.00 -						e alle alle solle alle alle solle alle	Dark brown fibrous PEAT (H3, B2).
	1.00 - 2.00	С	0.00 - 1.00	Recovery = 80%	1.00		to alke	Dark brown pseudo-fibrous PEAT (H4, B2).
	2.00 - 3.00	С	1.00 - 2.00	Recovery = 20%	2.00		alle alle al e alle	Dark brown pseudo-fibrous PEAT (H5, B2).
	3 -	C	2.00 - 3.00	Recovery = 50%	3.00		to silto silto	Peat Core Complete at 3.00m
	4 -							

Remarks:



Hole No.

PC02Sheet 1 of 1

 Project: Achany Wind Farm Grid Connection
 Client: Scottish & Southern Electricity Networks
 Dates:
 25-08-2023

 Project No: 428.V64120.00001
 Logger: ET
 Approved By: AH
 Coordinates:
 E: 252286.00 N: 901612.00

 Location: Achany, Lairg
 Hole Type: HA
 Level:
 Vertical Scale:
 1:26

Water Depth (m) Sample Type Depth Recovery (%) Depth (m) / Discontinuity Detail (mAOD) Legend Stratum Description Stratum Description Stratum Description	
0.00 - 1.00 - Continue of the state of th	
1 Recovery Silver Silve	
1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 1.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.00 - 2.	1
2.00 Recovery = 80% 2.00 Side side side side side side side side s	plant remains 2
2.00 - 3.00 Solid	3
	4
	5

Remarks:



Hole No.

PC03

Project: Achany Wind Farm Grid Connection Client: Scottish & Southern Electricity Networks Dates: 25-08-2023

Project No: 428.V64120.00001 Logger: ET Approved By: AH Coordinates: E: 252330.00 N: 901615.00

Location: Achany, Lairg Hole Type: HA Level: Vertical Scale: 1:26

	, teriarry, Earry			Tiole Type: Tirt	Leven			Vertical Scale. 1.20	
Water	Depth (m)	Sample Type	Depth	Recovery (%)	Depth (m) / Discontinuity Detail	Level (mAOD)		Stratum Description	
	0.00 - 1.00 -						alle alle a s alle alle alle salle alle alle salle alle alle alle alle alle alle alle	Dark brown fibrous PEAT (H3, B2).	
	1	С	0.00 - 1.00	Recovery	1.00		s alis alis alis alis alis alis alis alis alis alis alis	Dark brown pseudo-fibrous PEAT. Frequent plant remains	
	1.00 - 1.50			= 85%			316 316 3 6 316 316 3 8 316 316 8 316 316 3	present (H4, B2).	
	- -	С	1.00 - 1.50	Recovery = 100%	1.50		હ કોહ કોહ કોહ કોહ ક	Peat Core Complete at 1.50m	
	2 -								
	-								
	3 -								
	-								
	4 -								
	- ,								

Remarks:



Hole No.

PC04

Project: Achany Wind Farm Grid Connection Client: Scottish & Southern Electricity Networks Dates: 25-08-2023

Project No: 428.V64120.00001 Logger: ET Approved By: AH Coordinates: E: 248641.00 N: 903978.00

Location: Achany, Lairg Hole Type: HA Level: Vertical Scale: 1:26

	, teriarry, carry			riole type. Tirt	Leven			Vertical Scarc. 1.20	
Water	Depth (m)	Sample Type	Depth	Recovery (%)	Depth (m) / Discontinuity Detail	Level (mAOD)	Legend	Stratum Description	
	0.00 - 1.00						e allic alli	Dark brown fibrous PEAT (H3, B2).	
_	1.00 - 1.70	c	0.00 - 1.00	Recovery = 90%	1.00		alk alk a k alk alk alk alk a k alk alk a k alk alk k alk	Dark brown pseudo-fibrous PEAT (H4, B2).	-
-		- с -	1.00 - 1.70	Recovery = 100%	1.70		k sik sik	Peat Core Complete at 1.70m	
	2 -								
	3 -								
	-								
	4 -								
	-								
	-								1

Remarks:



Hole No.

PC05

Project: Achany Wind Farm Grid Connection Client: Scottish & Southern Electricity Networks Dates: 25-08-2023

Project No: 428.V64120.00001 Logger: ET Approved By: AH Coordinates: E: 248576.00 N: 904014.00

Location: Achany, Lairg Hole Type: HA Level: Vertical Scale: 1:26

	, teriarry, Earry			riole Type: Tirt	Level.			Vertical Scale. 1.20
Water	Depth (m)	Sample Type	Depth	Recovery (%)	Depth (m) / Discontinuity Detail	Level (mAOD)	Legend	Stratum Description
	0.00 - 1.00 -						silic silic s silic sil	Dark brown fibrous PEAT (H4, B2).
	1.00 - 2.60	C	0.00 - 1.00	Recovery = 80%	1.00		Ale	Dark brown pseudo-fibrous PEAT. Occasional plant remains present (H4, B2).
_	- -	C	1.00 - 2.60	Recovery = 100%	2.60		alk alk a s alk alk alk alk a s alk alk alk alk a	Peat Core Complete at 2.60m
	3 -							
	4 -							

Remarks:



Peat Auger 01 0 – 1.0m



Peat Auger 01 1.0 – 2.0m



Floor 2 4 Redheughs Rigg South Gyle Edinburgh EH12 9DQ

Tel: 0131 335 6830 Fax: 0131 335 6831

Web: www.slrconsulting.com

ACHANY WIND FARM GRID CONNECTION



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Peat Auger 01 2.0 – 3.0m



Peat Auger 02

0 - 1.0 m



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Peat Auger 02 1.0 – 2.0m



Peat Auger 02

2.0 - 3.0 m



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Peat Auger 03 0 - 1.0 m



Peat Auger 03

1.0 – 1.5m



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Peat Auger 04 0 – 1.0m



Peat Auger 04

1.0 – 1.7m



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Peat Auger 05

0 - 1.0 m



Peat Auger 05

1.0 – 2.0m



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Peat Auger 05 2.0 – 2.6m



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