

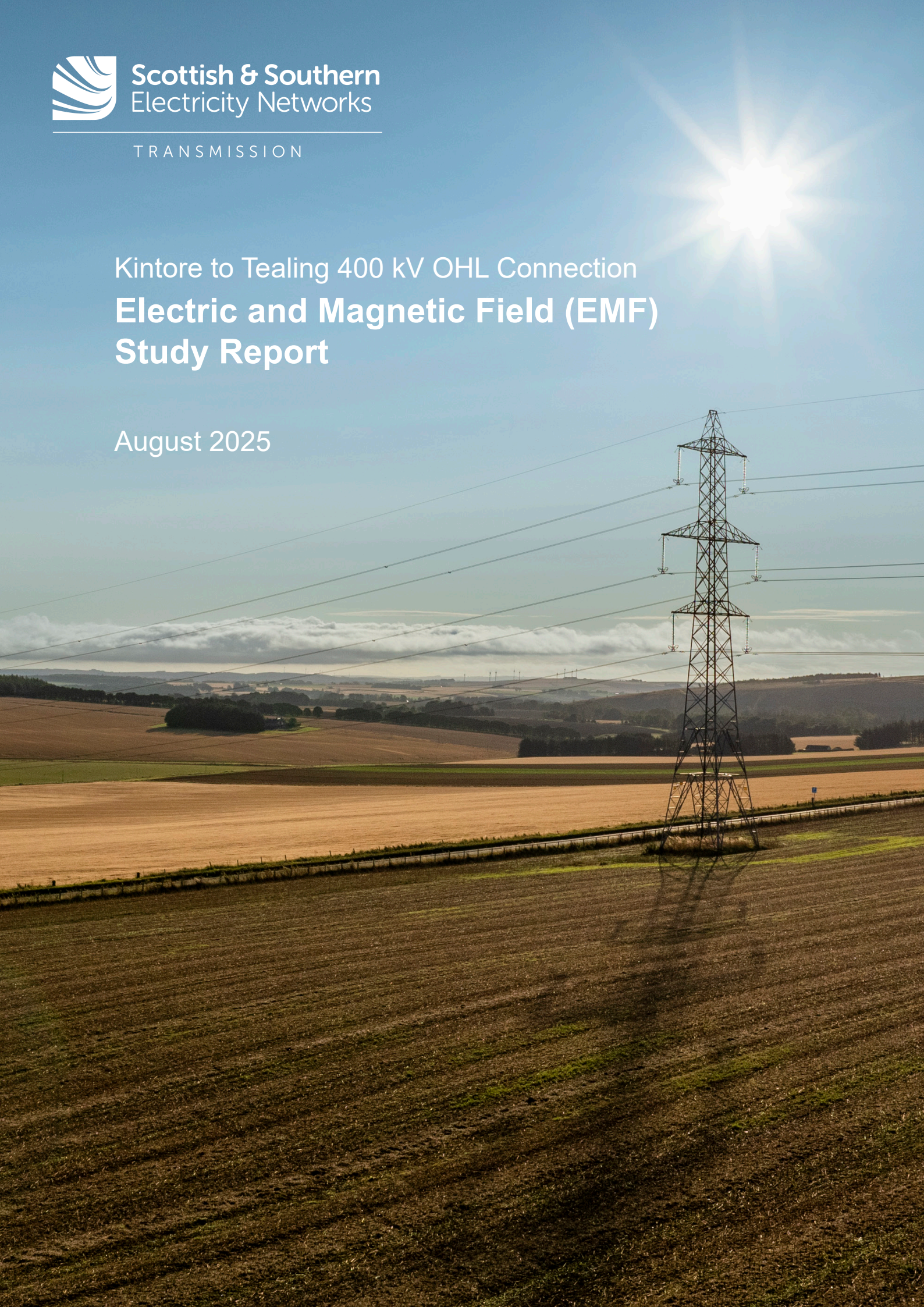


Scottish & Southern
Electricity Networks

TRANSMISSION

Kintore to Tealing 400 kV OHL Connection **Electric and Magnetic Field (EMF) Study Report**

August 2025



Electric & Magnetic Field Study Report

for

Kintore Tealing 400kV Overhead Lines



EMF-OHL-001	Electric & Magnetic Field Study Report Kintore Tealing 400kV		Applies to	
			Distribution	Transmission ✓
Revision: 1.00	Classification: Public	Issue Date: July 25		

Revision	Overview of Amendment & Text Affected	Previous Document	Revision Author	Date
1.0	N/A	-	-	-

	Name	Title
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Summary

This report summarises the assessments of Electric and Magnetic Fields (EMF) associated with the proposed Kintore Tealing 400kV Overhead line project, focusing on the project's compliance with the exposure limits in the UK's Code of Practice 'Power Lines: Demonstrating compliance with EMF public exposure guidelines (DECC: 2012)', validation process and assessment of the more complex arrangements. The project uses an AAAC Araucaria conductor in triple-bundled configuration per phase supported by lattice steel AS4 tower structures. SSEN undertook a comprehensive assessment of the EMF levels using PLS CADD software for two levels of current, 3370A and 5000A, for both transposed (optimal) and untransposed phasing scenarios. PLS CADD is the industry standard for overhead line design. To validate the results, an independent consultant, WSP, was engaged, using an alternative software package for the assessment, SES CDEGS. Both analyses produced consistent results, ensuring the accuracy and reliability of the findings.

The assessed EMF levels comply fully with the exposure limits set out in the UK's Code of Practice. These guidelines are based on internationally recognised limits and form the basis of the framework for EMF safety in the UK. The results confirm that EMF levels remain within the permissible thresholds, demonstrating the projects' compliance with the Code of Practice.

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1 Introduction

This document presents an assessment, results and compliance statement of the proposed Kintore Tealing 400kV overhead line in terms of Electric and Magnetic Fields (EMF). This report is applicable to the new build overhead line and the specific arrangements in section 5 only.

1.1 Objective of EMF Study

The goal of this study is to assess the Electric and Magnetic Field (EMF) levels generated by the new 400kV overhead line and to determine compliance with the UK's Code of Practice 'Power Lines: Demonstrating compliance with EMF public exposure guidelines (DECC: 2012)¹'. This report summarises the studies carried out on EMF levels from the proposed overhead lines to demonstrate a compliant design. The in-house design calculations were done using PLS CADD software with the results being independently validated by Consultants using SES CDGES software.

1.2 Project Background

Scottish and Southern Electricity Networks/ SSEN Transmission plc ("SSEN") is proposing to construct and operate approximately 105.2 kilometres (km) of new double circuit 400 kilovolts (kV) overhead transmission line (OHL) between Kintore and Tealing.

In July 2022, National Grid ESO (as of 1 October 2024 now known as the National Energy System Operator (NESO)) published the Pathway to 2030 Holistic Network Design (Pathway to 2023 HND), setting out the electricity transmission network infrastructure required to enable the forecasted growth in renewable electricity across Great Britain, in light of the UK and Scottish Government's 2030 offshore wind allocations of 50 gigawatt (GW) and 11 GW (through the Crown Estate and ScotWind leasing rounds) which are the main driver for these upgrades.

The proposed 400 kV overhead line (OHL) will consist of steel lattice towers using a new tower series known as the ASTI SSE400 or AS4 for short. These towers are expected to average 57 m in height across the routes. The conductor system is proposed to be 3 x 700 mm² AAAC Araucaria with 500 mm bundle spacing. The circuit is designed to function up to 90°C while maintaining a minimum ground clearance of 9 m under normal conditions. Although it is capable of operating at to 90°C, it is not currently intended to be used at this maximum rating.

¹ Power Lines: Demonstrating compliance with EMF public exposure guidelines (DECC: 2012)

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2 Electric and Magnetic Field

2.1 Introduction to Electric and Magnetic Field Study

Overhead Lines (OHLs) are used to carry high voltage electricity across long distances and are a source of electric and magnetic fields. There are long established concerns around the potential health effects of exposure of these fields. As a result, OHL have been subject to a large body of scientific research and regulatory initiatives. A summary of the known potential impacts is provided in this section.

2.2 Electric Fields

Electric fields are found wherever there is electricity. Electric fields are created by the presence of electric charges and are measured in volts per meter (V/m). An electric field is associated with any device or wire that is connected to a source of electricity, even when a current is not flowing. Electric fields are easily shielded by common objects such as trees, fences, and walls. It has been determined there is no body of evidence indicating a relationship between exposure to electric fields and human disease. However, strong electric fields can lead to micro-shocks from poorly earthed objects and sensory impacts (reversible on removal from the field and temporary in duration). As such it essential the electric field strength is controlled.

2.3 Magnetic Fields

Magnetic fields are created by charges (electrons) moving in a conductor, such as a wire. The number of electrons moving through a conductor at any given time is called the current (measured in amperes). As the powerflow increases, so does the magnetic field. The magnetic field decreases as the distance from the source increases. Scientific studies have identified that there is a statistical association between magnetic fields and childhood leukaemia however the evidence of the association has weakened in recent years. No biological mechanism has been found for this relationship and since this potential relationship was identified in the 1960's, subsequent studies have shown a steady decline in the potentially elevated risk. This is despite powerflows, and thus the magnetic field strength from OHLs, increasing over the same period. There is insufficient evidence of magnetic fields being linked to other diseases or cancers. As the statistical association with childhood leukaemia remains it is acknowledged as a potential impact and thus it is considered necessary to control the magnetic field strength to reduce the potential risk.

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2.4 EMF Exposure limits

To ensure the safety of the public due to EMF emissions from OHLs, the UK Government issued, following consultation, a Code of Practice for the industry ‘Power Lines: Demonstrating compliance with EMF public exposure guidelines’ issued via the Department of Energy & Climate Change in 2011 and updated in 2012. This was based on levels set by 1998 guidelines published by the International Commission on Non-Ionizing Radiation Protection (ICNIRP). These levels are set to minimise any health risk posed by the OHL. Additionally, whilst being low risk, the statistical association with childhood leukaemia was recognised and UK further introduced a precautionary measure requiring optimal phasing, where reasonably possible, in the Code of Practice.

The Code of Practice sets the maximum levels for long term public exposure as 360 μ T for magnetic fields and 9 kV/m for electric fields. Long term exposure relates to places of residence or similar where people regularly spend extended periods of time. The SSEN OHL design standard TG-NET-OHL-506 Rev 2.0 defines the exposure limits in accordance with the Code of Practice.

The following characteristics are defined by TG-NET-OHL-506 Rev 2.0 for calculation the EMF fields from overhead lines

- Fields shall be measured directly below the line
- Fields shall be calculated with maximum continuous current and voltage
- The conductors shall be modelled at the design minimum clearance
- Double circuit vertical transmission lines shall have optimum phase arrangement to reduce imbalance EMF and induced ground currents.

The UK Government have reconfirmed the principles and limits set out in the Code of Practice with their latest policy on EMF. National Policy Statement EN-5², (NPS EN-5) which was reissued in November 2023 and came into force on 17 January 2024. This policy confirmed the current UK Government guidance, informed by relevant international guidance, is therefore still considered appropriate.

² National Policy Statement EN-5

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3 EMF Calculations

This section summarises the SSEN Transmission calculations of EMF for the proposed OHLs.

3.1 Line Modelling Parameters

The Kintore Tealing overhead line is being designed with a triple bundled AAAC Araucaria conductor per phase on AS4 Towers (a modified version of the SSE400). The phase configurations are considered as optimal phasing i.e. a fully transposed phase arrangement.

The following conductor system design is proposed for this project as shown in the table 3.1 below.

Table 3.1 – Conductor System

Conductor	Construction	Diameter (mm)	Resistivity (nΩm)	No. of Sub conductors	Bundle Distance (mm)	Max. Operating Temperature (°C)
Araucaria	AAAC 700mm ²	37.26	30.5	3	500	90

Two power flow scenarios were considered:

1. Intended maximum power flow; 3370 Amps (winter pre-fault continuous based on a summer pre-fault continuous power flow of 2090MVA),
 - Maximum possible power flow; 5000A (maximum winter pre-fault continuous considering substation limitations)

It should be noted that although analysis has been carried out up to a maximum current of 5000A the line is only intended to operate up to 3370A but the full capability has been considered to be conservative.

The proposed structure design for the Kintore Tealing scheme is the AS4 series of lattice steel towers, specifically designed for the project. Proposed tower outline drawing for the standard suspension tower (AS4-AD) is attached in Appendix-A.

3.2 Design Calculations

The EMF calculations were performed in-house by SSEN Transmission's Onshore Capital Delivery Project Engineering team using PLS-CADD Software, an internationally recognised tool by the transmission industry. The line was modelled on the basis of the parameters defined in section 3.1 of this report. The calculations were performed for both transposed and untransposed (for reference only) phase arrangement and calculated at middle of the span where the conductor is nearest to the ground level; the worst-case scenario. These calculations were made for a range of different ground clearance options in order to determine the minimum ground clearance needed to ensure compliance with the Code of Practice. The smallest, minimum ground clearance which was found to be compliant is shown in green for each of the following scenarios:

- Transposed: Maximum possible power flow,

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- Transposed: Required maximum power flow,
- Untransposed: Maximum possible power flow,
- Untransposed: Required maximum power flow,

The below tables summarise the EMF level for the range of heights checked. The EMF reports, generated by the PLS-CADD software, used to populate these tables are enclosed in Appendix-B.

Table 3.2 - Transposed Phase Arrangement

Current: 5000 A			Current: 3370 A			
TRANPOSED (RYB-BYR)						
Clearance (m)	Electric Field (kV/m)	Magnetic Field (uT)		Clearance (m)	Electric Field (kV/m)	Magnetic Field (uT)
7.3	11.20	111.20		7.3	11.20	74.90
7.6	10.6	108.30		7.6	10.60	72.96
8.0	9.86	104.36		8.0	9.86	70.34
8.5	9.05	96.47		8.5	9.05	65.02
8.7	8.63	93.12		8.7	8.63	62.76
9.0	8.30	89.36		9.0	8.30	60.22
9.5	7.54	83.24		9.5	7.54	44.65

TRANSDPOSED

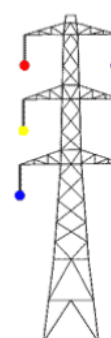
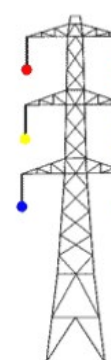


Table 3.3 - Un-Transposed Phase Arrangement

Current: 5000 A			Current: 3370 A			
UNTRANSDPOSED (RYB-RYB)						
Clearance (m)	Electric Field (kV/m)	Magnetic Field (uT)		Clearance (m)	Electric Field (kV/m)	Magnetic Field (uT)
7.3	11.79	92.50		7.3	11.79	67.80
7.6	11.19	91.66		7.6	11.19	64.90
8.0	10.49	90.55		8.0	10.50	61.03
8.5	9.70	83.91		8.5	9.70	56.56
8.7	9.36	81.11		8.7	9.36	54.67
9.0	8.98	77.90		9.0	8.98	52.51
9.5	8.37	72.85		9.5	8.37	49.10

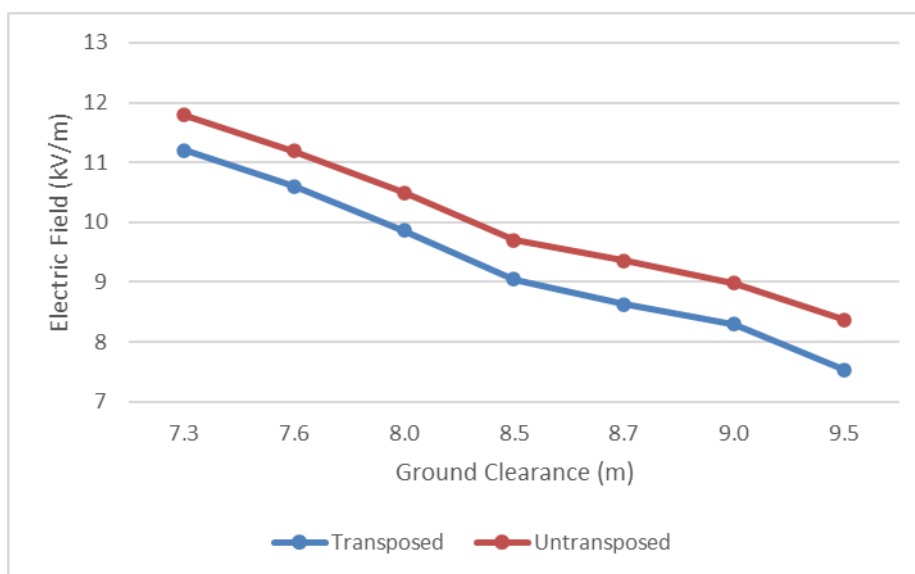
UNTRANSDPOSED



The calculated values for Electric field at the minimum statutory ground clearance (7.3m) are 11.20 kV/m and 11.79 kV/m for the transposed and untransposed scenarios respectively. These values are not within the acceptable limits (i.e. 9kV/m). The acceptable electric field exposure levels are not achieved until a ground clearance of 8.7m and 9.0m is achieved for the transposed and untransposed scenarios respectively. The following figure shows a graphical representation of the electric field in transposed and untransposed phasing scenarios.

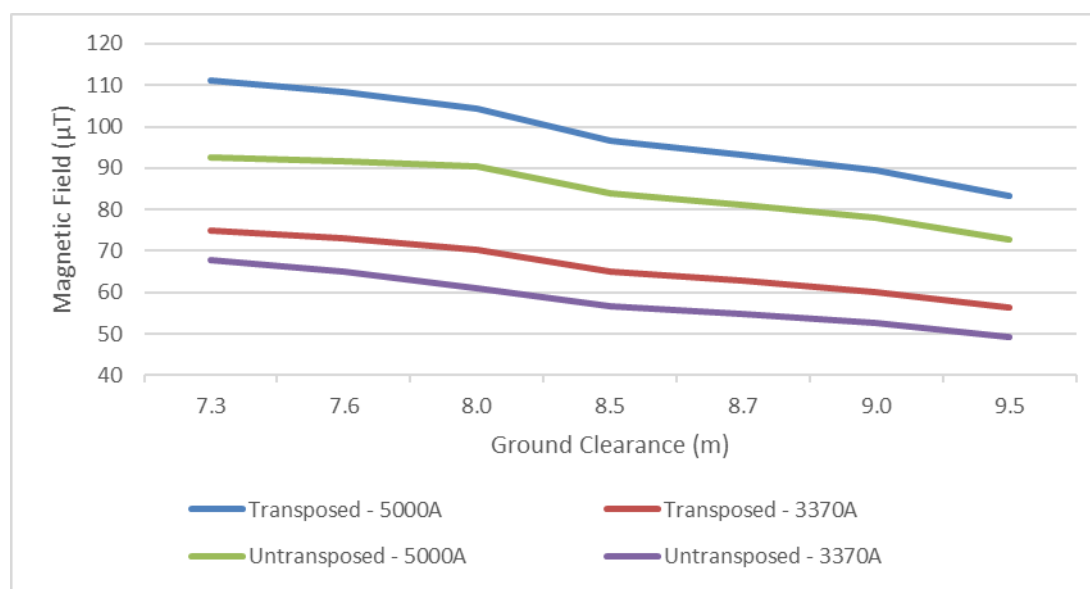
Figure 3.1 - Electric Field Arrangement

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The calculated values for the magnetic field varies with the increase in the current/load. However, the statutory limit for the magnetic field is 360 uT which is achieved at the 7.3m ground clearance for all scenarios. The following figure shows the graphical representation of the Magnetic Field at transposed and untransposed phasing scenarios and with two different power flows:

Figure 3.2 - Magnetic Field Arrangements



It was concluded from the above tables that the minimum compliant clearance to ground, 8.7m-9.0m, was relatively consistent for the four scenarios considered, including the conservative untransposed values. The overall tower height would not change whether an 8.7m or 9.0m clearance to ground was adopted. As such,

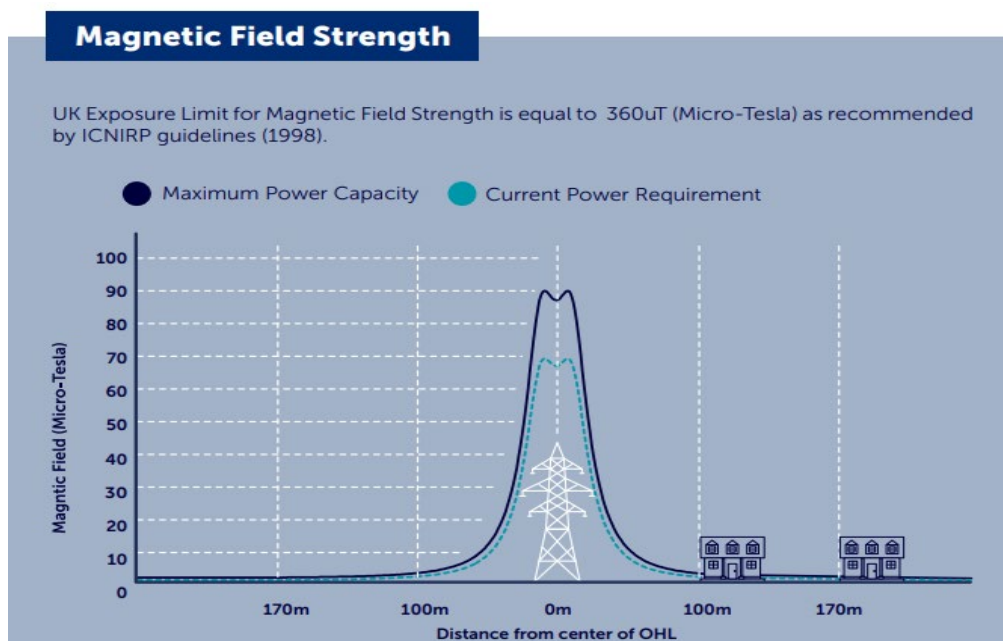
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there would be no change to the landscape & visual, or other environmental impacts and therefore the more conservative value of 9.0m clearance was adopted.

3.3 Summary of Assessment and Further Precautions

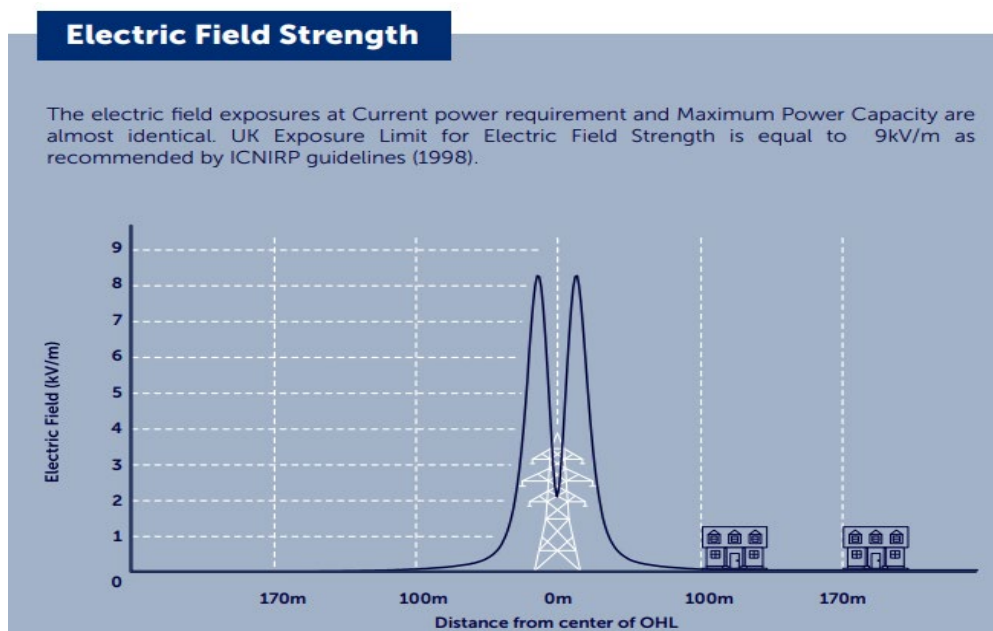
The Assessment of Electric and Magnetic Field levels for the proposed overhead line project confirms that with a minimum ground clearance of 9.0m, all calculated values are within the statutory exposure limits. It should be noted that these values are for a 1m height above ground, directly beneath the line and assume long term exposure that would be typical for a residence or similar. The routing of the Kintore Tealing project has avoided the oversail of residential (or similar) properties and looked to site the OHL away from the properties. Whilst this is not necessary under the Code of Practice, nor was the EMF levels the sole factor in these routing decisions, in practice this substantially reduces the EMF exposure levels compared to the values given in this report. This is visualised in the figures 3.3 and 3.4, shared at the projects’ public consultations in the Pathway to 2030 EMF leaflet.

Figure 3.3 - Magnetic Field Strength as per Pathway to 2030 EMF leaflet



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Figure 3.4 - Electric Field Strength as per Pathway to 2030 EMF leaflet



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4 Validation of EMF Result

SSEN Transmission commissioned the consultancy group WSP to provide an independent validation of the EMF levels generated by the proposed OHL. WSP utilised another industry standard tool, SES CDEGS software, for this work. The EMF reports generated by WSP by using CDEGS software are enclosed in Appendix-C. The results from WSP's analysis were consistent with those calculated in Section 3, see table 4.1, and confirmed that the EMF levels are well within the acceptable exposure limits set by the Code of Practice.

Table 4.1 - Comparison of WSP and SSEN-T EMF analysis

Power flow/ Current (3x Araucaria on AS4)	Clearance	Magnetic Field (under the line at mid span)		Electric Field (under the line at mid span)	
		SSEN-T (PLS-CADD)	WSP (CDEGS)	SSEN-T (PLS-CADD)	WSP (CDEGS)
5000 A	9.00 M	89.3 μ T	92 μ T	8.3 kV/m	7.9 kV/m
3370 A	9.00 M	60.2 μ T	62 μ T	8.3 kV/m	7.9 kV/m

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5 Complex OHL Arrangements

5.1 Cumulative Assessment

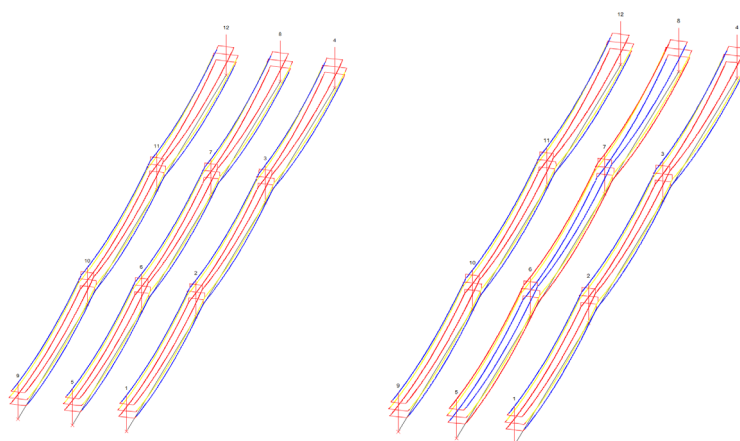
Where overhead lines come into close proximity to each other, their electric and magnetic fields can interact with one another and therefore a cumulative assessment is required to demonstrate compliance. Due to the fact that Electric and Magnetic fields are vector quantities and have both magnitude and direction, the way in which they combine is complex and the values cannot simply be added together. Although combining the EMFs from different sources is complex, generally when the field from one source is larger than the other, the larger field dominates, with the smaller field making a minor impact to the overall field. This is why at substations the largest fields typically come from the overhead lines entering the substation and the impact of the plant within the substation itself is considered to have minimal impact to the overall fields.

To demonstrate compliance a conservative assessment has been carried out within PLS-CADD considering three 400kV overhead lines, in parallel, all operating at 5000A using the parameters from section 3. The three lines have been spaced at 72m centre to centre which has been selected based off an 18m substation bay spacing and is considered to be the closest the lines will operate at this voltage on approach to a substation.

The exact field that is produced by the lines in parallel depends on specifics of relative phasing and loads however this assessment considers a number of scenarios that are considered to be representative of the cumulative effect.

Two phasing scenarios have been modelled. The first scenario (Case 1) considers all lines being optimally phased and the circuits between adjacent lines also being optimally phased. This is an ideal scenario as when circuits have optimal phasing the electric and magnetic fields can partially cancel each other out reducing the resultant fields. However, while the proposed development is to be optimally phased, as phasing of future developments is not yet confirmed a precautionary assessment was undertaken, therefore a second case (Case 2) was considered where the three individual lines were still optimally phased but the circuits between the adjacent lines were not optimally phased. This second arrangement has the potential to increase the magnitude of the resultant fields. Figure 5.1 below depicts the two cases described above.

Figure 5.1 – Case 1 on left, Case 2 on right



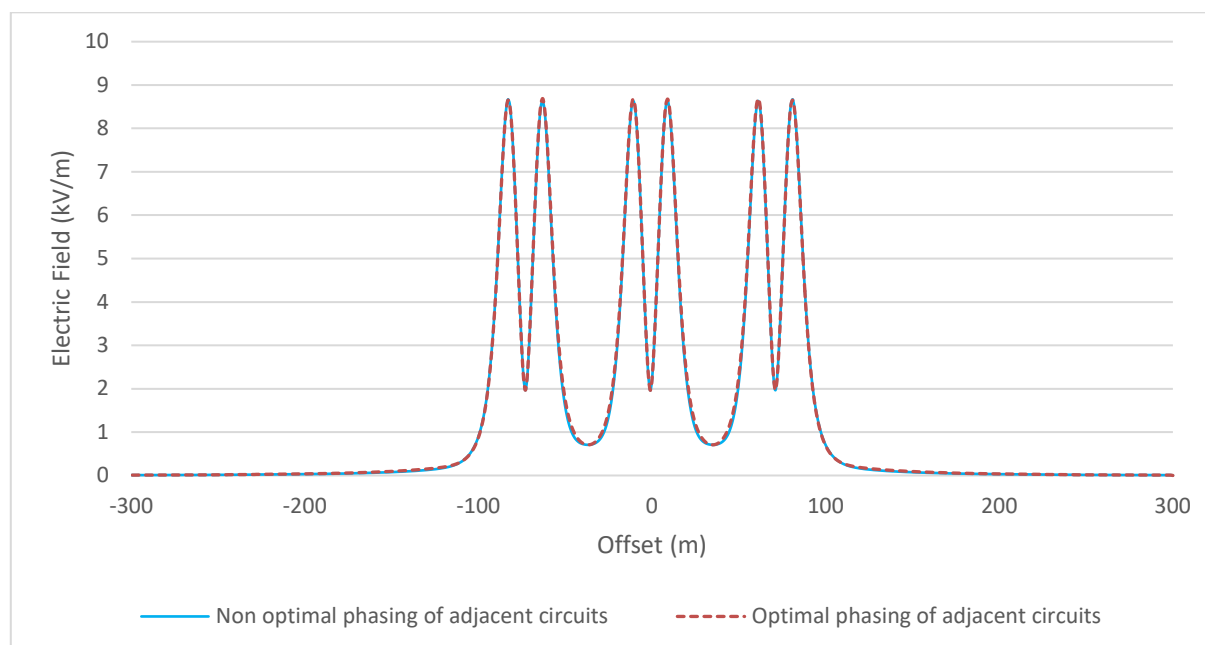
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The maximum fields for each scenario are presented in table 5.1 below. The full PLS-CADD report can be seen in Appendix-D. Figures 5.2 and 5.3 show the two cases for both the cumulative electric field and magnetic field extracted from the PLS Report.

Table 5.1 - Summary of Electric and Magnetic Field Values for Cumulative Assessment

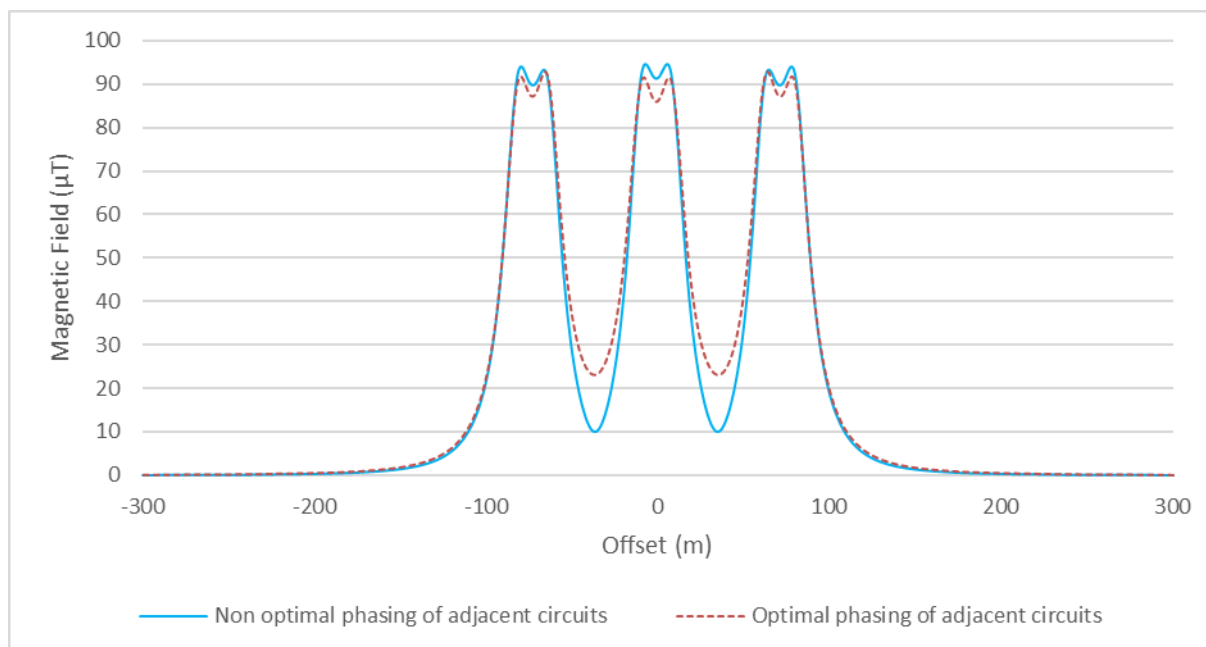
Cumulative Assessment Case	Maximum Magnetic Field (μT)	Maximum Electric Field (kV/m)
Case 1 – Optimal phasing of adjacent circuits	92.71	8.69
Case 2 – Non-Optimal phasing of adjacent circuits	94.71	8.67

Figure 5.2 - Cumulative Electric Field Results



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Figure 5.3 - Cumulative Magnetic Field Results



As stated above, this analysis depends on numerous factors such as phasing and load however the cases carried out demonstrate the mechanisms in which fields combine and are considered representative for the proposed development. This assessment demonstrates that the combined impact of electric and magnetic fields from parallel overhead lines does not affect the assessment of compliance for the proposed new overhead line with the maximum fields remaining within the acceptable exposure limits set by the Code of Practice.

5.2 Complex Crossings

Across the Kintore Tealing 400kV OHL there is a certain complex OHL arrangement that required further detailed analysis. This arrangement is a result of the proposed OHL crossing an existing OHL. Where this crossing occurs, the electric and magnetic fields of the respective OHL's can interact with one another and therefore the combined effects must be considered.

This analysis cannot be carried out in the same method as discussed in the previous section and requires specialist software, SES CDEGS, due to the complexity of these crossings involving multiple circuits directly crossing each other. This type of analysis is best suited to the specialist software to accurately model the resultant electric and magnetic fields. A specialist consultant, Arcadis Consulting (UK) Limited, was commissioned to carry out this detailed analysis and the full study is appended to this report.

An overview of the results for the proposed crossing is provided within 2 below.

Table 5.2 - Summary of Electric and Magnetic Field Values for Complex Arrangements

Description of Crossing	Maximum Magnetic Field (μT)	Maximum Electric Field (kV/m)
Craigiebuckler to Tarland 132kV OHL Crossing	98.81	8.44

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Based on the results in the table above it can be observed that both the maximum magnetic and electric fields observed at the crossing remain below the acceptable exposure limits set by the Code of Practice. The full details of this analysis can be seen in Appendix-E.

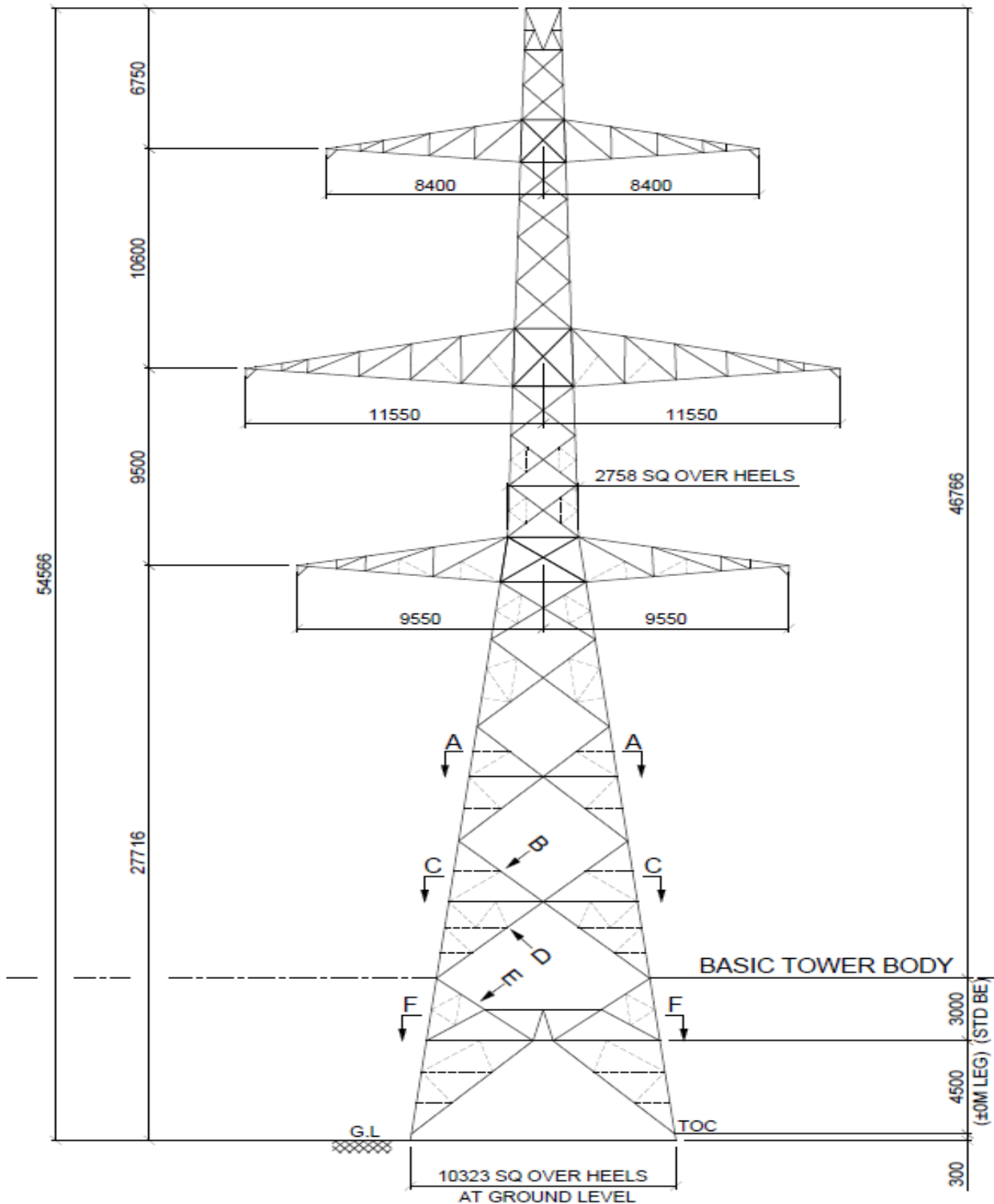
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6 Conclusion

In conclusion, as demonstrated by this report and its supporting documents, the proposed OHLs are compliant with the industry's current Code of Practice 'Power Lines: Demonstrating compliance with EMF public exposure guidelines' developed by the Department of Energy & Climate Change.

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Appendix A Tower Geometry



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Appendix B PLS CADD Electric and Magnetic Field Calculations

TRIPLE Araucaria (7.6m ground clearance)

PLS-CADD Version 18.00x64| 11:51:13 AM 06 July 2023
 Scottish and Southern Energy
 Project Name: 'C:\Users\AM25305\Desktop\CSR ASTI-\PLS Model ASTI\profile 637.don'

Criteria Notes:

Design criteria developed for SSE Beaulieu Blackhilllock Line reconductoring
 Global wind notes: wind directions are annotated NNW-330, E-90, etc as 'wind from' - angles in GLB wind are 'wind to' or wind azimuth
 delete - survey and maps confirm angle as per XYZ 19/08/08.Terrain 289: angle has been corrected in pfl. CHECK xyz
delete220/08/08.PFL 180 and 181 points edited
 tower 229 is a D10 with extended crossarms. It should be modeled???Erection loads???CHECK.

3D EMF Calculation Notes:

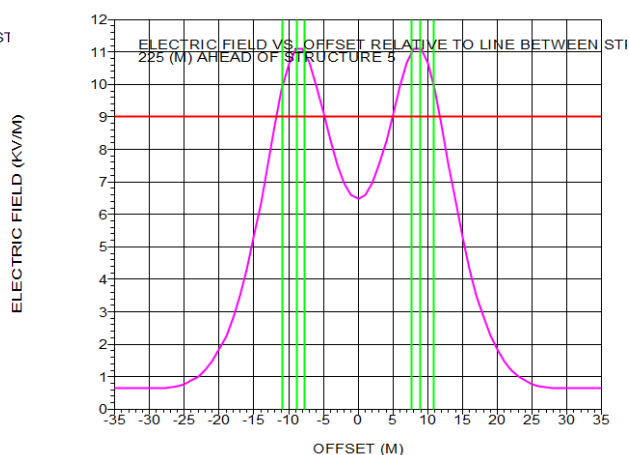
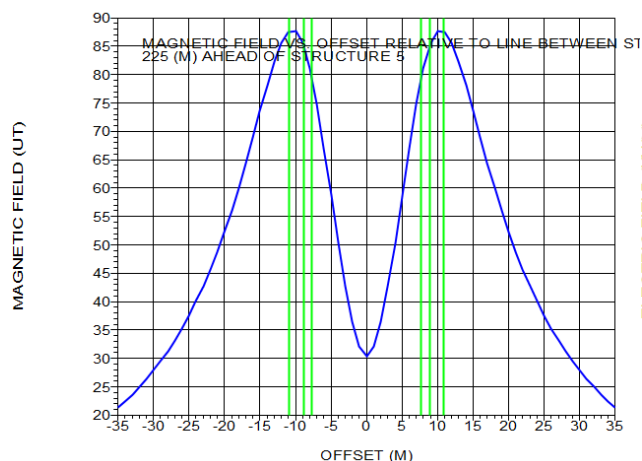
- 1) Calculations based on the EPRI Red Book methods (3rd Edition, 2005 - 7.4 Calculation of Magnetic Fields and Appendices 7.1 Calculation of Field Ellipse Parameters and 7.6 Electric Field Calculations for 3D Geometry).
- 2) All wire positions are modeled at the specified weather case and wind direction. Height above ground determined by the modeled ground TIN.
- 3) Only the effects of wires are being analyzed. The effects of structures are not included unless enabled as noted below.
- 4) Ground return is being ignored for magnetic field calculations.

Meter height above ground: 1.00 (m)
 Maximum wire distance: 150.00 (m)
 Maximum cable segment size: 3.00 (m)
 Cross section offset +/-: 35.00 (m)
 Result interval: 1.00 (m)
 Electric field limit: 9.00 (kV/m)
 Magnetic field limit: 360.00 (uT)
 Space potential limit: 0.00 (kV)
 Contour Map Spacing: 3 (m)
Analyzing spans between these structures: 1 - 6

One or more sections have wind from both directions which is not supported. A wind direction of left is being used for those sections.

Section Data for 3D EMF Results:

Section Number	Section Note	Voltage Ph-Ph (kV)	Current (Amps)	Filename	Description	Conductors Per Phase	Bundle Diameter (cm)	Cable Radius (cm)	Weather Case	Condition	Wind Dir.	Temperature (deg C)	WC	Effective Radius (cm)
1		400.0	4570.0	araucaria <u>lump1</u>	- 30.5.wir 700mm² AAAC - Araucaria	3	57.735	1.863	90°C	Creep RS	Left	90.000		16.700
2		400.0	4570.0	araucaria <u>lump1</u>	- 30.5.wir 700mm² AAAC - Araucaria	3	57.735	1.863	90°C	Creep RS	Left	90.000		16.700



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				Distribution	Transmission
Revision: 1.00	Classification: Public	Issue Date: July 25			✓

TRIPLE Araucaria (7.6m ground clearance)

3D EMF Point Results Span from 5 to 6:

Measurement			B					H					EF					Space Potential				
X	Y	Z	Real	Imaginary	Angle	Magnitude	Polarization	Magnitude	Real	Imaginary	Angle	Magnitude	Polarization	Real	Imaginary	Angle	Magnitude					
(m)	(m)	(m)	(uT)	(uT)	(deg)	(uT)	Axial Ratio %	(A/m)	(kV/m)	(kV/m)	(deg)	(kV/m)	Axial Ratio %	(kV)	(kV)	(deg)	(kV)					
275807.9	3098063.4	1.9	17.279	12.506	35.9	21.330	20.2	16.974	0.273	0.582	64.8	0.643	6.0	0.269	0.581	65.1	0.640					
275808.2	3098064.4	1.9	18.101	13.284	36.3	22.452	20.4	17.867	0.238	0.599	68.3	0.645	6.9	0.232	0.599	68.8	0.642					
275808.5	3098065.3	1.9	18.975	14.132	36.7	23.659	20.7	18.827	0.197	0.616	72.3	0.646	7.9	0.188	0.615	73.0	0.643					
275808.8	3098066.3	1.9	19.906	15.057	37.1	24.960	21.0	19.862	0.151	0.629	76.5	0.647	9.1	0.136	0.628	77.8	0.643					
275809.1	3098067.2	1.9	20.898	16.069	37.6	26.362	21.2	20.978	0.103	0.640	80.8	0.648	10.5	0.075	0.638	83.3	0.642					
275809.4	3098068.2	1.9	21.955	17.178	38.0	27.877	21.4	22.184	0.079	0.645	83.0	0.650	12.2	0.003	0.642	89.7	0.642					
275809.7	3098069.1	1.9	23.083	18.393	38.5	29.515	21.5	23.487	0.119	0.643	79.5	0.654	14.2	-0.081	0.640	-82.8	0.645					
275810.1	3098070.1	1.9	24.286	19.729	39.1	31.290	21.7	24.899	0.203	0.633	72.2	0.665	16.4	-0.178	0.628	-74.2	0.653					
275810.4	3098071.0	1.9	25.571	21.197	39.7	33.214	21.7	26.431	0.311	0.610	63.0	0.685	18.6	-0.291	0.604	-64.3	0.671					
275810.7	3098072.0	1.9	26.943	22.814	40.3	35.304	21.7	28.094	0.440	0.573	52.5	0.722	20.5	-0.422	0.564	-53.2	0.704					
275811.0	3098072.9	1.9	28.409	24.595	40.9	37.576	21.6	29.902	0.590	0.517	41.2	0.784	21.6	-0.574	0.502	-41.2	0.762					
275811.3	3098073.9	1.9	29.978	26.557	41.5	40.049	21.4	31.870	0.763	0.438	29.8	0.880	21.5	-0.748	0.413	-28.9	0.854					
275811.6	3098074.8	1.9	31.655	28.718	42.2	42.741	21.2	34.012	0.964	0.338	19.3	1.021	20.4	-0.948	0.290	-17.0	0.991					
275811.9	3098075.8	1.9	33.450	31.098	42.9	45.673	20.8	36.345	1.193	0.242	11.4	1.218	18.5	-1.177	0.122	-5.9	1.183					
275812.3	3098076.7	1.9	35.371	33.712	43.6	48.863	20.2	39.884	1.456	0.272	10.6	1.482	16.3	-1.439	-0.102	4.0	1.443					
275812.6	3098077.7	1.9	37.425	36.574	44.3	52.329	19.6	41.642	1.757	0.500	15.9	1.827	14.2	-1.739	-0.394	12.8	1.783					
275812.9	3098078.6	1.9	39.617	39.693	45.1	56.081	18.7	44.628	2.099	0.857	22.2	2.267	12.3	-2.079	-0.770	20.3	2.217					
275813.2	3098079.6	1.9	41.947	43.066	45.8	60.119	17.7	47.841	2.486	1.328	28.1	2.819	10.6	-2.464	-1.246	26.8	2.761					
275813.5	3098080.5	1.9	44.408	46.673	46.4	64.424	16.6	51.267	2.923	1.923	33.3	3.498	9.1	-2.897	-1.837	32.4	3.430					
275813.8	3098081.5	1.9	46.972	50.461	47.1	68.940	15.3	54.861	3.409	2.650	37.9	4.318	7.9	-3.378	-2.557	37.1	4.237					
275814.1	3098082.4	1.9	49.585	54.336	47.6	73.560	13.8	58.537	3.944	3.514	41.7	5.282	6.6	-3.906	-3.407	41.1	5.183					
275814.5	3098083.4	1.9	52.147	58.133	48.1	78.095	12.2	62.146	4.516	4.502	44.9	6.377	5.5	-4.469	-4.377	44.4	6.256					
275814.8	3098084.3	1.9	54.892	61.603	48.5	82.246	10.5	65.449	5.106	5.576	47.5	7.560	4.6	-5.047	-5.429	47.1	7.412					
275815.1	3098085.3	1.9	56.380	64.393	48.8	85.587	8.7	68.108	5.675	6.664	49.6	8.753	3.7	-5.602	-6.490	49.2	8.573					
275815.4	3098086.2	1.9	57.501	66.075	49.0	87.591	6.9	69.703	6.173	7.655	51.1	9.834	3.0	-6.084	-7.455	50.8	9.623					
275815.7	3098087.2	1.9	57.534	66.217	49.0	87.720	4.9	69.806	6.537	8.417	52.2	10.657	2.4	-6.436	-8.199	51.9	10.424					
275816.0	3098088.1	1.9	56.246	64.522	48.9	85.596	3.0	68.115	6.713	8.834	52.8	11.095	2.0	-6.609	-8.612	52.5	10.855					
275816.3	3098089.1	1.9	53.598	60.960	48.7	81.172	1.0	64.594	6.679	8.848	53.0	11.086	1.8	-6.582	-8.641	52.7	10.862					
275816.7	3098090.0	1.9	49.784	55.810	48.3	74.788	1.0	59.514	6.456	8.492	52.8	10.668	1.8	-6.375	-8.317	52.5	10.479					
275817.0	3098090.9	1.9	45.180	49.566	47.7	67.067	3.0	53.370	6.098	7.871	52.2	9.957	2.0	-6.039	-7.738	52.0	9.816					
275817.3	3098091.9	1.9	40.224	42.787	46.8	58.726	4.9	46.732	5.677	7.122	51.4	9.107	2.1	-5.641	-7.034	51.3	9.017					
275817.6	3098092.8	1.9	35.337	35.982	45.5	50.432	6.7	40.133	5.258	6.370	50.5	8.260	2.2	-5.244	-6.326	50.3	8.217					
275817.9	3098093.8	1.9	30.904	29.595	43.8	42.789	7.9	34.051	4.891	5.711	49.4	7.519	2.1	-4.895	-5.705	49.4	7.517					
275818.2	3098094.7	1.9	27.294	24.103	41.4	36.413	7.9	28.976	4.610	5.206	48.5	6.954	1.8	-4.628	-5.230	48.5	6.983					
275818.5	3098095.7	1.9	24.892	20.176	39.0	32.042	5.2	25.498	4.435	4.892	47.8	6.603	1.4	-4.461	-4.934	47.9	6.652					
275818.9	3098096.6	1.9	24.043	18.702	37.9	30.460	0.0	24.240	4.376	4.785	47.6	6.484	1.1	-4.405	-4.834	47.7	6.540					
275819.2	3098097.6	1.9	24.892	20.176	39.0	32.042	5.2	25.498	4.435	4.892	47.8	6.603	1.4	-4.461	-4.934	47.9	6.652					
275819.5	3098098.5	1.9	27.294	24.103	41.4	36.413	7.9	28.976	4.610	5.206	48.5	6.954	1.8	-4.628	-5.230	48.5	6.983					
275819.8	3098099.5	1.9	30.904	29.595	43.8	42.789	7.9	34.051	4.891	5.711	49.4	7.519	2.1	-4.895	-5.705	49.4	7.517					
275820.1	3098100.4	1.9	35.337	35.982	45.5	50.432	6.7	40.133	5.258	6.370	50.5	8.260	2.2	-5.244	-6.326	50.3	8.217					
275820.4	3098101.4	1.9	40.224	42.787	46.8	58.726	4.9	46.732	5.677	7.122	51.4	9.107	2.1	-5.641	-7.034	51.3	9.017					
275820.8	3098102.3	1.9	45.180	49.566	47.7	67.067	3.0	53.370	6.098	7.871	52.2	9.957	2.0	-6.039	-7.738	52.0	9.816					
275821.1	3098103.3	1.9	49.784	55.810	48.3	74.788	1.0	59.514	6.456	8.492	52.8	10.668	1.8	-6.375	-8.317	52.5	10.479					
275821.4	3098104.2	1.9	53.598	60.960	48.7	81.172	1.0	64.594	6.679	8.848	53.0	11.086	1.8	-6.582	-8.641	52.7	10.862					
275821.7	3098105.2	1.9	56.246	64.522	48.9	85.596	3.0	68.115	6.713	8.834	52.8	11.095	2.0	-6.609	-8.612	52.5	10.855					
275822.0	3098106.1	1.9	57.534	66.217	49.0	87.720	4.9	69.806	6.537	8.417	52.2	10.657	2.4	-6.436	-8.199	51.9	10.424					
275822.3	3098107.1	1.9	57.501	66.075	49.0	87.591	6.9	69.703	6.173	7.655	51.1	9.834	3.0	-6.084	-7.455	50.8	9.623					
275822.6	3098108.0	1.9	56.380	64.393	48.8	85.587	8.7	68.108	5.675	6.664	49.6	8.753	3.7	-5.602	-6.490	49.2	8.573					
275823.0	3098109.0	1.9	54.892	61.603	48.5	82.246	10.5	65.449	5.106	5.576	47.5	7.560	4.6	-5.047	-5.429	47.1	7.412					
275823.3	3098109.9	1.9	52.147	58.133	48.1	78.095	12.2	62.146	4.516	4.502	44.9	6.377	5.5	-4.469	-4.377	44.4	6.256					
275823.6	3098110.9	1.9	49.585	54.336	47.6	73.560	13.8	58.537	3.944	3.514	41.7	5.282	6.6	-3.906	-3.407	41.1	5.183					
275823.9	3098111.8	1.9	46.972	50.461	47.1	68.940	15.3	54.861	3.409	2.650	37.9	4.318	7.9	-3.378	-2.557	37.1	4.237					
275824.2	3098112.8	1.9	44.408	46.673	46.4	64.424	16.6	51.267	2.923	1.923	33.3	3.498	9.1	-2.897	-1.837	32.4	3.430					
275824.5	3098113.7	1.9	41.947	43.066	45.8	60.119	17.7	47.841	2.486	1.328	28.1	2.819	10.6	-2.464	-1.246	26.8	2.761					
275824.8	3098114.7	1.9	39.617	39.693	45.1	56.081	18.7	44.628	2.099	0.857	22.2	2.267	12.3	-2.079	-0.770	20.3	2.217					
275825.2	3098115.6	1.9	37.425	36.574	44.3	52.329	19.6	41.642	1.757	0.500	15.9	1.827	14.2	-1.739	-0.394	12.8	1.783					
275825.5	3098116.6	1.9	35.371	33.712	43.6	48.863	20.2	39.884	1.456	0.272	10.6	1.482	16.3	-1.439	-0.102	4.0	1.443					
275825.8	3098117.5	1.9	33.450	31.098	42.9	45.673	20.8	36.345	1.193	0.242	11.4	1.218	18.5	-1.177	0.122	-5.9	1.183					
275826.1	3098118.5	1.9	31.655	28.718	42.2	42.741	21.2	34.012	0.964	0.338	19.3	1.021	20.4	-0.948	0.29							

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TRIPLE Araucaria (9.0m ground clearance to achieve 9kV/m Electric Field)

PLS-CADD Version 18.00x64 2:28:01 PM 06 July 2023
 Scottish and Southern Energy
 Project Name: 'C:\Users\AM25305\Desktop\CSR ASTI-\PLS Model ASTI\profile 637.don'

Criteria Notes:

Design criteria developed for SSE Beaulieu Blackhillock Line reconductoring
 Global wind notes: wind directions are annotated NNW-330, E-90, etc as 'wind from' - angles in GLB wind are 'wind to' or wind azimuth
 delete - survey and maps confirm angle as per XYZ 19/08/08.Terrain 289: angle has been corrected in pfl. CHECK xyz
 delete?20/08/08.PFL 180 and 181 points edited
 tower 229 is a D10 with extended crossarms. It should be modeled???Erection loads??CHECK.

3D EMF Calculation Notes:

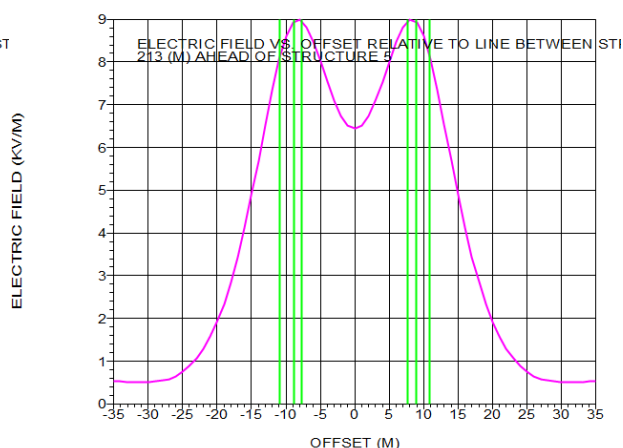
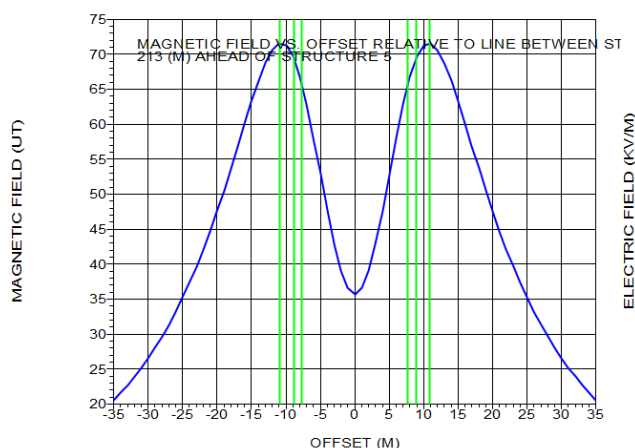
- 1) Calculations based on the EPRI Red Book methods (3rd Edition, 2005 - 7.4 Calculation of Magnetic Fields and Appendices 7.1 Calculation of Field Ellipse Parameters and 7.6 Electric Field Calculations for 3D Geometry).
- 2) All wire positions are modeled at the specified weather case and wind direction. Height above ground determined by the modeled ground TIN.
- 3) Only the effects of wires are being analyzed. The effects of structures are not included unless enabled as noted below.
- 4) Ground return is being ignored for magnetic field calculations.

Meter height above ground: 1.00 (m)
 Maximum wire distance: 150.00 (m)
 Maximum cable segment size: 3.00 (m)
 Cross section offset +/-: 35.00 (m)
 Result interval: 1.00 (m)
 Electric field limit: 9.00 (kV/m)
 Magnetic field limit: 360.00 (uT)
 Space potential limit: 0.00 (kV)
 Contour Map Spacing: 3 (m)
 Analyzing spans between these structures: 1 - 6

One or more sections have wind from both directions which is not supported. A wind direction of left is being used for those sections.

Section Data for 3D EMF Results:

Section Number	Section Note	Voltage (kV)	Current (Amps)	Filename	Description	Conductors Per Phase	Bundle Diameter (cm)	Cable Radius (cm)	Weather Case	Condition	Wind Dir.	Temperature (deg C)	WC Radius (cm)	Effective Radius (cm)
1		400.0	4570.0	araucaria_lump1	30.5.wir 700mm² AAAC - Araucaria	3	57.735	1.863	90°C	Creep RS	Left	90.000	16.700	
2		400.0	4570.0	araucaria_lump1	30.5.wir 700mm² AAAC - Araucaria	3	57.735	1.863	90°C	Creep RS	Left	90.000	16.700	



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TRIPLE Araucaria (9.0m ground clearance to achieve 9kV/m Electric Field)

3D EMF Point Results Span from 5 to 6:

Measurement			B					H		EF					Space Potential				
X (m)	Y (m)	Z (m)	Real (uT)	Imaginary (uT)	Angle (deg)	Magnitude (uT)	Polarization Axial Ratio %	Magnitude (A/m)	Real (kV/m)	Imaginary (kV/m)	Angle (deg)	Magnitude (kV/m)	Polarization Axial Ratio %	Real (kV)	Imaginary (kV)	Angle (deg)	Magnitude (kV)		
275818.8	3098059.8	1.9	16.631	12.096	36.0	20.564	19.3	16.364	0.185	0.497	69.6	0.530	7.4	0.179	0.496	70.2	0.527		
275819.1	3098060.8	1.9	17.391	12.820	36.4	21.605	19.6	17.193	0.147	0.505	73.8	0.526	8.6	0.137	0.504	74.7	0.522		
275819.4	3098061.7	1.9	18.197	13.605	36.8	22.720	19.8	18.080	0.106	0.510	78.3	0.521	10.1	0.089	0.508	80.1	0.516		
275819.7	3098062.7	1.9	19.052	14.457	37.2	23.916	19.9	19.032	0.071	0.511	82.1	0.516	11.9	0.033	0.509	86.3	0.510		
275820.0	3098063.6	1.9	19.958	15.383	37.6	25.198	20.1	20.052	0.076	0.507	81.5	0.513	13.9	-0.032	0.505	-86.4	0.506		
275820.3	3098064.5	1.9	20.919	16.375	38.1	26.575	20.2	21.145	0.131	0.497	75.2	0.514	16.3	-0.107	0.494	-77.8	0.505		
275820.7	3098065.5	1.9	21.939	17.488	38.6	28.056	20.3	22.326	0.211	0.479	66.3	0.523	18.7	-0.193	0.475	-67.9	0.512		
275821.0	3098066.4	1.9	23.020	18.683	39.1	29.648	20.4	23.593	0.307	0.450	55.8	0.545	20.6	-0.292	0.444	-56.7	0.532		
275821.3	3098067.4	1.9	24.168	19.986	39.6	31.361	20.3	24.956	0.418	0.409	44.4	0.585	21.7	-0.405	0.400	-44.6	0.569		
275821.6	3098068.3	1.9	25.385	21.406	40.1	33.206	20.3	26.424	0.547	0.353	32.9	0.651	21.4	-0.534	0.338	-32.3	0.633		
275821.9	3098069.3	1.9	26.676	22.953	40.7	35.191	20.1	28.004	0.694	0.281	22.1	0.748	19.9	-0.682	0.255	-20.5	0.728		
275822.2	3098070.2	1.9	28.043	24.637	41.3	37.328	19.9	29.705	0.861	0.201	13.2	0.884	17.9	-0.848	0.145	-9.7	0.861		
275822.5	3098071.2	1.9	29.491	26.466	41.9	39.626	19.6	31.533	1.050	0.165	8.9	1.063	15.6	-1.038	0.002	-0.1	1.038		
275822.9	3098072.1	1.9	31.021	28.449	42.5	42.091	19.1	33.495	1.264	0.267	11.9	1.292	13.5	-1.251	-0.181	8.2	1.264		
275823.2	3098073.1	1.9	32.635	30.589	43.1	44.729	18.6	35.594	1.504	0.474	17.5	1.577	11.7	-1.491	-0.413	15.5	1.547		
275823.5	3098074.0	1.9	34.331	32.885	43.8	47.540	17.9	37.931	1.774	0.755	23.0	1.928	10.2	-1.759	-0.701	21.7	1.894		
275823.8	3098075.0	1.9	36.103	35.331	44.4	50.515	17.1	40.198	2.074	1.107	28.1	2.351	8.9	-2.058	-1.056	27.2	2.313		
275824.1	3098075.9	1.9	37.941	37.905	45.0	53.631	16.2	42.679	2.406	1.537	32.6	2.855	7.7	-2.388	-1.484	31.9	2.811		
275824.4	3098076.9	1.9	39.821	40.573	45.5	56.850	15.2	45.240	2.769	2.049	36.5	3.445	6.7	-2.749	-1.993	35.9	3.395		
275824.7	3098077.8	1.9	41.708	43.275	46.1	60.102	14.0	47.828	3.162	2.645	39.9	4.122	5.8	-3.138	-2.583	39.5	4.064		
275825.1	3098078.8	1.9	43.544	45.920	46.5	63.283	12.7	50.359	3.577	3.318	42.8	4.879	5.0	-3.550	-3.248	42.5	4.811		
275825.4	3098079.7	1.9	45.244	48.383	46.9	66.241	11.3	52.713	4.005	4.051	45.3	5.697	4.3	-3.972	-3.971	45.0	5.617		
275825.7	3098080.7	1.9	46.994	50.492	47.2	68.774	9.9	54.728	4.428	4.811	47.4	6.538	3.6	-4.388	-4.720	47.1	6.445		
275826.0	3098081.6	1.9	47.750	52.046	47.5	70.632	8.3	56.207	4.821	5.548	49.0	7.350	2.9	-4.774	-5.446	48.8	7.243		
275826.3	3098082.6	1.9	48.253	52.827	47.6	71.548	6.7	56.936	5.154	6.201	50.3	8.064	2.4	-5.102	-6.089	50.0	7.944		
275826.6	3098083.5	1.9	48.062	52.646	47.6	71.285	5.0	56.727	5.399	6.703	51.1	8.608	1.9	-5.343	-6.586	50.9	8.481		
275827.0	3098084.5	1.9	47.091	51.392	47.5	69.704	3.4	55.469	5.532	7.003	51.7	8.925	1.6	-5.476	-6.886	51.5	8.798		
275827.3	3098085.4	1.9	45.345	49.078	47.3	66.819	1.8	53.173	5.545	7.076	51.9	8.990	1.4	-5.493	-6.967	51.7	8.872		
275827.6	3098086.4	1.9	42.933	45.847	46.9	62.811	0.2	49.984	5.448	6.937	51.9	8.821	1.4	-5.404	-6.844	51.7	8.720		
275827.9	3098087.3	1.9	40.052	41.955	46.3	58.004	1.3	46.158	5.268	6.633	51.5	8.471	1.4	-5.235	-6.561	51.4	8.394		
275828.2	3098088.3	1.9	36.949	37.715	45.6	52.798	2.6	42.016	5.039	6.233	51.0	8.016	1.5	-5.019	-6.185	50.9	7.965		
275828.5	3098089.2	1.9	33.889	33.461	44.6	47.624	3.6	37.898	4.800	5.807	50.4	7.534	1.5	-4.792	-5.783	50.4	7.510		
275828.8	3098090.2	1.9	31.134	29.533	43.5	42.913	4.1	34.149	4.582	5.415	49.8	7.093	1.4	-4.584	-5.413	49.7	7.093		
275829.2	3098091.1	1.9	28.930	26.293	42.3	39.093	3.7	31.109	4.409	5.105	49.2	6.745	1.2	-4.420	-5.119	49.2	6.763		
275829.5	3098092.1	1.9	27.498	24.120	41.3	36.578	2.2	29.108	4.300	4.907	48.8	6.524	1.0	-4.315	-4.933	48.8	6.554		
275829.8	3098093.0	1.9	27.001	23.348	40.9	35.696	0.0	28.406	4.262	4.839	48.6	6.448	0.9	-4.280	-4.869	48.7	6.482		
275830.1	3098094.0	1.9	27.498	24.120	41.3	36.578	2.2	29.108	4.300	4.907	48.8	6.524	1.0	-4.315	-4.933	48.8	6.554		
275830.4	3098094.9	1.9	28.930	26.293	42.3	39.093	3.7	31.109	4.409	5.105	49.2	6.745	1.2	-4.420	-5.119	49.2	6.763		
275830.7	3098095.9	1.9	31.134	29.533	43.5	42.913	4.1	34.149	4.582	5.415	49.8	7.093	1.4	-4.584	-5.413	49.7	7.093		
275831.0	3098096.8	1.9	33.889	33.461	44.6	47.624	3.6	37.898	4.800	5.807	50.4	7.534	1.5	-4.792	-5.783	50.4	7.510		
275831.4	3098097.8	1.9	36.949	37.715	45.6	52.798	2.6	42.016	5.039	6.233	51.0	8.016	1.5	-5.019	-6.185	50.9	7.965		
275831.7	3098098.7	1.9	40.052	41.955	46.3	58.004	1.3	46.158	5.268	6.633	51.5	8.471	1.4	-5.235	-6.561	51.4	8.394		
275832.0	3098099.7	1.9	42.933	45.847	46.9	62.811	0.2	49.984	5.448	6.937	51.9	8.821	1.4	-5.404	-6.844	51.7	8.720		
275832.3	3098100.6	1.9	45.345	49.078	47.3	66.819	1.8	53.173	5.545	7.076	51.9	8.990	1.4	-5.493	-6.967	51.7	8.872		
275832.6	3098101.6	1.9	47.091	51.392	47.5	69.704	3.4	55.469	5.532	7.003	51.7	8.925	1.6	-5.476	-6.886	51.5	8.798		
275832.9	3098102.5	1.9	48.062	52.646	47.6	71.285	5.0	56.727	5.399	6.703	51.1	8.608	1.9	-5.343	-6.586	50.9	8.481		
275833.2	3098103.5	1.9	48.253	52.827	47.6	71.548	6.7	56.936	5.154	6.201	50.3	8.064	2.4	-5.102	-6.089	50.0	7.944		
275833.6	3098104.4	1.9	47.750	52.046	47.5	70.632	8.3	56.207	4.821	5.548	49.0	7.350	2.9	-4.774	-5.446	48.8	7.243		
275833.9	3098105.4	1.9	46.994	50.492	47.2	68.774	9.9	54.728	4.428	4.811	47.4	6.538	3.6	-4.388	-4.720	47.1	6.445		
275834.2	3098106.3	1.9	45.244	48.383	46.9	66.241	11.3	52.713	4.005	4.051	45.3	5.697	4.3	-3.972	-3.971	45.0	5.617		
275834.5	3098107.3	1.9	43.544	45.920	46.5	63.283	12.7	50.359	3.577	3.318	42.8	4.879	5.0	-3.550	-3.248	42.5	4.811		
275834.8	3098108.2	1.9	41.708	43.275	46.1	60.102	14.0	47.828	3.162	2.645	39.9	4.122	5.8	-3.138	-2.583	39.5	4.064		
275835.1	3098109.2	1.9	39.821	40.573	45.5	56.850	15.2	45.240	2.769	2.049	36.5	3.445	6.7	-2.749	-1.993	35.9	3.395		
275835.4	3098110.1	1.9	37.941	37.905	45.0	53.631	16.2	42.679	2.406	1.537	32.6	2.855	7.7	-2.388	-1.484	31.9	2.811		
275835.8	3098111.1	1.9	36.103	35.331	44.4	50.515	17.1	40.198	2.074	1.107	28.1	2.351	8.9	-2.058	-1.056	27.2	2.313		
275836.1	3098112.0	1.9	34.331	32.885	43.8	47.540	17.9	37.931	1.774	0.755	23.0	1.928	10.2	-1.759	-0.701	21.7	1.894		
275836.4	3098113.0	1.9	32.635	30.589	43.1	44.729	18.6	35.594	1.504	0.474	17.5	1.577	11.7	-1.491	-0.413	15.5	1.547		
275836.7	3098113.9	1.9	31.021	28.449	42.5	42.091	19.1	33.495	1.264	0.267	11.9	1.292	13.5	-1.251	-0.181	8.2	1.264		
275837.0	3098114.9	1.9	29.491	26.466	41.9	39.626	19.6	31.533	1.050	0.165	8.9	1.063	15.6	-1.038	0.002	-0.1	1.038		
275837.3	3098115.8	1.9	28.043.0																

EMF-OHL-001	Electric & Magnetic Field Study Report Kintore Tealing 400kV		Applies to	
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Appendix C WSP Assessment



SCOTTISH & SOUTHERN ELECTRICITY
NETWORK (SSEN)

EMF ASSESSMENT STUDY FOR 400kV OHTL



SCOTTISH & SOUTHERN ELECTRICITY NETWORK (SSEN)

EMF ASSESSMENT STUDY FOR 400KV OHTL REPORT

TYPE OF DOCUMENT (THIRD ISSUE)

PROJECT NO. 70111023

OUR REF. NO. 70111023-509

DATE: JULY 2025



SCOTTISH & SOUTHERN ELECTRICITY NETWORK (SSEN)

EMF ASSESSMENT STUDY FOR 400KV OHTL REPORT

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QUALITY CONTROL

Issue/revision	First issue	Second issue	Third issue
Remarks	Draft Report	Final Report	Final Report
Date	July 2024	August 2024	July 2025
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Checked by	R Gopinath	R Gopinath	R Gopinath
Authorised by	Abdullah Emhmed	Abdullah Emhmed	Abdullah Emhmed
Project number	70111023	70111023	70111023
Report number	70111023-509	70111023-509	70111023-509

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TERMINOLOGY

Term	Definition
ENA	Energy Network Association
EMF	Electro Magnetic Fields
ELF	Extremely Low Frequency
ICNIRP	International Commission on Non-Ionizing Radiation Protection
INIRC	International Non-Ionizing Radiation Committee
IARC	International Agency for Research on Cancer
NPS	National Policy Statement
OHTL	Overhead Transmission Line
SCENIHR	Scientific Committee on Emerging and Newly Identified Health Risks
SSEN	Scottish and Southern Electricity Network
WHO	World Health Organisation

1 BACKGROUND AND SCOPE OF WORK

WSP is assigned as the consultant to perform a 400kV Substation and 400kV OHL EMF Assessment Study Report for Scottish & Southern Electricity Networks (SSEN). The EMF Assessment Study is essential to ensure that personnel available in Substations or nearby to the OHTL are not exposed to a harmful level of Electromagnetic Field (EMF).

As per our proposal (70111023) to undertake the EMF studies, the following report is issued by WSP.

- **EMF assessment Study Report for 400kV OHTL of SSEN – Transmission**

This report covers the EMF assessment study for the 400kV OHTL of SSEN Transmission. The proposed tower cross-section diagram considered for the entire study is shown below.

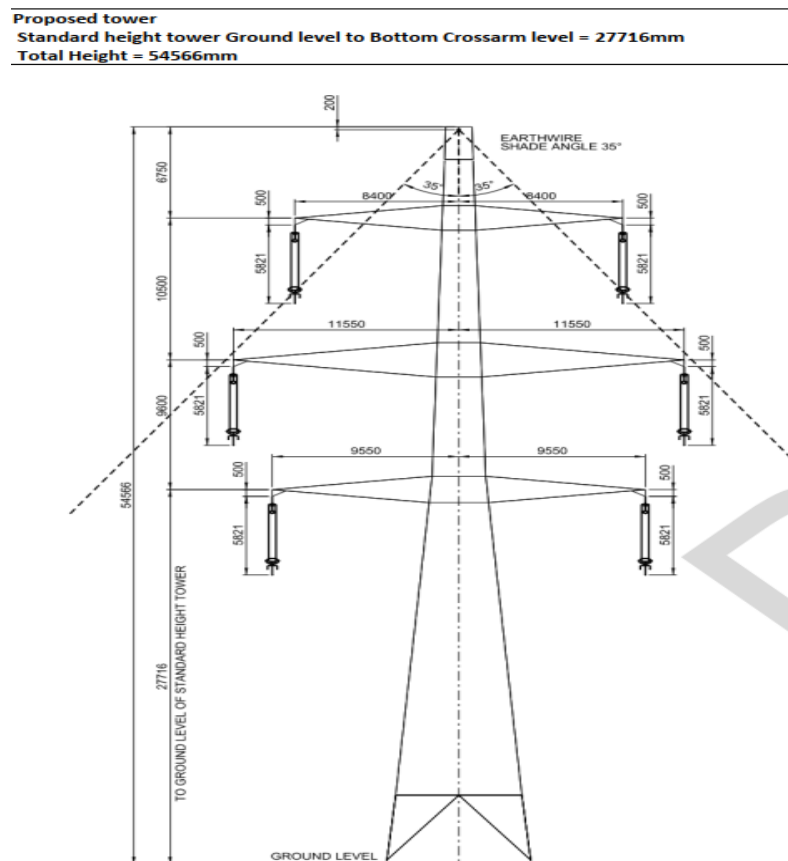


Figure 1- Proposed Suspension Tower AD & BD Diagram

2 INPUT DATA

The following are the input data received from SSEN for the undertaking the EMF studies.

Sl. No.	DESCRIPTION	VALUES	UNIT
A	Source Fault Level of 400kV OHTL		
	Phase Fault	45	kA
	Earth Fault	-	-
B	X/R Ratio of 400kV OHTL		
	Phase Fault	19.95	
	Earth Fault	6.7	
C	Length of the Overhead Transmission Line		
	Minimum	76	km
	Maximum	115	km
D	400kV Tension Insulator Details		
	Creepage Distance	10500	mm
	String Length	7.6	m
	Mechanical Strength	300	kN
	No. of Discs	22	-
	Disc Type	Glass	-
	Arc Horn Distance	2800	mm
E	400kV Suspension Insulator Details		
	Creepage Distance	4290	mm
	String Length	6	m
	Mechanical Strength	300	kN
	No. of Discs	24	-
	Disc Type	Glass	-
	Arc Horn Distance	2683	mm

F	400kV OHTL Conductors Details		
	Number of Conductor per phase	3	-
	Bundle Spacing	500	mm
	Maximum Continuous Current Rating of each circuit	5000	A
	Minimum Continuous Current Rating of each circuit	3370	A
	Soil Resistivity	100	ohm-m
	400kV Tower Footing Resistance	5	ohm
	400kV Transmission Line Minimum Ground Clearance	9	m

3 SIMULATION MODEL DEVELOPMENT

3.1 SIMULATION TOOL

CDEGS (Current Distribution, Electromagnetic Fields, Grounding and Soil Structure Analysis) tool was used to perform the EMF voltage assessment study for 400kV Overhead Transmission Line Tower.

CDEGS is a powerful set of integrated software tools designed to accurately analyse a variety of electromagnetic related problems encountered in all industries involving electric networks.

The use of CDEGS for EMF analysis is recognised within the industry as standard practice.

3.2 CONSIDERATIONS FOR THE STUDY

The following are the data considered as per the confirmation provided by SSEN

- 400kV Span Length is considered to be 350m.
- Ground Clearance of 400kV OHTL is considered as 9m.
- Optimum phasing is also included in the 400kV OHTL model.
- Maximum 400kV Overhead Transmission Line Length (i.e. 115km) is considered for the entire study.
- EMF observation points is extended up to 170m on cross section side of the tower.

3.3 MODEL DEVELOPMENT

The following are the models that have been developed in CDEGS simulation tool to carry out the required EMF assessment study. The insulator lengths provided within the inputs table in section 2 are approximate lengths and final lengths will be confirmed by SSEN during their detailed design. Slight variation in these lengths will have negligible impact on the EMF assessment as the conductor has been sagged to have a minimum clearance to ground of 9m and the EMF values are taken at this closest point to ground where fields are at their maximum.

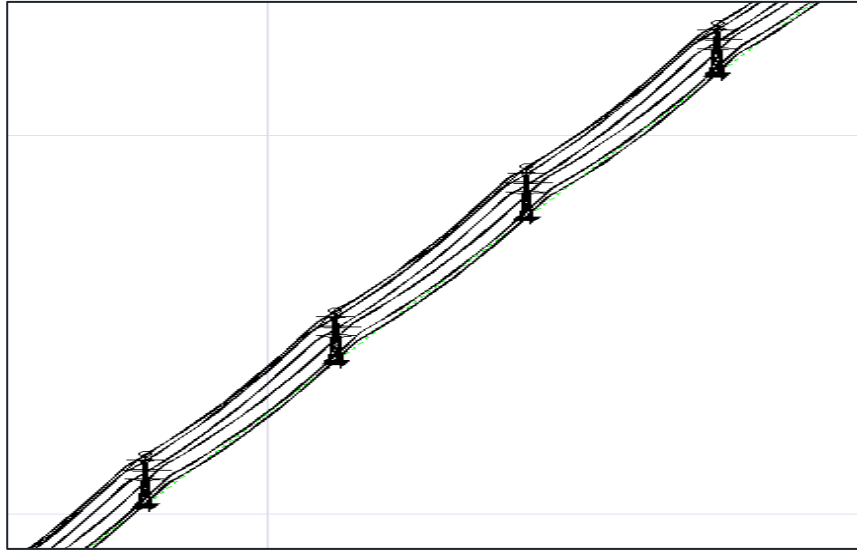


Figure 2 400kV OHTL Model

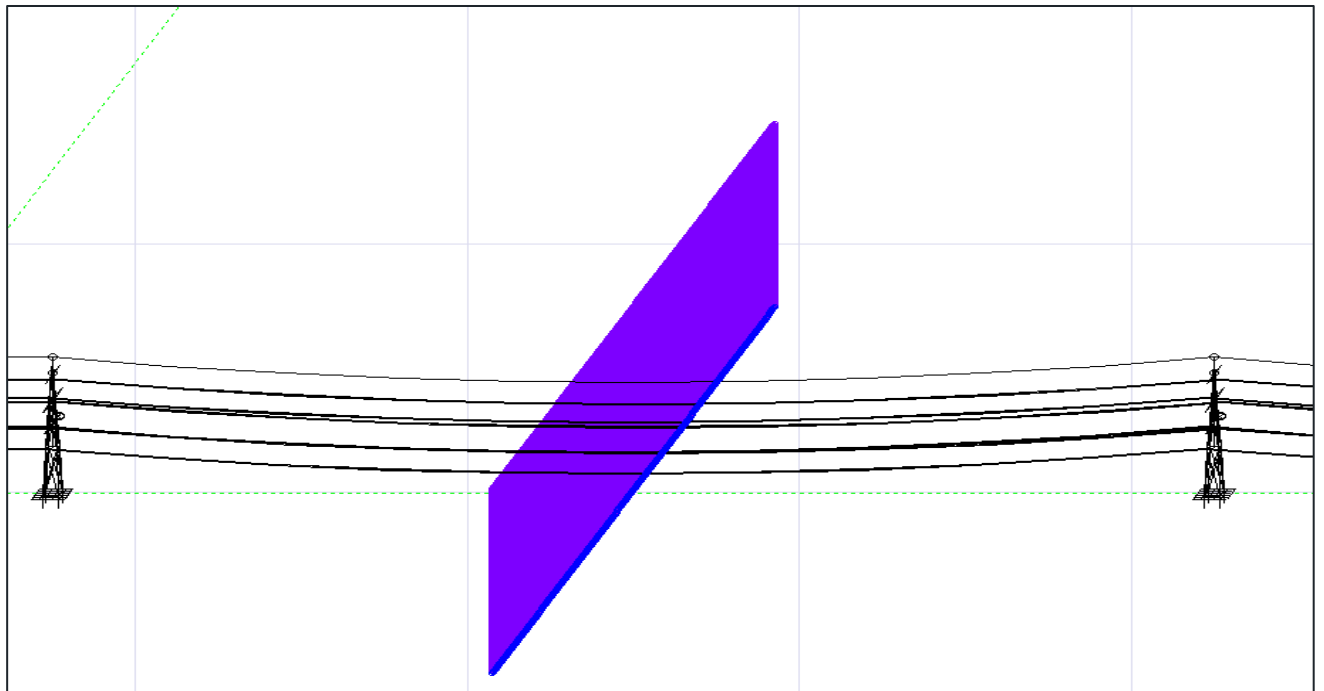


Figure 3 EMF Measuring points in YZ Plane in the mid of span

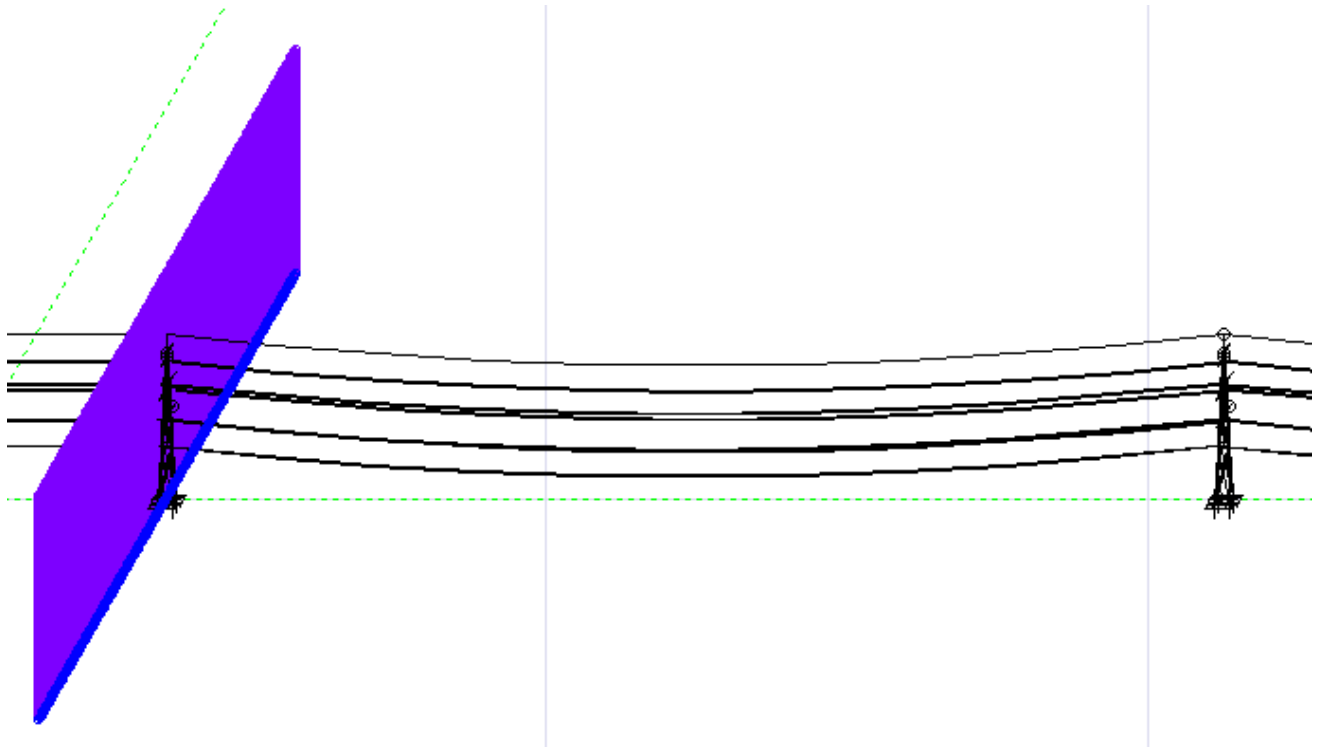


Figure 4 EMF Measuring points in YZ Plane in the mid of tower

4 STANDARD EXPOSURE LIMITS

4.1 PUBLIC EXPOSURE LIMITS

In March 2004, the UK adopted the 1998 guidelines published by ICNIRP. These guidelines (See [Table 1](#)) are designed to set conservative exposure levels for the general public to electric and magnetic fields, and they are endorsed by the UK's Health Protection Agency, the World Health Organisation and the UK Government.

It is the policy of the electricity industry to follow these independent guidelines. A Code of Practice CoP, published jointly in 2012 by industry and the Department for Energy and Climate Change (now part of the Department for Business, Energy and Industrial Strategy). This CoP sets out all the practical details needed to apply the exposure limits for transmission lines. All exposures in homes already comply with the ICNIRP guidelines. The electricity industry designs all new equipment to comply with the Government guidelines as set out in the Code of Practice. This includes measures such as adhering to statutory ground clearance requirements and ensuring optimum phasing of high voltage double-circuit overhead lines.

The CoP sets the maximum levels for long term public exposure as 360 μT for magnetic fields and 9 kV/m for electric fields. Long term exposure relates to places of residence or similar where people regularly spend extended periods of time. In other environments, where exposure can be deemed not to be for a significant period of time, the ICNIRP occupational guidelines, rather than the ICNIRP general public guidelines, shall be deemed to apply.

Table 1 – Public Exposure Limits for Power Frequency EMFs

Sl. No.	Public Exposure Levels	Electric Fields	Magnetic Fields
1	Reference level (external unperturbed field)	5kV/m	100 μT
2	Field corresponding to the basic restriction (external unperturbed field)	9kV/m	360 μT

4.2 OCCUPATIONAL EXPOSURE LIMITS

Occupational exposure (see [Table 2](#)) is defined as any exposure experienced by an individual during work related activities. The limits for occupational exposure are stated in the Control of Electromagnetic Fields at Work Regulations 2016. These limits are enforceable and should not be exceeded.

Table 2– Occupational Exposure Limits for Power Frequency EMFs

Sl. No.	Occupational Exposure Levels	Electric Fields	Magnetic Fields
1	<i>Reference level (external unperturbed field)</i>	<i>10kV/m</i>	<i>1000 μT</i>
2	<i>Field corresponding to the basic restriction (external unperturbed field)</i>	<i>20kV/m</i>	<i>6000 μT</i>

5 CASE SCENARIO

Based on the measuring profile and OHTL loading conditions, the following are the cases considered as discussed with SSEN.

Case A considers the expected continuous operating current for the proposed OHTL.

Case B considers the maximum possible current for the OHTL based on the substation equipment ratings being capped at 5000A. It should however be noted that some substation plant is limited at 4000A so although this assessment has been carried out, it is presented to consider the worst case load conditions however case A is representative of the actual operational values.

5.1 CASE - A

With partial loading of the OHTL (i.e. 3375A), the magnitudes of Electric and Magnetic Fields are measured at the mid of span.

5.2 CASE - B

With full loading of the OHTL (i.e. 5000A), the magnitudes of Electric and Magnetic Fields are measured at the mid of span.

6 STUDY RESULTS

This section presents the simulation results of the EMF assessment study for the Partial and full loading of the 400kV OHTL Circuit and results are tabulated in the [Table 3](#) and [Table 4](#).

6.1 SIMULATED GRAPH FOR ELECTRIC FIELD

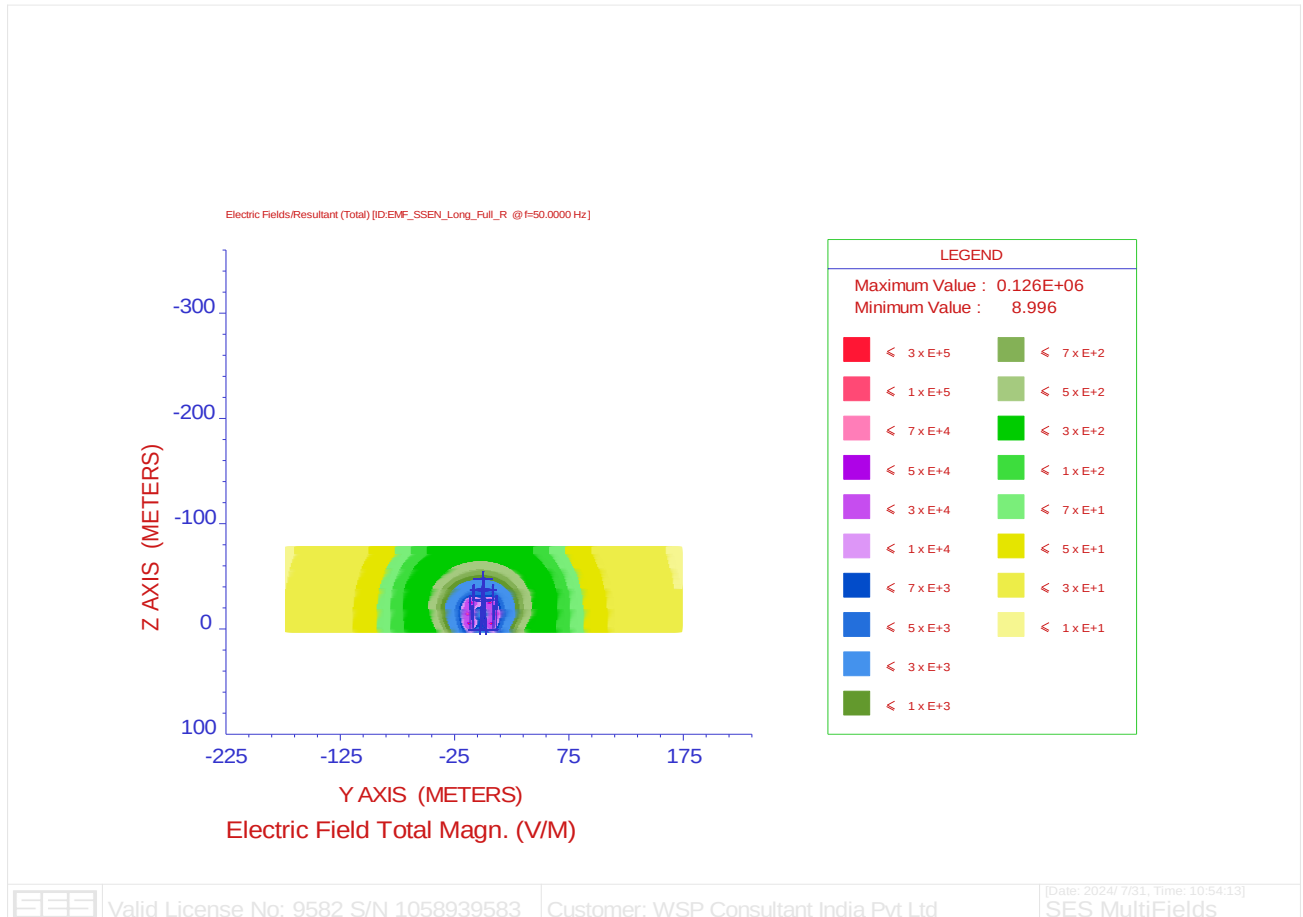


Figure 5 Electric Field Graph for Case A

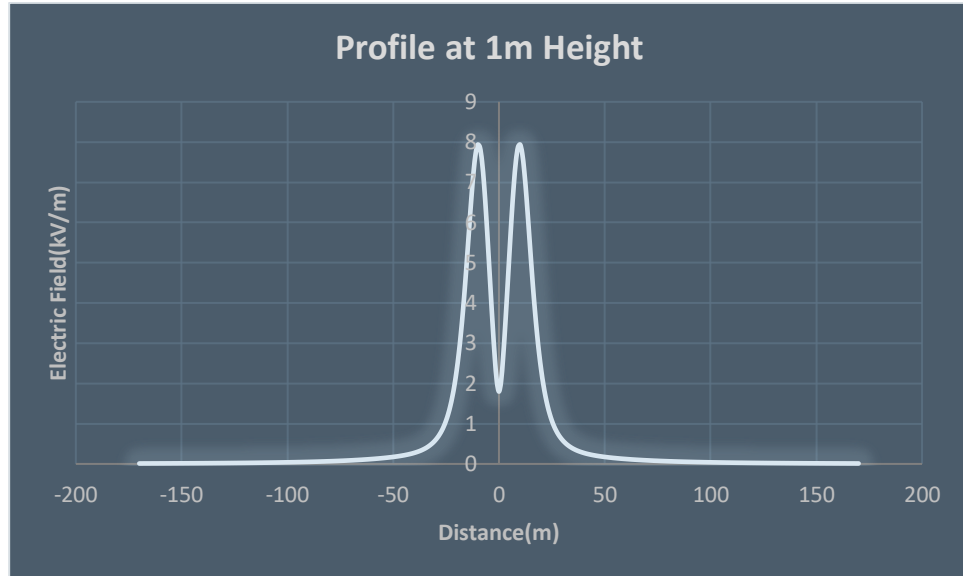


Figure 6 Electric Field Profile at 1m Height for Case A

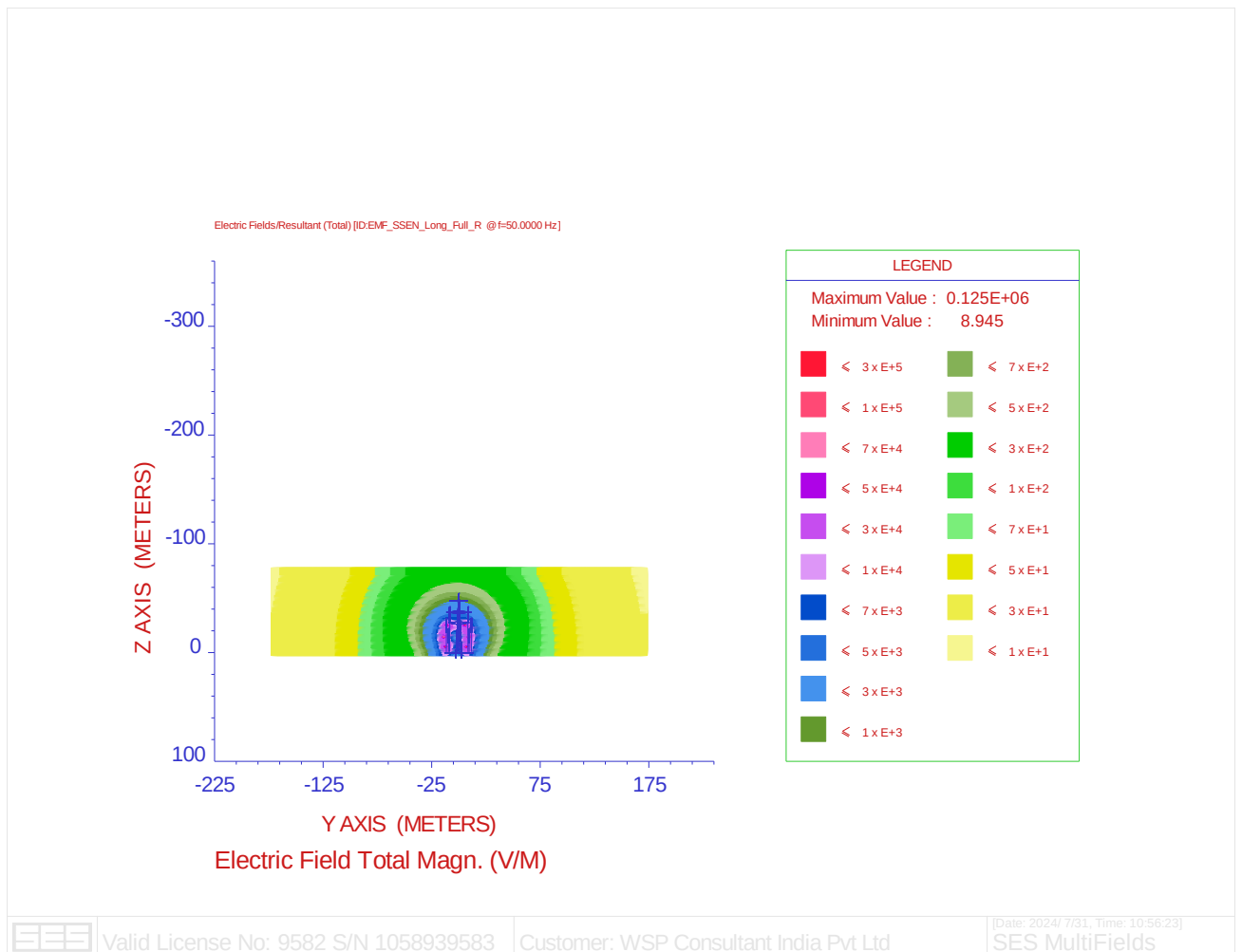


Figure 7 Electric Field Graph for Case B

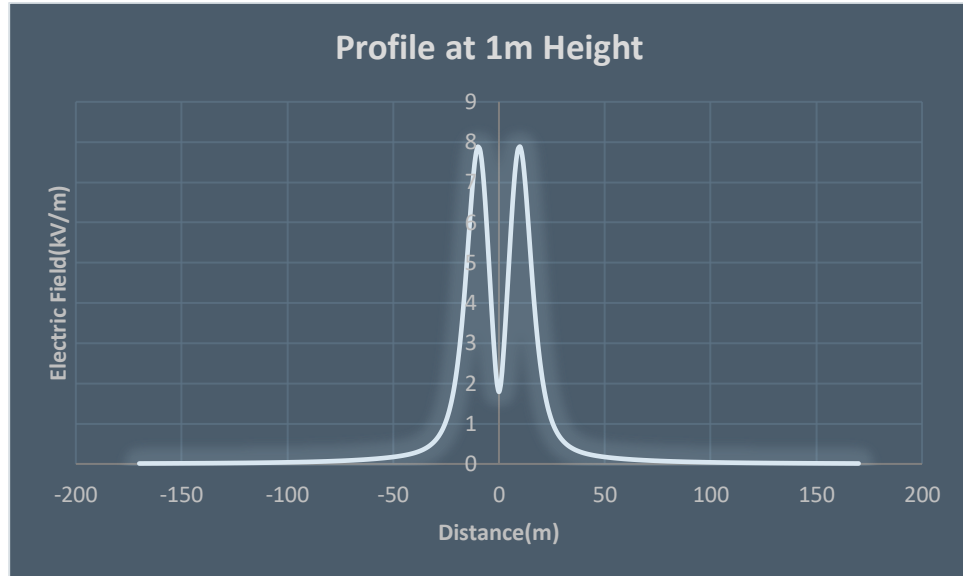


Figure 8 Electric Field Profile at 1m Height for Case B

6.2 TABULATED CASE RESULTS FOR ELECTRIC FIELD

Table 3 Electric Field result with change in OHTL loading and profile location

CASES	MAGNITUDE OF ELECTRIC FIELD FOR VARIOUS CASES					
	PROFILE LOCATION	400kV OHTL LOADING	SIMULATED VALUE AT 1m HEIGHT FROM GROUND		UK PUBLIC EXPOSURE LIMIT	SAFE/ UNSAFE
			± 9 m from Centre (Lowest Conductor Below)	± 170 m from Centre		
	TOWER/MID OF SPAN	A	kV/m		kV/m	
A	MID OF SPAN	3375 A	7.936394	0.010479	9.0	SAFE
B	MID OF SPAN	5000 A	7.881355	0.01043		SAFE

6.3 SIMULATED GRAPH FOR MAGNETIC FIELD

Figure 9 Magnetic Field Graph for Case A

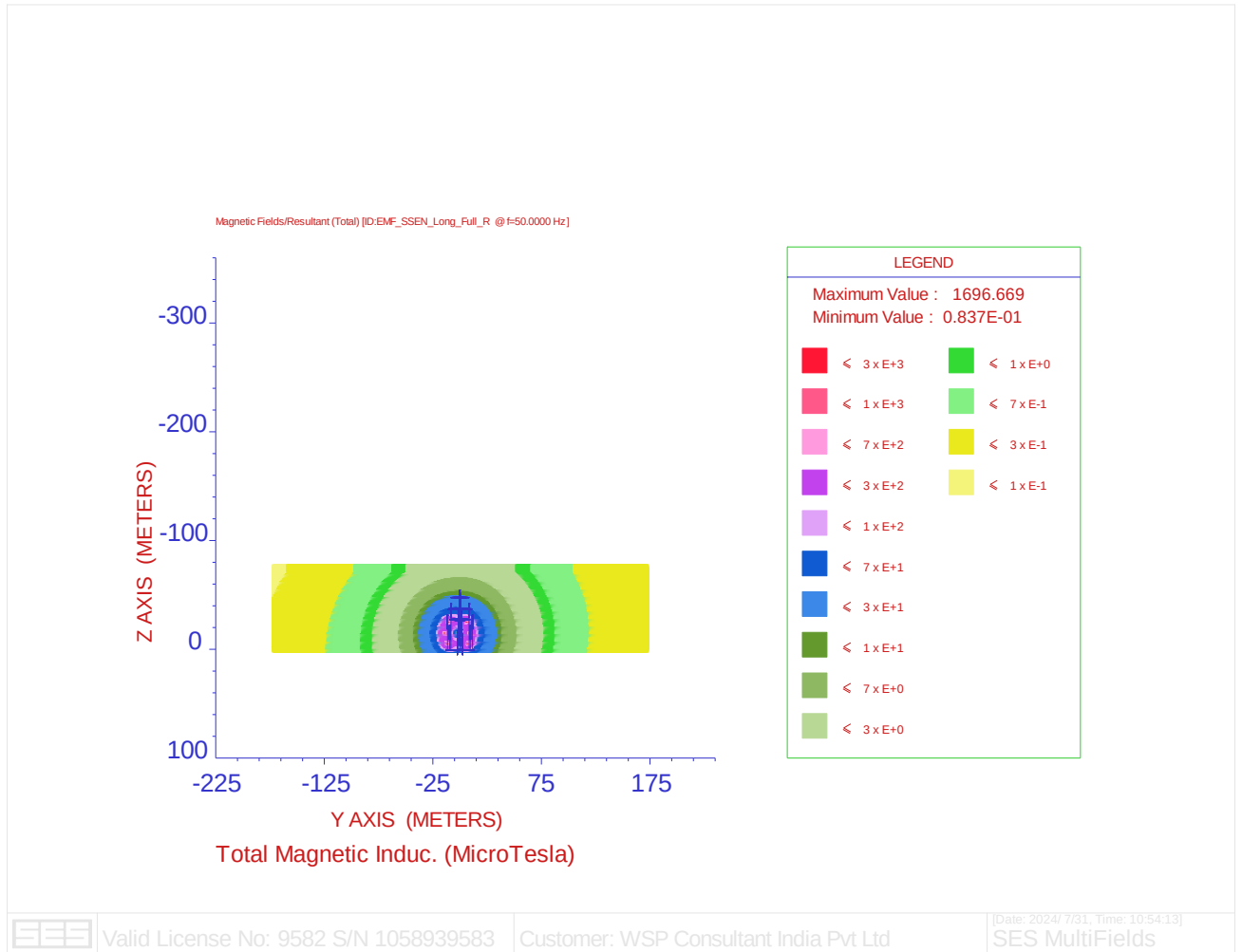


Figure 10 Magnetic Field Graph for Case A

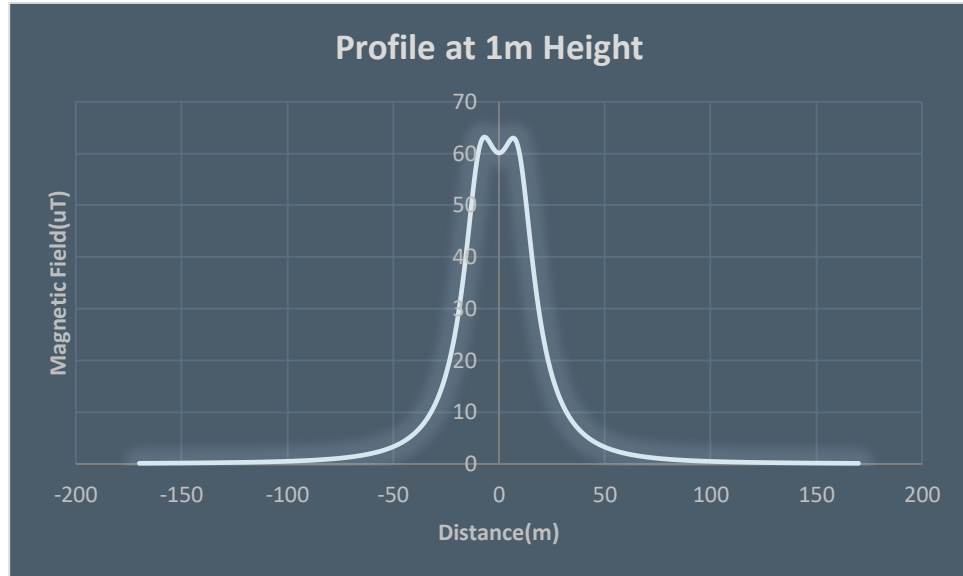


Figure 11 Magnetic Field Profile at 1m Height for Case A

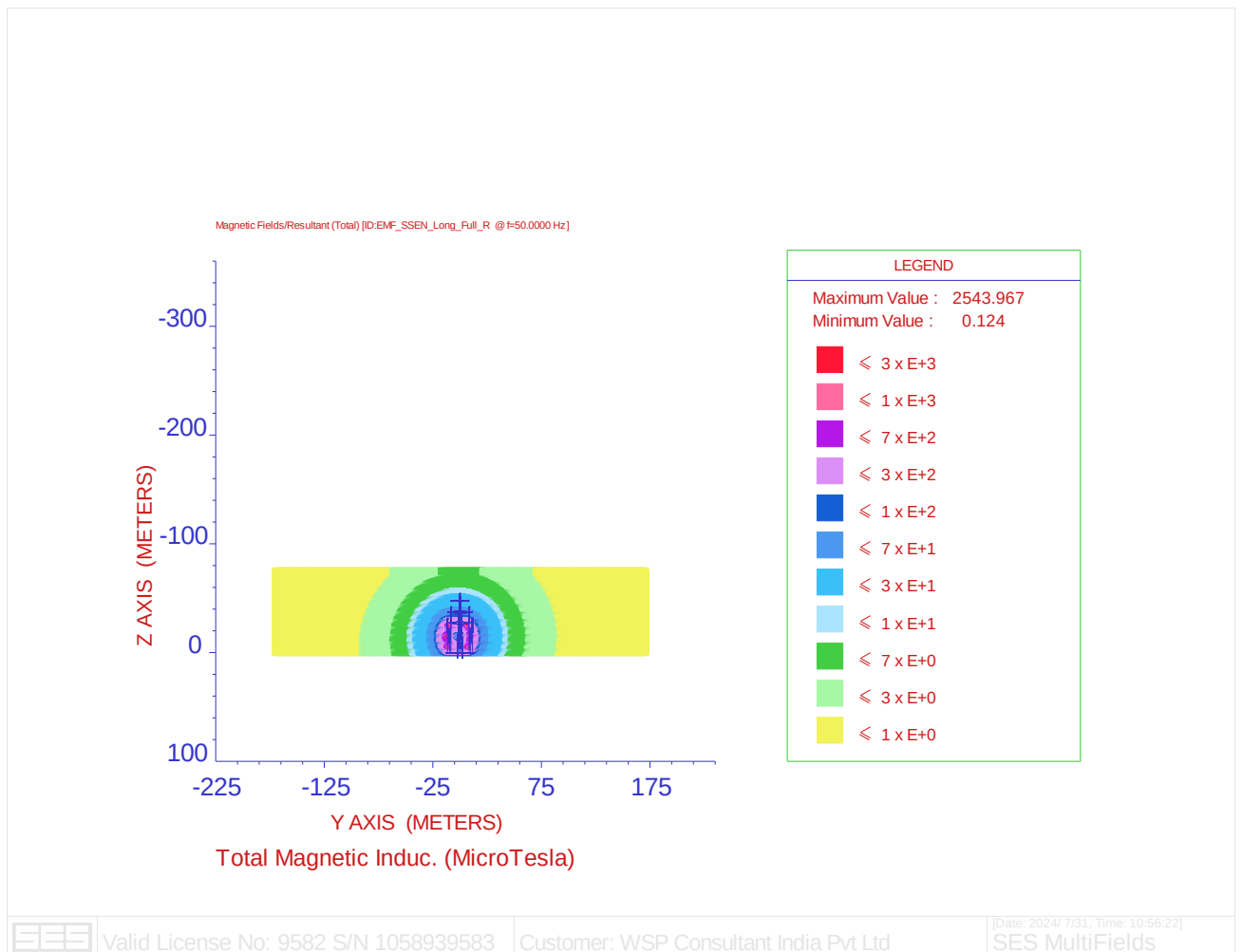


Figure 12 Magnetic Field Graph for Case B

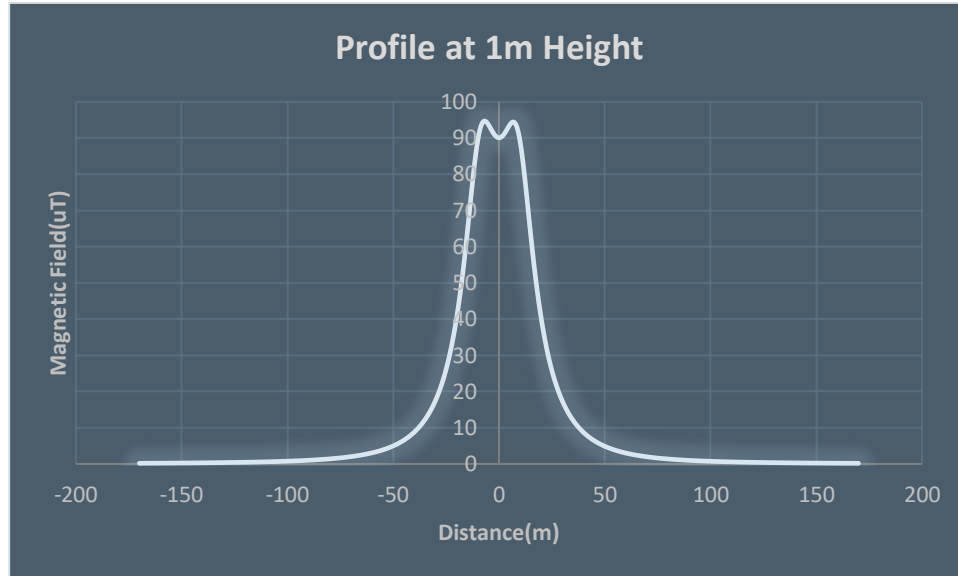


Figure 13 Magnetic Field Profile at 1m Height for Case B

6.4 TABULATED CASE RESULTS FOR MAGNETIC FIELD

Table 4 Magnetic Field result with change in OHTL loading and profile location

CASES	MAGNITUDE OF MAGNETIC FIELD FOR VARIOUS CASES					
	PROFILE LOCATION	400kV OHTL LOADING	SIMULATED VALUE AT 1m HEIGHT FROM GROUND		UK PUBLIC EXPOSURE LIMIT	SAFE/ UNSAFE
			± 9 m from Centre (Lowest Conductor Below)	± 170 m from Centre		
	TOWER/MID OF SPAN	A	Micro Tesla		Micro Tesla	
A	MID OF SPAN	3375 A	62.74127	0.123508	360	SAFE
B	MID OF SPAN	5000 A	92.30611	0.182544		SAFE

7 CONCLUSION

- In all the simulated test cases, the results have shown that the simulated values of Electric Field are well within the UK Exposure Limit.
- Similarly, the simulated value of the Magnetic Field is well within the UK Exposure Limit.

8 REFERENCES

- ICNIRP- Guidelines for Limiting Exposure to time varying Electric, Magnetic and EMF (Up to 300GHz)
- Electric and Magnetic Fields the facts – Produced by ENA - September 2017
- Working Group C4.208, "EMC within Power Plants and Substations," CIGRE2013
- IEEE Reference paper - Magnetic field calculations within substation environment for EMC studies
- National Policy Statement for Electricity Networks Infrastructure (EN-5)

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Appendix D PLS CADD Report for Cumulative Assessment

Optimal Phasing of Adjacent Circuits

PLS-CADD Version 20.01x64 14:23:43 02 July 2025
Scottish and Southern Energy
Project Name: 'C:\PS\Combined_EMF_Check Temp\Combined_EMF_Check.don'
Line Title: 'Max Op'

3D EMF Calculation Notes:
1) Calculations based on the EPRI Red Book methods (3rd Edition, 2005 - 7.4 Calculation of Magnetic Fields and Appendices 7.1 Calculation of Field Ellipse Parameters and 7.6 Electric Field Calculations for 3D Geometry).
2) All wire positions are modeled at the specified weather case and wind direction. Height above ground determined by the modeled ground TIN.
3) Only the effects of wires are being analysed. The effects of structures are not included unless enabled as noted below.
4) Ground return is being ignored for magnetic field calculations.

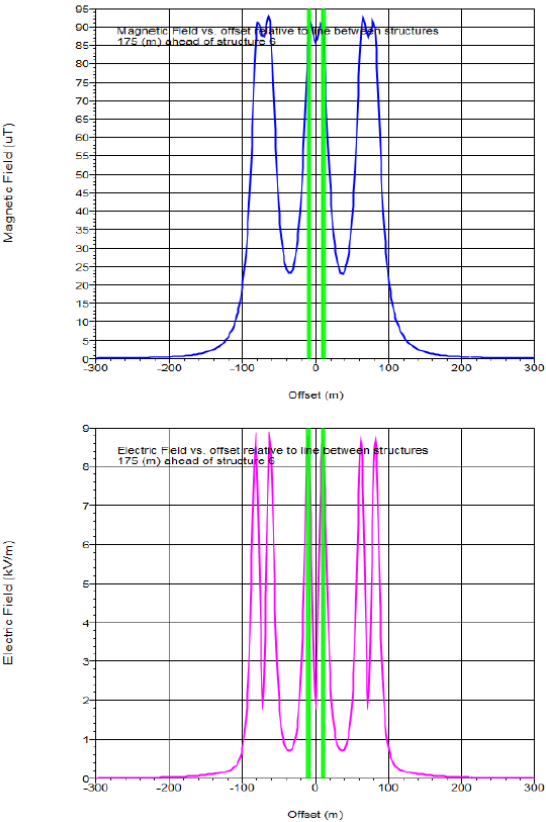
Header height above ground: 1.00 (m)
Maximum wire distance: 300.00 (m)
Maximum cable segment size: 3.00 (m)
Cross section offset +/-: 300.00 (m)
Result interval: 1.00 (m)
Electric field limit: 5.00 (kV/m)
Magnetic field limit: 160.00 (uT)
Space potential limit: 0.00 (kV)
Contour Map Spacing: 3 (m)
Analysing spans between these structures: 6 - 7

One or more sections have wind from both directions which is not supported. A wind direction of left is being used for those sections.

Section Data for 3D EMF Results:

Section Number	Section Note	Voltage (kV)	Current (Amps)	Filename	Description	Conductors Per Phase	Bundle Diameter (cm)	Cable Radius (cm)	Weather Case	Condition	Wind Dir.	Temperature (deg C)	WC Effective Radius (cm)
1	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
2	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
3	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
4	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
5	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
6	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
7	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
8	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
9	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
10	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
11	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
12	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
13	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
14	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
15	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
16	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
17	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700
18	400.0 5000.0	700mm AAC	AAAC	700mm ⁴ AAAC	- Araucaria (H)	3	57.735	1.863	Max Op	Creep FE Left	Left	90.000	16.700

Wire low point cross section results between structures 6 and 7





Revision: 1.00

Classification: Public

Issue Date: July 25

3D EMF Point Results Span from 6 to 7:

Measurement		B		H		EF		Space Potential		
X (m)	Y (m)	Real Imaginary (kV)	Angle Magnitude (deg)	Polarization (deg)	Magnitude (kV)	Real Imaginary (kV)	Angle Magnitude (deg)	Polarization (deg)	Real Imaginary (kV)	Angle Magnitude (deg)
372.0	525.0	0.000	51.8	0.000	0.000	0.000	0.000	0.000	0.000	0.000
371.0	525.0	0.071	51.8	0.115	7.8	0.092	0.000	0.009	87.1	0.009
370.0	525.0	0.072	51.8	0.116	6.9	0.093	0.000	0.009	87.3	0.009
369.0	525.0	0.073	51.8	0.118	7.2	0.094	0.000	0.009	87.2	0.009
368.0	525.0	0.073	51.8	0.119	7.9	0.095	0.000	0.009	87.1	0.009
367.0	525.0	0.074	51.8	0.120	7.6	0.096	0.001	0.010	86.9	0.009
366.0	525.0	0.075	51.8	0.121	7.5	0.097	0.001	0.010	86.8	0.010
365.0	525.0	0.076	51.8	0.123	7.4	0.098	0.001	0.010	86.7	0.010
364.0	525.0	0.077	51.8	0.124	7.8	0.099	0.001	0.010	86.5	0.010
363.0	525.0	0.078	51.8	0.125	7.9	0.100	0.001	0.010	86.4	0.010
362.0	525.0	0.078	51.8	0.127	8.0	0.101	0.001	0.010	86.3	0.010
361.0	525.0	0.079	51.8	0.128	8.2	0.102	0.001	0.010	86.1	0.010
360.0	525.0	0.080	51.8	0.130	8.3	0.103	0.001	0.010	86.0	0.010
359.0	525.0	0.081	51.8	0.131	8.5	0.104	0.001	0.010	85.8	0.010
358.0	525.0	0.082	51.8	0.133	8.6	0.106	0.001	0.010	85.7	0.010
357.0	525.0	0.083	51.8	0.134	8.8	0.107	0.001	0.011	85.5	0.011
356.0	525.0	0.084	51.8	0.136	8.9	0.108	0.001	0.011	85.4	0.011
355.0	525.0	0.085	51.8	0.137	9.1	0.109	0.001	0.011	85.3	0.011
354.0	525.0	0.086	51.8	0.139	9.2	0.111	0.001	0.011	85.1	0.011
353.0	525.0	0.087	51.8	0.141	9.4	0.112	0.001	0.011	85.0	0.011
352.0	525.0	0.088	51.8	0.142	9.5	0.113	0.001	0.011	84.8	0.011
351.0	525.0	0.089	51.8	0.144	9.7	0.114	0.001	0.011	84.7	0.011
350.0	525.0	0.090	51.8	0.146	9.8	0.116	0.001	0.011	84.5	0.011
349.0	525.0	0.091	51.8	0.147	10.0	0.117	0.001	0.011	84.4	0.011
348.0	525.0	0.092	51.7	0.149	10.1	0.119	0.001	0.012	84.2	0.012
347.0	525.0	0.093	51.8	0.151	10.3	0.120	0.001	0.012	84.0	0.012
346.0	525.0	0.094	51.8	0.153	10.5	0.122	0.001	0.012	83.9	0.012
345.0	525.0	0.096	51.2	0.155	10.6	0.123	0.001	0.012	83.7	0.012
344.0	525.0	0.097	51.2	0.156	10.8	0.124	0.001	0.012	83.6	0.012
343.0	525.0	0.098	51.4	0.158	10.9	0.126	0.001	0.012	83.4	0.012
342.0	525.0	0.099	51.7	0.160	11.1	0.128	0.001	0.012	83.2	0.012
341.0	525.0	0.101	51.8	0.162	11.2	0.130	0.001	0.012	83.1	0.012
340.0	525.0	0.102	51.7	0.164	11.4	0.131	0.002	0.013	82.9	0.013
339.0	525.0	0.103	51.7	0.167	11.6	0.133	0.002	0.013	82.7	0.013
338.0	525.0	0.104	51.7	0.169	11.7	0.134	0.002	0.013	82.6	0.013
337.0	525.0	0.106	51.7	0.171	11.9	0.136	0.002	0.013	82.4	0.013
336.0	525.0	0.107	51.7	0.173	12.0	0.138	0.002	0.013	82.2	0.013
335.0	525.0	0.109	51.7	0.175	12.2	0.139	0.002	0.013	82.1	0.013
334.0	525.0	0.110	51.7	0.177	12.3	0.141	0.002	0.013	81.9	0.013
333.0	525.0	0.112	51.4	0.180	12.6	0.143	0.002	0.014	81.7	0.014
332.0	525.0	0.113	51.3	0.182	12.8	0.145	0.002	0.014	81.5	0.014
331.0	525.0	0.115	51.6	0.185	12.9	0.147	0.002	0.014	81.4	0.014
330.0	525.0	0.116	51.4	0.187	13.1	0.149	0.002	0.014	81.2	0.014
329.0	525.0	0.118	51.8	0.188	13.2	0.151	0.002	0.014	81.0	0.014
328.0	525.0	0.119	51.6	0.192	13.4	0.153	0.002	0.014	80.8	0.014
327.0	525.0	0.121	51.5	0.195	13.6	0.155	0.002	0.015	80.6	0.015
326.0	525.0	0.123	51.5	0.197	13.7	0.157	0.002	0.015	80.4	0.015
325.0	525.0	0.125	51.5	0.200	13.9	0.159	0.003	0.015	80.2	0.015
324.0	525.0	0.126	51.5	0.203	14.1	0.161	0.003	0.015	80.1	0.015
323.0	525.0	0.128	51.5	0.206	14.3	0.164	0.003	0.015	79.9	0.015
322.0	525.0	0.130	51.4	0.209	14.6	0.165	0.003	0.015	79.7	0.015
321.0	525.0	0.132	51.4	0.211	14.6	0.168	0.003	0.016	79.5	0.016
320.0	525.0	0.134	51.4	0.214	14.8	0.171	0.003	0.016	79.3	0.016
319.0	525.0	0.136	51.4	0.218	15.0	0.173	0.003	0.016	79.1	0.016
318.0	525.0	0.138	51.3	0.221	15.1	0.176	0.003	0.016	78.9	0.016
317.0	525.0	0.140	51.3	0.224	15.3	0.178	0.003	0.016	78.7	0.016
316.0	525.0	0.142	51.3	0.227	15.5	0.181	0.003	0.017	78.5	0.017
315.0	525.0	0.143	51.3	0.230	15.7	0.183	0.003	0.017	78.3	0.017
314.0	525.0	0.146	51.2	0.248	14.0	0.198	0.003	0.019	80.1	0.019
313.0	525.0	0.158	51.1	0.252	14.2	0.200	0.003	0.019	79.9	0.020
312.0	525.0	0.160	51.1	0.255	14.4	0.204	0.004	0.020	79.7	0.020
311.0	525.0	0.163	51.1	0.259	14.6	0.206	0.004	0.020	79.5	0.020
310.0	525.0	0.165	51.1	0.263	14.8	0.209	0.004	0.020	79.3	0.020
309.0	525.0	0.167	51.0	0.266	15.0	0.212	0.004	0.020	79.0	0.021
308.0	525.0	0.170	51.0	0.270	15.2	0.214	0.004	0.020	78.8	0.021
307.0	525.0	0.173	51.0	0.274	15.4	0.218	0.004	0.021	78.6	0.021
306.0	525.0	0.175	51.0	0.278	15.6	0.221	0.004	0.021	78.4	0.021
305.0	525.0	0.178	50.9	0.282	15.8	0.225	0.004	0.021	78.2	0.021
304.0	525.0	0.181	50.9	0.287	16.0	0.228	0.005	0.021	77.9	0.022
303.0	525.0	0.184	50.9	0.291	16.2	0.231	0.005	0.022	77.7	0.022
302.0	525.0	0.187	50.8	0.295	16.4	0.235	0.005	0.022	77.5	0.022
301.0	525.0	0.190	50.8	0.300	16.6	0.239	0.005	0.022	77.3	0.022
300.0	525.0	0.193	50.8	0.304	16.8	0.242	0.005	0.022	77.0	0.022
299.0	525.0	0.195	50.7	0.309	16.9	0.245	0.006	0.022	76.8	0.022
298.0	525.0	0.198	50.7	0.314	17.1	0.248	0.006	0.022	76.6	0.022
297.0	525.0	0.201	50.8	0.320	17.3	0.251	0.007	0.022	76.4	0.022
296.0	525.0	0.204	50.8	0.325	17.5	0.254	0.007	0.022	76.2	0.022
295.0	525.0	0.207	50.8	0.330	17.7	0.257	0.007	0.022	76.0	0.022
294.0	525.0	0.210	50.7	0.336	17.9	0.260	0.007	0.022	75.8	0.022
293.0	525.0	0.213	50.7	0.341	18.1	0.263	0.007	0.022	75.6	0.022
292.0	525.0	0.216	50.7	0.346	18.3	0.266	0.007	0.022	75.4	0.022
291.0	525.0	0.219	50.6	0.351	18.5	0.269	0.008	0.022	75.2	0.022
290.0	525.0	0.222	50.6	0.356	18.7	0.272	0.008	0.022	75.0	0.022
289.0	525.0	0.225	50.6	0.361	18.9	0.275	0.008	0.022	74.8	0.022
288.0	525.0	0.228	50.6	0.366	19.1	0.278	0.008	0.022	74.6	0.022
287.0	525.0	0.231	50.6	0.371	19.3	0.281	0.008	0.022	74.4	0.022
286.0	525.0	0.234	50.6	0.376	19.5	0.284	0.008	0.022	74.2	0.022
285.0	525.0	0.237	50.6	0.381	19.7	0.287	0.008	0.022	74.0	0.022
284.0	525.0	0.240	50.6	0.386	19.9	0.290	0.008	0.022	73.8	0.022
283.0	525.0	0.243	50.6	0.391	20.1	0.293	0.008	0.022	73.6	0.022
282.0	525.0	0.246	50.6	0.396	20.3	0.296	0.008	0.022	73.4	0.022
281.0	525.0	0.249	50.6	0.401	20.5	0.299	0.008	0.022	73.2	0.022
280.0	525.0	0.252	50.6	0.406	20.7	0.302	0.008	0.022	73.0	0.022
279.0	525.0	0.255	50.6	0.411	20.9	0.305	0.008	0.022	72.8	0.022
278.0	525.0	0.258	50.6	0.416	21.1	0.308	0.008	0.022	72.6	0.022
277.0	525.0	0.261	50.6	0.421	21.3	0.311	0.008	0.022	72.4	0.022
276.0	525.0	0.264	50.6	0.426	21.5	0.314	0.008	0.022	72.2	0.022
275.0	525.0	0.267	50.6	0.431	21.7	0.317	0.008	0.022	72.0	0.022
274.0	525.0	0.270								

EMF-OHL-2001				Electric & Magnetic Field Study Report										Applies to	
				Kintore Tealing 400kV										Distribution	Transmission
Revision: 1.00				Classification: Public											✓
Issue Date: July 25															

217.0	525.0	1.0	1.527	1.492	44.3	2.135	35.2	1.699	0.078	0.068	40.8	0.104	1.7	-0.078	-0.068	40.8	0.104
216.0	525.0	1.0	1.594	1.540	44.2	2.209	35.5	1.758	0.081	0.068	39.8	0.106	1.8	-0.081	-0.068	39.8	0.106
215.0	525.0	1.0	1.644	1.590	44.0	2.287	35.7	1.820	0.084	0.068	38.8	0.108	1.9	-0.084	-0.068	38.8	0.108
214.0	525.0	1.0	1.707	1.643	43.9	2.369	36.0	1.885	0.088	0.068	37.7	0.111	1.9	-0.088	-0.068	37.7	0.111
213.0	525.0	1.0	1.774	1.698	43.8	2.456	36.3	1.954	0.091	0.068	36.6	0.113	2.0	-0.091	-0.067	36.6	0.113
212.0	525.0	1.0	1.844	1.756	43.6	2.547	36.6	2.026	0.094	0.067	35.5	0.116	2.1	-0.094	-0.067	35.4	0.116
211.0	525.0	1.0	1.918	1.817	43.5	2.642	36.9	2.103	0.098	0.067	34.2	0.118	2.2	-0.098	-0.067	34.2	0.118
210.0	525.0	1.0	1.996	1.881	43.3	2.743	37.2	2.183	0.101	0.066	33.0	0.121	2.2	-0.101	-0.066	33.0	0.121
209.0	525.0	1.0	2.079	1.948	43.1	2.849	37.5	2.267	0.105	0.065	31.7	0.124	2.3	-0.105	-0.065	31.7	0.124
208.0	525.0	1.0	2.166	2.019	42.9	2.961	37.8	2.356	0.109	0.064	30.3	0.127	2.4	-0.109	-0.064	30.3	0.127
207.0	525.0	1.0	2.259	2.093	42.8	3.080	38.1	2.451	0.113	0.063	28.9	0.130	2.5	-0.113	-0.063	28.9	0.130
206.0	525.0	1.0	2.357	2.171	42.7	3.205	38.5	2.550	0.118	0.061	27.4	0.133	2.7	-0.118	-0.061	27.4	0.133
205.0	525.0	1.0	2.460	2.254	42.6	3.337	38.8	2.653	0.122	0.059	25.9	0.136	2.8	-0.122	-0.059	25.9	0.136
204.0	525.0	1.0	2.571	2.341	42.3	3.477	39.1	2.767	0.127	0.057	24.3	0.139	2.9	-0.127	-0.057	24.2	0.139
203.0	525.0	1.0	2.688	2.432	42.1	3.625	39.4	2.884	0.131	0.055	22.6	0.142	3.1	-0.131	-0.054	22.5	0.142
202.0	525.0	1.0	2.812	2.529	42.0	3.782	39.7	3.009	0.136	0.052	20.8	0.146	3.2	-0.136	-0.051	20.7	0.146
201.0	525.0	1.0	2.944	2.631	41.8	3.948	40.0	3.142	0.141	0.048	18.9	0.149	3.4	-0.141	-0.048	18.8	0.149
200.0	525.0	1.0	3.085	2.739	41.6	4.125	40.3	3.283	0.146	0.045	17.0	0.153	3.6	-0.146	-0.044	16.8	0.153
199.0	525.0	1.0	3.235	2.853	41.4	4.313	40.7	3.432	0.151	0.040	14.9	0.157	3.8	-0.151	-0.040	14.7	0.156
198.0	525.0	1.0	3.395	2.974	41.2	4.513	41.0	3.592	0.157	0.035	12.7	0.160	4.0	-0.156	-0.035	12.5	0.160
197.0	525.0	1.0	3.566	3.102	41.0	4.726	41.3	3.761	0.162	0.030	10.5	0.165	4.2	-0.162	-0.029	10.2	0.164
196.0	525.0	1.0	3.749	3.238	40.8	4.953	41.6	3.942	0.167	0.024	8.1	0.169	4.7	-0.167	-0.023	7.7	0.169
195.0	525.0	1.0	3.944	3.382	40.6	5.196	42.0	4.134	0.173	0.017	5.8	0.174	4.7	-0.173	-0.015	5.1	0.173
194.0	525.0	1.0	4.154	3.534	40.4	5.454	42.3	4.340	0.178	0.011	3.7	0.178	5.0	-0.178	-0.007	3.3	0.178
193.0	525.0	1.0	4.379	3.697	40.2	5.733	42.6	4.560	0.183	0.010	3.1	0.184	5.3	-0.183	-0.002	-0.7	0.183
192.0	525.0	1.0	4.620	3.869	39.9	6.027	42.9	4.796	0.189	0.016	5.0	0.189	5.7	-0.189	0.012	-3.8	0.189
191.0	525.0	1.0	4.880	4.053	39.7	6.344	43.3	5.048	0.194	0.027	7.9	0.195	6.0	-0.193	0.024	-7.1	0.195
190.0	525.0	1.0	5.160	4.248	39.5	6.684	43.6	5.319	0.198	0.039	11.2	0.202	6.4	-0.198	0.037	-10.6	0.202
189.0	525.0	1.0	5.462	4.457	39.2	7.049	43.9	5.610	0.203	0.054	14.8	0.209	6.7	-0.202	0.052	-14.4	0.209
188.0	525.0	1.0	5.787	4.679	39.0	7.442	44.2	5.922	0.208	0.070	18.7	0.218	7.1	-0.208	0.068	-18.3	0.217
187.0	525.0	1.0	6.139	4.916	38.7	7.865	44.5	6.259	0.209	0.088	22.8	0.227	7.5	-0.209	0.086	-22.5	0.226
186.0	525.0	1.0	6.521	5.168	38.4	8.321	44.8	6.621	0.211	0.108	27.1	0.237	7.9	-0.211	0.107	-26.9	0.236
185.0	525.0	1.0	6.934	5.439	38.1	8.812	45.2	7.013	0.212	0.131	31.7	0.249	8.3	-0.211	0.139	-31.5	0.248
184.0	525.0	1.0	7.378	5.727	37.8	9.344	45.5	7.434	0.213	0.156	36.6	0.261	8.6	-0.213	0.164	-36.4	0.260
183.0	525.0	1.0	7.872	6.036	37.5	9.919	45.7	7.894	0.209	0.184	41.4	0.278	8.9	-0.208	0.182	-41.3	0.277
182.0	525.0	1.0	8.404	6.366	37.1	11.543	46.0	8.390	0.204	0.215	46.5	0.296	9.3	-0.203	0.213	-46.5	0.295
181.0	525.0	1.0	8.985	6.719	36.8	12.219	46.3	8.916	0.206	0.249	51.4	0.315	9.8	-0.205	0.247	-51.4	0.314
180.0	525.0	1.0	9.620	7.097	36.4	13.053	46.6	9.513	0.185	0.287	57.2	0.342	9.8	-0.183	0.286	-57.3	0.339
179.0	525.0	1.0	10.310	7.500	36.0	14.039	46.7	10.150	0.170	0.329	63.7	0.367	10.0	-0.168	0.327	-63.7	0.363
178.0	525.0	1.0	11.079	7.936	35.6	15.268	46.7	10.845	0.150	0.375	68.2	0.404	10.1	-0.146	0.373	-68.6	0.401
177.0	525.0	1.0	11.918	8.400	35.2	16.581	46.8	11.603	0.125	0.425	73.6	0.443	10.2	-0.118	0.423	-74.4	0.439
176.0	525.0	1.0	12.826	8.894	34.7	18.024	46.9	12.432	0.094	0.480	78.9	0.482	10.3	-0.082	0.478	-80.3	0.477
175.0	525.0	1.0	13.863	9.427	34.2	19.675	46.8	13.341	0.065	0.539	83.1	0.543	10.4	-0.036	0.537	-86.2	0.538
174.0	525.0	1.0	15.039	9.995	33.7	21.558	46.7	14.347	0.037	0.607	86.7	0.607	10.4	-0.022	0.601	-92.1	0.607
173.0	525.0	1.0	16.240	10.601	33.1	23.694	46.5	15.434	0.120	0.672	79.9	0.683	10.4	0.094	0.670	82.0	0.676
172.0	525.0	1.0	17.477	11.248	32.5	26.010	46.2	16.640	0.204	0.745	70.7	0.773	10.4	0.163	0.743	74.1	0.772
171.0	525.0	1.0	18.749	11.937	31.9	28.582	45.7	17.970	0.313	0.823	69.2	0.860	10.0	0.298	0.820	70.9	0.862
170.0	525.0	1.0	20.086	12.669	31.2	31.428	45.2	19.439	0.450	0.904	63.5	1.009	10.2	0.433	0.900	64.3	0.999
169.0	525.0	1.0	21.486	13.456	30.4	34.564	44.5	21.044	0.647	0.987	57.4	1.164	10.3	0.683	0.983	60.3	1.163
168.0	525.0	1.0	24.939	14.267	29.8	38.732	43.7	22.864	0.935	1.071	52.4	1.352	9.8	0.807	1.067	52.9	1.338
167.0	525.0	1.0	27.329	15.123	29.2	43.039	42.8	24.817	1.276	1.155	47.9	1.557	9.1	1.057	1.149	47.4	1.552
166.0	525.0	1.0	30.000	16.042	28.1	48.464	41.5	27.072	1.381	1.236	41.8	1.853	9.1	1.358	1.231	42.2	1.833
165.0	525.0	1.0	32.886	16.993	27.3	53.010	40.2	29.528	1.747	1.311	36.9	2.184	8.6	1.721	1.306	37.2	2.160
164.0	525.0	1.0	36.016	17.982	26.6	58.524	38.7	32.248	2.183	1.378	32.3	2.553	7.8	2.132	1.372	32.7	2.529
163.0	525.0	1.0	40.020	19.005	25.4	64.304	37.0	35.256	2.697	1.432	28.0	3.054	7.4	2.662	1.426	28.2	3.020
162.0	525.0	1.0	44.959	20.059	24.1	70.464	35.4	38.567	3.411	1.464	24.1	3.654	6.7	3.411	1.464	24.2	3.627
161.0	525.0	1.0	48.414	21.136	23.5	76.910	33.2	42.184	3.980	1.490	20.5	4.250	6.0	3.930	1.482	20.7	4.200
160.0	525.0	1.0	53.483	22.231	22.6	83.519	31.0	46.090	4.743	1.487	17.4	4.970	5.3	4.681	1.478	17.5	4.909
159.0	525.0	1.0	58.658	23.337	21.7	91.330	28.8	50.327	5.862	1.459	14.7	5.750	4.7	5.475	1.447	14.8	5.675
158.0	525.0	1.0	64.011	24.450	20.9	98.522	26.9	54.928	6.402	1.406	12.4	6.594	4.0	6.311	1.398	12.5	6.463
157.0	525.0	1.0	69.543	25.583	20.3	107.203	25.0	59.903	7.203	1.329	10.3	7.595	3.5	7.203	1.329	10.3	7.595
156.0	525.0	1.0	74.367	26.744	19.7	116.006	21.8	62.871	7.890	1.233	8.9	7.986	2.9	7.764	1.234	9.0	7.860
155.0	525.0	1.0	78.771	27.984	19.4	124.527	19.4	66.469	8.378	1.123	7.6	8.452	2.4	8.237	1.113	7.7	8.312
154.0	525.0	1.0	82.846	28.894	19.1	133.173	17.2	69.370	8.903	1.003	6.7	8.952	2.0	8.445	0.992	6.7	8.502
153.0	525.0	1.0															

EMF-OHL-2001

Electric & Magnetic Field Study Report
Kintore Tealing 400kV

Applies to

Distribution

Transmission



Revision: 1.00

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Issue Date: July 25

70.0	525.0	1.0	72.576	47.274	33.1	86.615	4.8	68.926	1.096	2.667	67.7	2.883	19.2	-0.760	-2.604	73.7	2.713
69.0	525.0	1.0	72.079	49.641	34.6	87.520	5.5	69.646	1.712	3.327	62.8	3.741	10.1	-1.525	-3.259	64.9	3.599
68.0	525.0	1.0	71.726	52.084	36.0	88.642	6.5	70.539	2.390	4.041	59.4	4.695	5.6	-2.261	-3.966	60.3	4.565
67.0	525.0	1.0	71.401	54.492	37.4	89.819	7.8	71.476	3.062	4.781	57.4	5.478	3.3	-2.961	-4.696	57.8	5.552
66.0	525.0	1.0	70.956	56.709	38.6	90.833	9.3	72.283	3.695	5.506	56.1	6.631	2.2	-3.607	-5.408	56.3	6.501
65.0	525.0	1.0	70.738	58.532	39.8	91.414	11.0	72.745	4.257	6.152	55.3	7.481	1.8	-4.233	-6.041	55.7	7.344
64.0	525.0	1.0	69.016	59.737	40.9	91.278	13.0	72.636	4.714	6.650	54.7	8.151	1.8	-4.635	-6.527	54.6	8.005
63.0	525.0	1.0	67.220	60.122	41.9	90.194	15.1	72.766	5.033	6.930	54.0	8.565	1.9	-4.957	-6.800	53.9	8.415
62.0	525.0	1.0	64.785	59.565	42.6	88.006	17.4	70.033	5.193	6.950	53.2	8.676	2.1	-5.122	-6.818	53.1	8.528
61.0	525.0	1.0	61.767	58.063	43.2	84.773	19.7	67.460	5.193	6.704	52.2	8.480	2.5	-5.129	-6.577	52.1	8.340
60.0	525.0	1.0	58.335	55.738	43.7	80.668	21.3	64.193	5.050	6.236	51.0	8.717	3.1	-4.650	-6.110	50.7	7.892
59.0	525.0	1.0	54.623	52.797	44.0	75.969	24.6	60.454	4.796	5.584	49.3	7.361	3.6	-4.750	-5.480	49.1	7.253
58.0	525.0	1.0	50.864	49.478	44.2	70.974	27.9	56.469	4.469	4.851	47.6	6.256	4.2	-4.429	-4.761	47.0	6.501
57.0	525.0	1.0	47.253	45.998	44.2	65.944	29.4	52.477	4.104	4.096	44.9	5.798	4.8	-4.075	-4.019	44.6	5.724
56.0	525.0	1.0	43.831	42.528	44.1	61.072	31.8	48.599	3.728	3.369	42.1	5.025	5.6	-3.706	-3.304	41.7	4.964
55.0	525.0	1.0	40.474	39.187	43.9	56.806	33.8	44.945	3.360	2.705	38.8	4.313	6.4	-3.243	-2.648	38.4	4.264
54.0	525.0	1.0	37.803	36.048	43.6	52.235	35.8	41.567	3.012	2.119	35.1	3.682	7.1	-2.998	-2.068	34.6	3.642
53.0	525.0	1.0	35.214	33.149	43.3	48.362	37.7	38.686	2.689	1.616	31.0	3.137	7.9	-2.678	-1.570	30.4	3.104
52.0	525.0	1.0	32.894	30.506	42.8	44.863	39.4	35.700	2.395	1.194	26.5	2.676	8.5	-2.386	-1.151	25.7	2.649
51.0	525.0	1.0	30.829	28.148	42.4	40.720	40.9	32.650	2.129	0.844	21.9	2.207	9.1	-2.121	-0.803	20.7	2.206
50.0	525.0	1.0	28.973	25.974	41.9	38.911	42.2	30.965	1.890	0.585	16.6	1.973	9.6	-1.884	-0.520	15.4	1.955
49.0	525.0	1.0	27.330	24.060	41.4	36.412	43.3	28.975	1.677	0.345	11.6	1.713	10.0	-1.672	-0.291	9.9	1.697
48.0	525.0	1.0	25.844	21.380	40.8	34.021	44.1	26.195	1.488	0.191	7.3	1.500	10.2	-1.484	-0.107	4.1	1.488
47.0	525.0	1.0	24.580	20.856	40.3	32.236	45.1	25.653	1.320	0.140	6.1	1.327	10.3	-1.316	0.040	-1.7	1.317
46.0	525.0	1.0	23.448	19.532	39.8	30.514	45.7	24.282	1.173	0.184	5.4	1.187	10.3	-1.148	0.156	6.4	1.179
45.0	525.0	1.0	22.448	18.373	39.3	29.008	46.2	23.084	1.040	0.267	14.4	1.073	10.2	-1.037	0.248	-13.4	1.066
44.0	525.0	1.0	21.584	17.364	38.8	27.702	46.8	22.044	0.924	0.332	19.8	0.981	10.0	-0.921	0.320	-19.2	0.975
43.0	525.0	1.0	20.844	16.493	38.4	26.580	46.9	21.152	0.821	0.386	25.2	0.907	9.8	-0.819	0.379	-24.8	0.902
42.0	525.0	1.0	20.221	15.749	37.9	25.630	47.1	20.396	0.730	0.431	30.6	0.848	9.6	-0.728	0.426	-30.3	0.844
41.0	525.0	1.0	19.711	15.121	37.3	24.843	47.2	19.769	0.649	0.469	35.8	0.801	9.3	-0.647	0.466	-35.7	0.797
40.0	525.0	1.0	19.310	14.601	37.1	24.208	47.3	19.264	0.577	0.502	41.0	0.764	9.1	-0.575	0.499	-41.0	0.762
39.0	525.0	1.0	19.015	14.182	36.7	23.721	47.4	18.877	0.512	0.531	46.1	0.738	8.9	-0.510	0.520	-46.1	0.735
38.0	525.0	1.0	18.807	13.857	36.4	23.372	47.5	18.603	0.452	0.560	51.2	0.719	8.7	-0.450	0.559	-51.2	0.717
37.0	525.0	1.0	18.745	13.622	36.0	23.171	47.5	18.439	0.397	0.588	55.9	0.709	8.6	-0.394	0.587	-56.1	0.705
36.0	525.0	1.0	18.709	13.470	35.7	23.010	47.6	18.288	0.345	0.617	60.8	0.707	8.4	-0.342	0.616	-61.0	0.705
35.0	525.0	1.0	18.694	13.399	35.3	23.171	47.6	18.439	0.294	0.648	65.6	0.711	8.5	-0.289	0.648	-65.9	0.710
34.0	525.0	1.0	18.694	13.399	35.3	23.171	47.6	18.439	0.244	0.682	70.4	0.722	8.7	-0.244	0.682	-70.4	0.722
33.0	525.0	1.0	19.518	13.483	34.6	23.722	47.6	18.877	0.192	0.719	75.0	0.744	8.7	-0.193	0.719	-75.0	0.742
32.0	525.0	1.0	20.007	13.634	34.3	24.211	47.6	19.267	0.140	0.760	79.6	0.773	8.8	-0.142	0.760	-79.6	0.770
31.0	525.0	1.0	20.564	13.854	33.9	24.745	47.5	19.638	0.086	0.805	83.4	0.811	9.0	-0.086	0.805	-83.4	0.808
30.0	525.0	1.0	21.391	14.143	33.5	25.643	47.4	20.406	0.081	0.856	84.6	0.860	9.2	-0.016	0.856	-84.6	0.856
29.0	525.0	1.0	22.406	14.498	32.9	26.580	47.3	21.205	0.135	0.911	87.1	0.911	9.4	0.102	0.911	83.6	0.917
28.0	525.0	1.0	23.383	14.918	32.5	27.736	47.0	22.072	0.226	0.971	76.9	0.997	9.7	0.203	0.971	78.2	0.992
27.0	525.0	1.0	24.640	15.402	32.0	29.008	46.7	23.124	0.343	1.035	71.7	1.091	9.9	0.324	1.024	72.6	1.084
26.0	525.0	1.0	25.498	15.949	31.4	30.584	46.2	24.388	0.466	1.103	66.2	1.206	10.0	0.450	1.102	66.5	1.197
25.0	525.0	1.0	27.768	16.558	30.8	32.330	45.6	25.707	0.680	1.174	60.6	1.347	10.0	0.643	1.172	61.2	1.337
24.0	525.0	1.0	29.440	17.227	30.1	34.317	44.6	27.143	0.971	1.246	55.3	1.530	10.0	0.853	1.243	55.5	1.508
23.0	525.0	1.0	31.858	17.954	29.4	36.569	43.9	29.101	1.125	1.317	49.5	1.732	9.8	1.106	1.314	49.9	1.718
22.0	525.0	1.0	34.061	18.743	28.7	39.077	43.1	31.287	1.401	1.387	43.1	1.983	9.5	1.410	1.383	44.4	1.975
21.0	525.0	1.0	37.121	19.571	27.8	41.964	41.5	33.394	1.798	1.451	38.9	2.310	9.0	1.773	1.446	39.2	2.288
20.0	525.0	1.0	40.264	20.452	26.9	45.160	40.0	35.937	2.234	1.506	34.0	2.694	8.5	2.206	1.501	34.2	2.668
19.0	525.0	1.0	43.781	21.377	26.0	48.721	38.4	38.713	2.748	1.550	29.4	3.155	7.8	2.714	1.544	29.7	3.123
18.0	525.0	1.0	47.690	22.338	25.1	52.662	36.5	41.907	3.346	1.578	25.3	3.699	7.1	3.305	1.572	25.4	3.660
17.0	525.0	1.0	51.949	23.429	24.2	56.984	34.5	45.246	4.028	1.588	20.8	4.260	6.4	3.979	1.580	21.0	4.226
16.0	525.0	1.0	56.650	24.344	23.3	61.459	32.3	49.087	4.788	1.574	18.2	5.040	5.8	4.727	1.566	18.3	4.980
15.0	525.0	1.0	61.601	25.375	22.4	66.623	30.1	53.017	5.605	1.537	15.3	5.812	4.9	5.531	1.528	15.4	5.738
14.0	525.0	1.0	66.709	26.416	21.6	71.749	27.7	57.086	6.442	1.470	12.6	6.609	4.2	6.389	1.462	12.7	6.519
13.0	525.0	1.0	71.768	27.462	20.9	76.843	25.3	61.149	7.241	1.390	10.9	7.373	3.6	7.133	1.381	11.0	7.266
12.0	525.0	1.0	77.401	28.511	20.1	81.904	22.8	65.124	8.025	1.287	9.2	8.008	3.0	7.907	1.275	9.3	7.840
11.0	525.0	1.0	80.587	29.561	20.1	85.838	20.4	68.307	8.411	1.170	7.9	8.492	2.5	8.271	1.160	8.0	8.352
10.0	525.0	1.0	84.14	30.614	20.1	89.819	18.0	71.444	8.749	1.044	6.9	9.038	1.9	8.619	1.033	6.9	8.589
9.0	525.0	1.0	85.733	31.678	20.3	91.398	15.7	72.732	8.529	0.933	6.1	8.577	1.9	8.379	0.939	6.1	8.427
8.0	52																

Revision: 1.00

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-77.0	525.0	1.0	1.716	0.743	23.4	1.870	34.0	1.488	0.092	0.025	15.5	0.095	1.5	0.092	0.025	15.4	0.095
-78.0	525.0	1.0	1.664	0.714	23.2	1.811	33.7	1.441	0.090	0.024	14.6	0.093	1.5	0.090	0.024	14.6	0.093
-79.0	525.0	1.0	1.615	0.684	23.0	1.755	33.4	1.396	0.089	0.022	13.8	0.091	1.4	0.089	0.022	13.8	0.091
-80.0	525.0	1.0	1.568	0.660	22.8	1.701	33.2	1.353	0.087	0.020	13.0	0.090	1.4	0.087	0.020	13.0	0.090
-81.0	525.0	1.0	1.522	0.635	22.6	1.649	32.9	1.312	0.086	0.019	12.2	0.088	1.4	0.086	0.019	12.2	0.088
-82.0	525.0	1.0	1.479	0.611	22.4	1.600	32.6	1.273	0.084	0.017	11.4	0.086	1.3	0.084	0.017	11.4	0.086
-83.0	525.0	1.0	1.437	0.588	22.3	1.553	32.3	1.236	0.083	0.016	10.7	0.084	1.3	0.083	0.016	10.7	0.084
-84.0	525.0	1.0	1.397	0.566	22.1	1.508	32.0	1.200	0.081	0.014	10.0	0.083	1.3	0.081	0.014	9.9	0.083
-85.0	525.0	1.0	1.359	0.546	21.9	1.464	31.8	1.165	0.080	0.013	9.3	0.081	1.2	0.080	0.013	9.2	0.081
-86.0	525.0	1.0	1.322	0.524	21.7	1.423	31.5	1.132	0.078	0.012	8.6	0.079	1.2	0.078	0.012	8.5	0.079
-87.0	525.0	1.0	1.286	0.507	21.5	1.383	31.2	1.100	0.077	0.011	7.9	0.078	1.2	0.077	0.011	7.9	0.078
-88.0	525.0	1.0	1.252	0.489	21.3	1.344	30.9	1.070	0.076	0.010	7.2	0.076	1.1	0.076	0.010	7.2	0.076
-89.0	525.0	1.0	1.219	0.472	21.1	1.308	30.7	1.040	0.075	0.009	6.6	0.075	1.1	0.074	0.009	6.6	0.075
-90.0	525.0	1.0	1.188	0.456	21.0	1.272	30.4	1.012	0.073	0.008	6.0	0.073	1.1	0.073	0.008	5.9	0.073
-91.0	525.0	1.0	1.157	0.440	20.8	1.238	30.1	0.987	0.072	0.007	5.4	0.072	1.1	0.072	0.007	5.3	0.072
-92.0	525.0	1.0	1.128	0.425	20.6	1.205	29.9	0.959	0.070	0.006	4.8	0.071	1.0	0.070	0.006	4.7	0.071
-93.0	525.0	1.0	1.100	0.410	20.5	1.174	29.6	0.934	0.069	0.005	4.2	0.069	1.0	0.069	0.005	4.2	0.069
-94.0	525.0	1.0	1.073	0.396	20.3	1.144	29.3	0.910	0.068	0.004	3.6	0.068	1.0	0.068	0.004	3.6	0.068
-95.0	525.0	1.0	1.046	0.383	20.1	1.114	29.1	0.887	0.067	0.004	3.1	0.067	1.0	0.067	0.004	3.0	0.067
-96.0	525.0	1.0	1.021	0.371	19.9	1.084	28.8	0.865	0.066	0.003	2.5	0.066	0.9	0.066	0.003	2.5	0.066
-97.0	525.0	1.0	0.997	0.358	19.8	1.059	28.5	0.843	0.064	0.003	2.0	0.065	0.9	0.064	0.003	1.9	0.065
-98.0	525.0	1.0	0.973	0.347	19.6	1.033	28.3	0.822	0.063	0.002	1.5	0.063	0.9	0.063	0.002	1.4	0.063
-99.0	525.0	1.0	0.951	0.336	19.4	1.008	28.0	0.801	0.062	0.002	1.0	0.062	0.9	0.062	0.001	0.9	0.062
-100.0	525.0	1.0	0.914	0.325	19.4	0.970	28.4	0.772	0.059	0.002	1.5	0.059	0.9	0.059	0.002	1.5	0.059
-101.0	525.0	1.0	0.893	0.315	19.4	0.947	28.2	0.753	0.058	0.001	1.1	0.058	0.9	0.058	0.001	1.0	0.058
-102.0	525.0	1.0	0.872	0.305	19.3	0.924	27.9	0.735	0.057	0.001	0.7	0.057	0.8	0.057	0.000	0.5	0.057
-103.0	525.0	1.0	0.852	0.295	19.1	0.902	27.7	0.718	0.056	0.000	0.5	0.056	0.8	0.056	-0.000	-0.5	0.056
-104.0	525.0	1.0	0.833	0.286	19.0	0.881	27.4	0.703	0.055	0.001	0.7	0.055	0.8	0.055	-0.000	-0.5	0.055
-105.0	525.0	1.0	0.815	0.277	18.8	0.861	27.2	0.685	0.054	0.001	1.0	0.054	0.8	0.054	-0.001	-0.9	0.054
-106.0	525.0	1.0	0.797	0.269	18.6	0.841	26.9	0.669	0.053	0.001	1.5	0.053	0.8	0.053	-0.001	-1.4	0.053
-107.0	525.0	1.0	0.779	0.260	18.5	0.822	26.7	0.654	0.052	0.002	1.9	0.052	0.8	0.052	-0.002	-1.8	0.052
-108.0	525.0	1.0	0.762	0.253	18.3	0.803	26.4	0.639	0.051	0.002	2.3	0.051	0.8	0.051	-0.002	-2.3	0.051
-109.0	525.0	1.0	0.746	0.245	18.2	0.785	26.2	0.625	0.050	0.002	2.7	0.051	0.7	0.050	-0.002	-2.7	0.051
-110.0	525.0	1.0	0.730	0.238	18.0	0.768	25.9	0.611	0.050	0.003	3.1	0.050	0.7	0.050	-0.003	-3.1	0.050
-111.0	525.0	1.0	0.715	0.231	17.9	0.751	25.7	0.597	0.049	0.003	3.5	0.049	0.7	0.049	-0.003	-3.5	0.049
-112.0	525.0	1.0	0.700	0.224	17.7	0.735	25.5	0.585	0.048	0.003	4.0	0.048	0.7	0.048	-0.003	-3.9	0.048
-113.0	525.0	1.0	0.686	0.217	17.6	0.719	25.3	0.573	0.047	0.004	4.4	0.047	0.7	0.047	-0.004	-4.4	0.047
-114.0	525.0	1.0	0.672	0.211	17.4	0.704	25.0	0.560	0.046	0.004	4.7	0.046	0.7	0.046	-0.004	-4.7	0.046
-115.0	525.0	1.0	0.658	0.205	17.3	0.689	24.7	0.549	0.045	0.004	5.1	0.046	0.7	0.046	-0.004	-5.1	0.046
-116.0	525.0	1.0	0.645	0.199	17.2	0.675	24.5	0.537	0.044	0.004	5.4	0.045	0.7	0.045	-0.004	-5.4	0.045
-117.0	525.0	1.0	0.632	0.194	17.0	0.661	24.3	0.526	0.044	0.005	5.9	0.044	0.7	0.044	-0.005	-5.9	0.044
-118.0	525.0	1.0	0.620	0.188	16.8	0.648	24.0	0.515	0.043	0.005	6.3	0.044	0.6	0.043	-0.005	-6.3	0.044
-119.0	525.0	1.0	0.608	0.183	16.7	0.635	23.8	0.505	0.043	0.005	6.6	0.043	0.6	0.043	-0.005	-6.6	0.043
-120.0	525.0	1.0	0.596	0.178	16.6	0.622	23.5	0.495	0.042	0.005	7.0	0.042	0.6	0.042	-0.005	-7.0	0.042
-121.0	525.0	1.0	0.585	0.173	16.5	0.610	23.3	0.485	0.041	0.005	7.3	0.041	0.6	0.041	-0.005	-7.3	0.041
-122.0	525.0	1.0	0.574	0.168	16.3	0.598	23.1	0.476	0.041	0.005	7.7	0.041	0.6	0.041	-0.005	-7.7	0.041
-123.0	525.0	1.0	0.563	0.164	16.2	0.586	22.8	0.466	0.040	0.006	8.0	0.040	0.6	0.040	-0.006	-8.0	0.040
-124.0	525.0	1.0	0.552	0.159	16.1	0.575	22.6	0.457	0.039	0.006	8.4	0.040	0.6	0.039	-0.006	-8.4	0.040
-125.0	525.0	1.0	0.542	0.155	16.0	0.564	22.4	0.449	0.039	0.006	8.7	0.039	0.6	0.039	-0.006	-8.7	0.039
-126.0	525.0	1.0	0.532	0.151	15.8	0.553	22.2	0.440	0.038	0.006	9.0	0.038	0.6	0.038	-0.006	-9.0	0.038
-127.0	525.0	1.0	0.523	0.147	15.7	0.543	21.9	0.432	0.037	0.006	9.3	0.038	0.6	0.037	-0.006	-9.3	0.038
-128.0	525.0	1.0	0.513	0.143	15.5	0.533	21.7	0.424	0.037	0.006	9.7	0.037	0.6	0.037	-0.006	-9.7	0.037
-129.0	525.0	1.0	0.504	0.139	15.4	0.523	21.5	0.416	0.036	0.006	10.0	0.037	0.5	0.036	-0.006	-10.0	0.037
-130.0	525.0	1.0	0.495	0.135	15.3	0.513	21.3	0.408	0.036	0.006	10.3	0.036	0.5	0.036	-0.006	-10.3	0.036
-131.0	525.0	1.0	0.487	0.132	15.2	0.504	21.1	0.401	0.035	0.007	10.6	0.036	0.5	0.035	-0.007	-10.6	0.036
-132.0	525.0	1.0	0.478	0.128	15.0	0.495	20.8	0.394	0.035	0.007	10.9	0.035	0.5	0.035	-0.007	-10.9	0.035
-133.0	525.0	1.0	0.469	0.125	14.9	0.486	20.6	0.387	0.034	0.007	11.2	0.035	0.5	0.034	-0.007	-11.2	0.035
-134.0	525.0	1.0	0.462	0.122	14.8	0.478	20.3	0.380	0.034	0.007	11.5	0.034	0.5	0.034	-0.007	-11.5	0.034
-135.0	525.0	1.0	0.454	0.119	14.7	0.469	20.1	0.373	0.033	0.007	11.8	0.033	0.5	0.033	-0.007	-11.8	0.033
-136.0	525.0	1.0	0.446	0.116	14.6	0.461	19.9	0.367	0.033	0.007	12.0	0.033	0.5	0.033	-0.007	-12.0	0.033
-137.0	525.0	1.0	0.439	0.113													

EMF-OHL-001	Electric & Magnetic Field Study Report Kintore Tealing 400kV		Applies to	
			Distribution	Transmission ✓
Revision: 1.00	Classification: Public	Issue Date: July 25		

Optimal Phasing of Adjacent Circuits

PLS-CADD Version 20.01x64 13:59:08 02 July 2025

Scottish and Southern Energy

Project Name: 'C:\PLS\Combined_EMF_Check Temp\Combined_EMF_Check.don'

Line Title: 'Max Op'

3D EMF Calculation Notes:

1) Calculations based on the EPRI Red Book methods (3rd Edition, 2005 - 7.4 Calculation of Magnetic Fields and Appendices 7.1 Calculation of Field Ellipse Parameters and 7.6 Electric Field Calculations for 3D Geometry).

2) All wire positions are modeled at the specified weather case and wind direction. Height above ground determined by the modeled ground TTN.

3) Only the effects of wires are being analyzed. The effects of structures are not included unless enabled as noted below.

4) Ground return is being ignored for magnetic field calculations.

Meter height above ground: 1.00 (m)

Maximum wire distance: 300.00 (m)

Maximum cable segment size: 1.00 (m)

Cross section offset +/-: 300.00 (m)

Result interval: 1.00 (m)

Electric field limit: 5.00 (kV/m)

Magnetic field limit: 380.00 (uT)

Space potential limit: 0.00 (kV)

Contour Map Spacing: 3 (m)

Analyzing spans between these structures: 6 - 7

One or more sections have wind from both directions which is not supported. A wind direction of left is being used for those sections.

Section Data for 3D EMF Results:

Section Number	Section Note	Section Voltage (kV)	Current (Amps)	File Name	Description	Conductors Per Phase	Bundle Diameter (cm)	Cable Radius (cm)	Weather Case	Condition	Wind Dir.	Temp. (deg C)	WC Effective Radius (cm)
1		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
2		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
3		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
4		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
5		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
6		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
7		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
8		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
9		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
10		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
11		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
12		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
13		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
14		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
15		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
16		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
17		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700
18		400.0	5000.0	700mm aaac araucaria.wir 700mm ³ AAAC - Araucaria (R)		3	57.735	1.863	Max Op	Creep FE Left		90.000	16.700

Wire low point cross section results between structures 6 and 7

Magnetic Field vs. offset relative to line between structures 175 (m) ahead of structure 6

Electric Field vs. offset relative to line between structures 175 (m) ahead of structure 6



Revision: 1.00

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3D EMF Point Results Span from 6 to 7:

Measurement				B				H				EF				Space Potential							
X	Y	Z	I	Real Imaginary	Angle	Magnitude	Polarization	X	Y	Z	I	Real Imaginary	Angle	Magnitude	Polarization	X	Y	Z	I	Real Imaginary	Angle	Magnitude	Polarization
(m)	(m)	(m)	(A)	(V/m)	(deg)	(V/m)	(A/m)	(m)	(m)	(m)	(A)	(V/m)	(deg)	(V/m)	(A/m)	(m)	(m)	(m)	(A)	(V)	(deg)	(V)	(V)
372.0	525.0	1.0	0.052	0.066	51.7	0.084	7.5	0.067	0.002	0.008	78.2	0.008	0.2	-0.002	-0.008	78.2	0.008	0.009	0.009	-0.002	-0.009	78.2	0.008
371.0	525.0	1.0	0.023	0.062	69.6	0.066	12.7	0.053	0.001	0.009	86.2	0.009	0.2	0.001	-0.009	86.2	0.009	0.009	0.009	0.001	-0.009	86.2	0.009
370.0	525.0	1.0	0.023	0.063	69.5	0.067	12.9	0.053	0.001	0.009	86.3	0.009	0.2	0.001	-0.009	86.3	0.009	0.009	0.009	0.001	-0.009	86.3	0.009
369.0	525.0	1.0	0.024	0.064	69.5	0.068	13.1	0.054	0.001	0.009	86.4	0.009	0.2	0.001	-0.009	86.4	0.009	0.009	0.009	0.001	-0.009	86.4	0.009
368.0	525.0	1.0	0.024	0.064	69.5	0.069	13.3	0.055	0.001	0.009	86.5	0.009	0.2	0.001	-0.009	86.5	0.009	0.009	0.009	0.001	-0.009	86.5	0.009
367.0	525.0	1.0	0.024	0.064	69.4	0.069	13.4	0.055	0.001	0.009	86.5	0.009	0.2	0.001	-0.009	86.5	0.009	0.009	0.009	0.001	-0.009	86.5	0.009
366.0	525.0	1.0	0.025	0.066	69.4	0.070	13.8	0.056	0.001	0.009	86.7	0.009	0.2	0.001	-0.009	86.7	0.009	0.009	0.009	0.001	-0.009	86.7	0.009
365.0	525.0	1.0	0.025	0.066	69.4	0.071	14.0	0.057	0.001	0.009	86.8	0.009	0.2	0.001	-0.009	86.8	0.009	0.009	0.009	0.001	-0.009	86.8	0.009
364.0	525.0	1.0	0.025	0.067	69.3	0.072	14.2	0.057	0.000	0.009	86.9	0.009	0.2	0.000	-0.009	86.9	0.009	0.009	0.009	0.000	-0.009	86.9	0.009
363.0	525.0	1.0	0.026	0.068	69.3	0.073	14.4	0.058	0.000	0.009	87.0	0.009	0.2	0.000	-0.009	87.0	0.009	0.009	0.009	0.000	-0.009	87.0	0.009
362.0	525.0	1.0	0.026	0.069	69.2	0.074	14.6	0.059	0.000	0.009	87.1	0.009	0.2	0.000	-0.009	87.1	0.009	0.009	0.009	0.000	-0.009	87.1	0.009
361.0	525.0	1.0	0.026	0.070	69.2	0.074	14.9	0.059	0.000	0.010	87.2	0.010	0.2	0.000	-0.010	87.2	0.010	0.009	0.009	0.000	-0.010	87.2	0.010
360.0	525.0	1.0	0.027	0.070	69.1	0.075	15.1	0.060	0.000	0.010	87.3	0.010	0.2	0.000	-0.010	87.3	0.010	0.009	0.009	0.000	-0.010	87.3	0.010
359.0	525.0	1.0	0.027	0.071	69.1	0.076	15.3	0.061	0.000	0.010	87.5	0.010	0.2	0.000	-0.010	87.5	0.010	0.009	0.009	0.000	-0.010	87.5	0.010
358.0	525.0	1.0	0.028	0.072	69.0	0.077	15.5	0.061	0.000	0.010	87.6	0.010	0.2	0.000	-0.010	87.6	0.010	0.009	0.009	0.000	-0.010	87.6	0.010
357.0	525.0	1.0	0.028	0.073	69.0	0.078	15.7	0.062	0.000	0.010	87.7	0.010	0.2	0.000	-0.010	87.7	0.010	0.009	0.009	0.000	-0.010	87.7	0.010
356.0	525.0	1.0	0.028	0.074	68.9	0.078	16.0	0.063	0.000	0.010	87.8	0.010	0.2	0.000	-0.010	87.8	0.010	0.009	0.009	0.000	-0.010	87.8	0.010
355.0	525.0	1.0	0.029	0.075	68.9	0.080	16.2	0.064	0.000	0.010	87.9	0.010	0.2	0.000	-0.010	87.9	0.010	0.009	0.009	0.000	-0.010	87.9	0.010
354.0	525.0	1.0	0.029	0.076	68.8	0.081	16.4	0.065	0.000	0.010	88.0	0.010	0.2	0.000	-0.010	88.0	0.010	0.009	0.009	0.000	-0.010	88.0	0.010
353.0	525.0	1.0	0.030	0.076	68.8	0.082	16.7	0.065	0.000	0.010	88.2	0.010	0.2	0.000	-0.010	88.2	0.010	0.009	0.009	0.000	-0.010	88.2	0.010
352.0	525.0	1.0	0.030	0.077	68.7	0.083	16.9	0.066	0.000	0.010	88.3	0.010	0.2	0.000	-0.010	88.3	0.010	0.009	0.009	0.000	-0.010	88.3	0.010
351.0	525.0	1.0	0.031	0.078	68.6	0.084	17.1	0.067	0.000	0.010	88.4	0.010	0.2	0.000	-0.010	88.4	0.010	0.009	0.009	0.000	-0.010	88.4	0.010
350.0	525.0	1.0	0.031	0.079	68.6	0.085	17.3	0.068	0.000	0.011	88.5	0.011	0.2	0.000	-0.011	88.5	0.011	0.009	0.009	0.000	-0.011	88.5	0.011
349.0	525.0	1.0	0.032	0.080	68.5	0.086	17.6	0.069	0.000	0.011	88.6	0.011	0.2	0.000	-0.011	88.6	0.011	0.009	0.009	0.000	-0.011	88.6	0.011
348.0	525.0	1.0	0.032	0.081	68.5	0.087	17.8	0.070	0.000	0.011	88.8	0.011	0.2	0.000	-0.011	88.8	0.011	0.009	0.009	0.000	-0.011	88.8	0.011
347.0	525.0	1.0	0.033	0.082	68.4	0.089	18.0	0.070	0.000	0.011	88.9	0.011	0.2	0.000	-0.011	88.9	0.011	0.009	0.009	0.000	-0.011	88.9	0.011
346.0	525.0	1.0	0.033	0.083	68.3	0.090	18.3	0.071	0.000	0.011	89.0	0.011	0.2	0.000	-0.011	89.0	0.011	0.009	0.009	0.000	-0.011	89.0	0.011
345.0	525.0	1.0	0.034	0.084	68.2	0.091	18.5	0.072	0.000	0.011	89.2	0.011	0.2	0.000	-0.011	89.2	0.011	0.009	0.009	0.000	-0.011	89.2	0.011
344.0	525.0	1.0	0.034	0.086	68.2	0.092	18.7	0.073	0.000	0.011	89.3	0.011	0.2	0.000	-0.011	89.3	0.011	0.009	0.009	0.000	-0.011	89.3	0.011
343.0	525.0	1.0	0.035	0.087	68.1	0.093	18.9	0.074	0.000	0.011	89.4	0.011	0.2	0.000	-0.011	89.4	0.011	0.009	0.009	0.000	-0.011	89.4	0.011
342.0	525.0	1.0	0.035	0.088	68.0	0.094	19.2	0.075	0.000	0.011	89.5	0.011	0.2	0.000	-0.011	89.5	0.011	0.009	0.009	0.000	-0.011	89.5	0.011
341.0	525.0	1.0	0.036	0.089	68.0	0.096	19.4	0.076	0.000	0.012	89.7	0.012	0.2	0.000	-0.012	89.7	0.012	0.009	0.009	0.000	-0.012	89.7	0.012
340.0	525.0	1.0	0.037	0.090	67.9	0.097	19.7	0.077	0.000	0.012	89.8	0.012	0.2	0.000	-0.012	89.8	0.012	0.009	0.009	0.000	-0.012	89.8	0.012
339.0	525.0	1.0	0.037	0.091	67.8	0.099	19.9	0.078	0.000	0.012	89.9	0.012	0.2	0.000	-0.012	89.9	0.012	0.009	0.009	0.000	-0.012	89.9	0.012
338.0	525.0	1.0	0.038	0.092	67.7	0.100	20.1	0.079	0.000	0.012	90.0	0.012	0.2	0.000	-0.012	90.0	0.012	0.009	0.009	0.000	-0.012	90.0	0.012
337.0	525.0	1.0	0.039	0.094	67.6	0.101	20.4	0.081	0.000	0.012	90.2	0.012	0.3	-0.000	-0.012	90.2	0.012	0.009	0.009	0.000	-0.012	90.2	0.012
336.0	525.0	1.0	0.039	0.095	67.5	0.103	20.6	0.082	0.000	0.012	90.5	0.012	0.3	-0.000	-0.012	90.5	0.012	0.009	0.009	0.000	-0.012	90.5	0.012
335.0	525.0	1.0	0.040	0.096	67.4	0.104	20.8	0.083	0.000	0.012	90.7	0.012	0.3	-0.000	-0.012	90.7	0.012	0.009	0.009	0.000	-0.012	90.7	0.012
334.0	525.0	1.0	0.041	0.097	67.4	0.106	21.1	0.084	0.000	0.012	90.9	0.012	0.3	-0.000	-0.012	90.9	0.012	0.009	0.009	0.000	-0.012	90.9	0.012
333.0	525.0	1.0	0.041	0.099	67.3	0.107	21.3	0.085	0.000	0.013	91.1	0.013	0.3	-0.000	-0.013	91.1	0.013	0.009	0.009	0.000	-0.013	91.1	0.013
332.0	525.0	1.0	0.042	0.100	67.2	0.109	21.5	0.086	0.000	0.013	91.0	0.013	0.3	-0.000	-0.013	91.0	0.013	0.009	0.009	0.000	-0.013	91.0	0.013
331.0	525.0	1.0	0.042	0.101	67.1	0.110	21.8	0.087	0.000	0.013	91.2	0.013	0.3	-0.000	-0.013	91.2	0.013	0.009	0.009	0.000	-0.013	91.2	0.013
330.0	525.0	1.0	0.044	0.103	67.0	0.112	22.0	0.089	0.000	0.013	91.3	0.013	0.3	-0.000	-0.013	91.3	0.013	0.009	0.009	0.000	-0.013	91.3	0.013
329.0	525.0	1.0	0.044	0.104	66.9	0.113	22.2	0.090	0.000	0.013	91.5	0.013	0.3	-0.000	-0.013	91.5	0.013	0.009	0.009	0.000	-0.013	91.5	0.013
328.0	525.0	1.0	0.045	0.106	66.8	0.115	22.5	0.092	0.000	0.013	91.3	0.013	0.3	-0.000	-0.013	91.3	0.013	0.009	0.009	0.000	-0.013	91.3	0.013
327.0	525.0	1.0	0.046	0.107	66.7	0.117	22.7	0.093	0.000	0.013	91.1	0.013	0.3	-0.000	-0.013	91.1	0.013	0.009	0.009	0.000	-0.013	91.1	0.013
326.0	525.0	1.0	0.047	0.109																			

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217.0	525.0	1.0	1.105	1.284	49.3	1.694	43.4	1.348	0.062	0.058	43.3	0.085	2.2	-0.062	-0.058	43.3	0.085
216.0	525.0	1.0	1.104	1.330	49.1	1.761	43.6	1.401	0.064	0.058	42.1	0.087	2.2	-0.064	-0.058	42.1	0.086
215.0	525.0	1.0	1.105	1.378	48.9	1.830	43.8	1.457	0.067	0.058	40.8	0.091	2.3	-0.067	-0.058	40.8	0.088
214.0	525.0	1.0	1.109	1.428	48.6	1.904	44.0	1.515	0.070	0.058	39.5	0.091	2.4	-0.070	-0.058	39.5	0.090
213.0	525.0	1.0	1.117	1.481	48.4	1.982	44.2	1.577	0.073	0.057	38.1	0.093	2.5	-0.073	-0.057	38.1	0.093
212.0	525.0	1.0	1.128	1.537	48.1	2.064	44.4	1.642	0.076	0.057	36.7	0.095	2.5	-0.076	-0.057	36.6	0.095
211.0	525.0	1.0	1.142	1.595	47.9	2.151	44.6	1.711	0.079	0.056	35.2	0.097	2.6	-0.079	-0.056	35.2	0.097
210.0	525.0	1.0	1.161	1.657	47.6	2.242	44.8	1.784	0.083	0.055	33.6	0.099	2.7	-0.083	-0.055	33.6	0.099
209.0	525.0	1.0	1.183	1.722	47.4	2.339	45.0	1.861	0.086	0.054	32.1	0.102	2.8	-0.086	-0.054	32.0	0.102
208.0	525.0	1.0	1.180	1.790	47.2	2.442	45.1	1.943	0.090	0.053	30.4	0.104	3.0	-0.090	-0.053	30.4	0.104
207.0	525.0	1.0	1.182	1.863	46.9	2.550	45.3	2.029	0.094	0.051	28.7	0.107	3.1	-0.094	-0.051	28.7	0.107
206.0	525.0	1.0	1.829	1.939	46.7	2.665	45.5	2.121	0.098	0.050	26.9	0.110	3.2	-0.098	-0.050	26.9	0.110
205.0	525.0	1.0	1.921	2.018	46.4	2.787	45.7	2.217	0.102	0.048	25.1	0.113	3.3	-0.102	-0.048	25.0	0.112
204.0	525.0	1.0	2.020	2.104	46.2	2.917	45.9	2.321	0.106	0.045	23.1	0.116	3.5	-0.106	-0.045	23.0	0.115
203.0	525.0	1.0	2.125	2.194	45.9	3.054	46.1	2.431	0.111	0.043	21.1	0.118	3.6	-0.111	-0.043	21.0	0.118
202.0	525.0	1.0	2.237	2.289	45.7	3.201	46.3	2.547	0.115	0.040	19.0	0.122	3.8	-0.115	-0.040	18.9	0.122
201.0	525.0	1.0	2.357	2.390	45.4	3.357	46.5	2.671	0.120	0.036	16.8	0.125	4.0	-0.120	-0.036	16.7	0.125
200.0	525.0	1.0	2.485	2.497	45.1	3.523	46.7	2.803	0.125	0.032	14.5	0.129	4.2	-0.125	-0.032	14.3	0.129
199.0	525.0	1.0	2.622	2.610	44.9	3.699	46.9	2.944	0.130	0.028	12.2	0.133	4.4	-0.130	-0.027	11.9	0.132
198.0	525.0	1.0	2.769	2.730	44.6	3.888	47.1	3.094	0.135	0.023	9.7	0.137	4.6	-0.135	-0.022	9.3	0.136
197.0	525.0	1.0	2.926	2.858	44.3	4.090	47.3	3.255	0.140	0.018	7.2	0.141	4.8	-0.140	-0.016	6.6	0.141
196.0	525.0	1.0	3.095	2.993	44.0	4.305	47.5	3.426	0.145	0.012	4.8	0.145	5.1	-0.145	-0.010	3.8	0.145
195.0	525.0	1.0	3.276	3.138	43.8	4.536	47.7	3.606	0.150	0.008	2.2	0.150	5.3	-0.150	0.000	0.9	0.150
194.0	525.0	1.0	3.471	3.291	43.5	4.781	47.9	3.806	0.155	0.011	3.9	0.156	5.6	-0.155	0.006	-2.2	0.155
193.0	525.0	1.0	3.680	3.455	43.2	5.048	48.1	4.017	0.160	0.018	5.4	0.161	5.9	-0.160	0.015	-5.6	0.161
192.0	525.0	1.0	3.907	3.629	42.9	5.332	48.3	4.243	0.165	0.028	9.6	0.168	6.1	-0.165	0.026	-8.9	0.167
191.0	525.0	1.0	4.151	3.815	42.6	5.638	48.5	4.487	0.170	0.039	13.0	0.175	6.4	-0.170	0.038	-12.5	0.174
190.0	525.0	1.0	4.416	4.013	42.3	5.967	48.7	4.748	0.175	0.052	16.7	0.182	6.7	-0.174	0.051	-16.2	0.182
189.0	525.0	1.0	4.701	4.225	41.9	6.321	48.9	5.030	0.179	0.067	20.6	0.191	7.0	-0.178	0.066	-20.2	0.190
188.0	525.0	1.0	5.011	4.451	41.6	6.702	49.1	5.334	0.182	0.083	24.6	0.200	7.3	-0.182	0.083	-24.3	0.199
187.0	525.0	1.0	5.347	4.693	41.3	7.114	49.3	5.661	0.185	0.102	28.8	0.211	7.6	-0.184	0.100	-28.6	0.210
186.0	525.0	1.0	5.712	4.952	40.9	7.560	49.4	6.016	0.187	0.122	33.2	0.223	7.9	-0.186	0.121	-33.0	0.222
185.0	525.0	1.0	6.109	5.229	40.6	8.042	49.6	6.399	0.187	0.145	37.7	0.237	8.1	-0.187	0.144	-37.6	0.236
184.0	525.0	1.0	6.543	5.526	40.2	8.564	49.8	6.815	0.186	0.170	42.4	0.252	8.4	-0.186	0.169	-42.3	0.251
183.0	525.0	1.0	7.015	5.844	39.8	9.131	49.9	7.268	0.184	0.198	47.1	0.267	8.7	-0.183	0.197	-47.1	0.266
182.0	525.0	1.0	7.532	6.185	39.4	9.746	50.0	7.756	0.179	0.229	52.0	0.291	8.8	-0.178	0.228	-52.0	0.289
181.0	525.0	1.0	8.098	6.551	38.9	10.409	50.1	8.284	0.177	0.264	57.0	0.315	9.0	-0.176	0.263	-57.0	0.312
180.0	525.0	1.0	8.719	6.944	38.5	11.146	50.2	8.870	0.160	0.302	62.0	0.341	9.1	-0.158	0.300	-62.2	0.339
179.0	525.0	1.0	9.401	7.365	38.1	11.942	50.3	9.503	0.145	0.343	67.1	0.373	9.2	-0.142	0.342	-67.4	0.370
178.0	525.0	1.0	10.152	7.816	37.6	12.812	50.3	10.185	0.123	0.389	72.1	0.407	9.3	-0.120	0.388	-72.1	0.406
177.0	525.0	1.0	10.981	8.300	37.1	13.765	50.2	10.954	0.101	0.439	77.1	0.451	9.4	-0.093	0.438	-77.6	0.449
176.0	525.0	1.0	11.796	8.820	36.6	14.803	50.0	11.785	0.074	0.494	82.0	0.495	9.5	-0.064	0.493	-82.0	0.494
175.0	525.0	1.0	12.509	9.376	35.9	15.955	49.9	12.697	0.054	0.553	86.5	0.556	9.6	-0.011	0.551	-86.9	0.552
174.0	525.0	1.0	13.120	9.970	35.0	17.240	49.7	13.700	0.077	0.617	91.2	0.627	9.7	0.047	0.613	-91.7	0.617
173.0	525.0	1.0	13.633	10.610	34.8	18.604	49.3	14.604	0.096	0.686	95.9	0.700	9.8	0.119	0.684	-96.1	0.694
172.0	525.0	1.0	14.071	11.293	34.2	20.135	48.9	15.603	0.225	0.759	73.5	0.792	9.8	0.209	0.757	74.6	0.785
171.0	525.0	1.0	14.430	12.019	33.4	21.838	48.4	16.638	0.335	0.835	68.7	0.830	9.8	0.300	0.834	69.0	0.823
170.0	525.0	1.0	14.951	12.793	32.7	23.700	47.6	18.860	0.472	0.917	62.8	1.032	9.8	0.457	0.914	63.5	1.022
169.0	525.0	1.0	15.486	13.614	31.9	25.746	46.9	21.208	0.614	0.974	51.2	1.267	9.8	0.614	0.977	51.7	1.264
168.0	525.0	1.0	16.053	14.486	31.1	28.079	45.8	23.244	0.947	1.084	50.0	1.376	9.5	0.830	1.081	52.5	1.362
167.0	525.0	1.0	16.482	15.408	30.2	30.637	44.7	24.380	1.098	1.168	46.8	1.603	9.2	1.079	1.164	47.2	1.587
166.0	525.0	1.0	16.904	16.372	29.3	33.480	43.3	26.443	1.402	1.249	41.7	1.877	8.9	1.380	1.244	42.7	1.858
165.0	525.0	1.0	17.325	17.384	28.3	36.641	41.8	29.158	1.767	1.324	36.8	2.208	8.4	1.743	1.318	37.1	2.185
164.0	525.0	1.0	17.746	18.438	27.3	40.131	39.3	32.503	2.202	1.393	32.0	2.574	7.9	2.104	1.392	32.5	2.577
163.0	525.0	1.0	18.167	19.529	26.3	44.039	38.3	35.045	2.717	1.444	28.0	3.077	7.3	2.483	1.438	28.2	3.044
162.0	525.0	1.0	18.588	20.653	25.3	48.489	36.3	38.455	3.315	1.482	24.1	3.632	6.7	2.774	1.475	24.3	3.591
161.0	525.0	1.0	19.009	21.820	24.3	53.509	34.3	42.819	4.001	1.509	20.3	4.222	6.0	3.049	1.491	20.7	4.222
160.0	525.0	1.0	19.430	23.032	23.3	59.119	31.9	48.249	4.760	1.497	17.5	4.990	5.3	3.499	1.489	17.6	4.929
159.0	525.0	1.0	19.851	24.285	22.3	65.350	29.4	54.940	5.603	1.460	14.6	5.805	4.6	3.949	1.460	14.5	5.805
158.0	525.0	1.0	20.272	25.578	21.3	72.230	27.0	62.904	6.419	1.416	12.4	6.673	4.0	4.328	1.408	12.5	6.482
157.0	525.0	1.0	20.693	26.914	20.3	79.764	24.6	71.537	7.293	1.349	10.2	7.603	3.3	4.712	1.349		

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70.0	525.0	1.0	81.761	42.17	27.3	91.996	4.6	73.208	2.784	0.728	14.6	2.878	19.2	2.630	-0.647	-13.8	2.708
69.0	525.0	1.0	83.332	40.581	26.0	92.687	5.4	73.758	3.708	0.430	6.6	3.733	10.1	3.577	-0.314	-5.0	3.591
68.0	525.0	1.0	84.024	39.106	24.7	93.496	6.2	74.401	4.676	0.263	3.2	4.632	5.6	4.454	-0.031	-0.4	4.554
67.0	525.0	1.0	86.366	37.724	23.6	94.246	7.9	74.998	5.655	0.332	3.2	5.663	3.3	5.533	0.207	2.1	5.537
66.0	525.0	1.0	87.426	36.433	22.6	94.706	9.6	75.565	6.596	0.480	4.0	6.612	2.2	6.469	0.409	3.6	6.462
65.0	525.0	1.0	87.828	35.150	21.8	94.601	11.5	75.981	7.454	0.632	4.7	7.459	1.8	7.286	0.583	4.6	7.321
64.0	525.0	1.0	87.292	33.917	21.2	93.649	13.8	74.524	8.089	0.755	5.3	8.124	1.7	7.944	0.736	5.3	7.978
63.0	525.0	1.0	85.398	32.696	20.9	91.629	16.6	72.016	8.687	0.889	6.0	8.533	1.9	8.337	0.875	6.0	8.362
62.0	525.0	1.0	82.658	31.474	20.0	88.447	18.8	70.384	8.578	1.016	6.8	8.638	2.1	8.429	1.006	6.8	8.489
61.0	525.0	1.0	78.257	30.242	21.1	86.177	21.7	66.956	9.297	1.136	7.3	9.434	2.5	9.217	1.126	7.8	9.294
60.0	525.0	1.0	73.537	28.996	21.5	79.047	24.6	62.904	7.864	1.201	9.0	7.963	2.9	7.738	1.241	9.1	7.837
59.0	525.0	1.0	67.928	27.733	22.2	73.371	27.7	58.987	7.172	1.349	10.7	7.298	3.5	7.063	1.340	10.7	7.189
58.0	525.0	1.0	58.805	26.456	23.1	67.472	30.8	53.499	6.385	1.429	12.7	6.574	4.1	6.337	1.420	12.8	6.434
57.0	525.0	1.0	56.244	25.169	24.1	61.619	34.1	49.035	5.520	1.486	15.1	5.716	4.9	5.443	1.477	15.2	5.639
56.0	525.0	1.0	50.627	23.965	25.2	56.004	37.3	41.657	4.594	1.518	17.9	4.873	5.8	4.630	1.508	18.1	4.870
55.0	525.0	1.0	45.432	22.599	26.4	50.742	40.7	40.379	3.925	1.526	21.2	4.211	6.4	3.872	1.518	21.4	4.159
54.0	525.0	1.0	40.629	21.331	27.7	45.889	44.0	36.613	3.236	1.570	25.3	3.354	7.3	3.190	1.505	25.2	3.537
53.0	525.0	1.0	36.267	20.087	29.0	41.458	47.5	32.991	2.630	1.479	29.3	3.017	8.2	2.592	1.473	29.6	2.981
52.0	525.0	1.0	32.334	18.874	30.3	37.440	51.0	29.794	2.109	1.430	34.2	2.548	9.1	2.076	1.425	34.5	2.518
51.0	525.0	1.0	28.805	17.700	31.6	33.858	54.7	26.904	1.666	1.371	39.4	2.158	9.9	1.837	1.366	39.3	2.132
50.0	525.0	1.0	25.444	16.570	32.9	30.532	58.6	24.297	1.295	1.304	45.2	1.837	10.7	1.589	1.300	45.7	1.816
49.0	525.0	1.0	22.818	15.493	34.2	27.580	62.8	21.847	0.985	1.232	51.4	1.577	11.4	1.347	1.229	51.0	1.559
48.0	525.0	1.0	20.290	14.467	35.5	24.919	67.4	19.830	0.728	1.158	57.8	1.368	12.0	1.103	1.156	58.7	1.353
47.0	525.0	1.0	17.829	13.501	36.8	22.430	72.4	17.817	0.517	1.085	64.5	1.204	12.6	0.942	1.084	65.6	1.190
46.0	525.0	1.0	16.005	12.596	38.2	20.387	77.8	16.208	0.346	1.035	71.2	1.072	12.3	0.818	1.014	72.6	1.062
45.0	525.0	1.0	14.195	11.756	39.6	18.431	82.8	14.667	0.211	0.948	77.4	0.937	12.0	0.716	0.948	79.5	0.944
44.0	525.0	1.0	12.379	10.985	41.1	16.700	84.9	13.290	0.117	0.887	82.5	0.895	11.4	0.560	0.887	86.1	0.889
43.0	525.0	1.0	11.143	10.284	42.7	15.163	80.5	12.067	0.093	0.832	83.6	0.872	10.4	-0.034	0.832	-87.7	0.833
42.0	525.0	1.0	9.878	9.659	44.4	13.816	71.6	10.994	0.132	0.783	80.4	0.794	9.2	-0.108	0.784	-82.1	0.791
41.0	525.0	1.0	8.783	9.135	46.1	12.658	60.5	10.073	0.180	0.741	76.3	0.763	7.9	-0.168	0.742	-77.3	0.761
40.0	525.0	1.0	7.866	8.656	47.7	11.697	48.5	9.368	0.242	0.706	72.6	0.740	6.4	-0.213	0.709	-73.2	0.740
39.0	525.0	1.0	7.143	8.290	49.3	10.942	35.9	8.708	0.252	0.679	69.6	0.725	4.9	-0.247	0.681	-70.1	0.725
38.0	525.0	1.0	6.635	8.021	50.4	10.409	22.9	8.093	0.274	0.660	67.4	0.715	3.3	-0.271	0.662	-67.8	0.715
37.0	525.0	1.0	6.266	7.854	51.0	10.010	9.6	7.485	0.287	0.646	65.4	0.707	1.8	-0.289	0.648	-64.4	0.709
36.0	525.0	1.0	6.351	7.794	50.8	10.054	38.6	7.091	0.292	0.644	65.6	0.707	0.8	-0.289	0.647	-65.9	0.708
35.0	525.0	1.0	6.588	7.840	50.5	10.241	16.8	6.588	0.291	0.648	63.1	0.709	1.8	-0.284	0.651	-63.0	0.710
34.0	525.0	1.0	7.056	7.993	48.6	10.662	29.8	6.485	0.275	0.660	67.4	0.715	3.3	-0.271	0.662	-67.7	0.715
33.0	525.0	1.0	7.759	8.299	45.2	11.257	45.2	6.256	0.248	0.679	69.6	0.725	4.9	-0.248	0.681	-69.5	0.725
32.0	525.0	1.0	8.582	8.602	45.1	12.151	53.9	6.670	0.222	0.706	72.6	0.740	6.4	-0.215	0.708	-73.1	0.740
31.0	525.0	1.0	9.596	9.047	43.3	13.189	64.5	7.035	0.181	0.741	76.2	0.762	7.8	-0.169	0.742	-77.1	0.761
30.0	525.0	1.0	10.728	9.578	41.7	14.451	73.1	7.417	0.141	0.783	80.4	0.783	11.1	-0.145	0.783	-82.0	0.784
29.0	525.0	1.0	12.079	10.190	40.2	15.803	78.5	7.875	0.094	0.831	83.5	0.836	10.4	-0.036	0.831	-87.5	0.832
28.0	525.0	1.0	13.659	10.976	38.7	17.676	85.9	8.374	0.056	0.884	86.4	0.884	9.2	0.057	0.886	-92.5	0.884
27.0	525.0	1.0	15.192	11.634	37.4	19.135	76.6	8.925	0.029	0.948	77.6	0.970	12.0	0.173	0.947	-79.6	0.963
26.0	525.0	1.0	16.817	12.289	36.0	20.690	64.5	9.489	0.149	1.034	69.6	1.034	11.1	0.149	1.034	-82.0	1.034
25.0	525.0	1.0	19.046	13.349	35.0	23.257	68.2	10.507	0.514	1.084	64.6	1.200	12.3	0.489	1.083	-65.7	1.188
24.0	525.0	1.0	21.304	14.298	33.9	25.657	64.1	10.417	0.725	1.157	57.9	1.366	12.0	0.700	1.155	-58.8	1.350
23.0	525.0	1.0	23.625	15.308	32.7	28.337	62.3	10.332	0.913	1.253	51.4	1.574	10.8	0.961	1.228	-51.4	1.574
22.0	525.0	1.0	26.625	16.368	31.6	31.254	56.7	24.871	1.291	1.303	45.3	1.834	10.8	1.264	1.259	-45.8	1.812
21.0	525.0	1.0	29.754	17.484	30.4	34.604	49.4	24.663	1.643	1.370	39.3	2.143	10.8	1.633	1.339	-40.3	2.143
20.0	525.0	1.0	33.241	18.636	29.3	38.108	49.9	30.326	2.105	1.429	34.2	2.544	9.1	2.072	1.424	-34.5	2.514
19.0	525.0	1.0	37.116	19.826	28.1	41.826	49.9	36.488	2.656	1.477	29.4	3.015	8.2	2.568	1.471	-29.6	2.977
18.0	525.0	1.0	41.405	21.059	27.0	46.453	43.5	36.966	3.231	1.510	25.0	3.566	7.3	3.186	1.503	-25.3	3.523
17.0	525.0	1.0	46.115	22.311	25.8	51.229	40.4	40.767	3.921	1.524	21.2	4.207	6.4	3.868	1.516	-21.4	4.155
16.0	525.0	1.0	51.228	23.578	24.7	56.393	37.3	44.876	4.696	1.514	18.1	4.873	5.6	4.586	1.507	-18.0	4.855
15.0	525.0	1.0	56.678	24.853	23.7	61.847	34.2	49.248	5.516	1.484	15.1	5.712	4.9	5.439	1.515	-15.2	5.635
14.0	525.0	1.0	62.341	26.127	22.7	67.595	30.9	53.941	6.427	1.430	12.3	6.594	4.2	6.359	1.519	-12.5	6.519
13.0	525.0	1.0	68.014	27.395	21.9	73.324	28.1	58.349	7.168	1.347	9.6	7.294	3.5	7.058	1.338	-10.7	7.184
12.0	525.0	1.0	73.415	28.651	21.1	78.807	25.1	62.713	7.840	1.248	9.0	7.955	2.9	7.733	1.239	-9.1	7.833
11.0	525.0	1.0	78.711	29.894	20.9	83.730	20.8	66.630	8.353	1.130	7.5	8.439	2.5	8.205	1.125	-7.8	8.399
10.0	525.0	1.0	82.983	31.126	20.8	87.796	15.5	69.858	8.573	1.013	6.7	8.833	2.1	8.424	1.002	-6.8	8.483
9.0	525.0	1.0	86.289	32.351	20.9	91.795	10.9	72.609	8.481	0.885	6.0	9.331	1.9	8.868	0.873	-6.0	8.931
8.0	525.0	1.0	88.286	33.580	21.3	92.590	14.5	73.680	8.083	0.751	5.3	9.818	1.7	7.938	0.731	-5.3	7.972
7.0	525.0	1.0	89.428	34.825	21.9	93.164	18.6	74.458	7								

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Revision: 1.00	Classification: Public	Issue Date: July 25		

-77.0	525.0	1.0	1.334	0.593	24.0	1.460	42.6	1.162	0.076	0.016	12.1	0.078	1.9	0.076	0.016	12.0	0.078
-78.0	525.0	1.0	1.288	0.568	23.8	1.408	42.4	1.121	0.075	0.014	11.0	0.076	1.9	0.075	0.014	10.9	0.076
-79.0	525.0	1.0	1.240	0.545	23.6	1.359	42.2	1.081	0.073	0.013	9.9	0.074	1.8	0.073	0.013	9.9	0.074
-80.0	525.0	1.0	1.204	0.523	23.5	1.312	41.9	1.044	0.072	0.011	8.9	0.073	1.8	0.072	0.011	8.9	0.073
-81.0	525.0	1.0	1.164	0.500	23.4	1.267	41.7	1.007	0.071	0.011	7.9	0.071	1.7	0.071	0.011	7.9	0.071
-82.0	525.0	1.0	1.126	0.480	23.2	1.223	41.5	0.975	0.069	0.008	7.0	0.070	1.7	0.069	0.008	6.9	0.070
-83.0	525.0	1.0	1.090	0.463	23.0	1.184	41.3	0.942	0.068	0.007	6.0	0.069	1.6	0.068	0.007	6.0	0.069
-84.0	525.0	1.0	1.055	0.445	22.8	1.145	41.1	0.911	0.067	0.006	5.1	0.067	1.6	0.067	0.006	5.1	0.067
-85.0	525.0	1.0	1.022	0.427	22.7	1.108	40.9	0.882	0.066	0.005	4.2	0.066	1.6	0.066	0.005	4.1	0.066
-86.0	525.0	1.0	0.990	0.411	22.6	1.072	40.7	0.853	0.064	0.004	3.4	0.065	1.5	0.064	0.004	3.3	0.065
-87.0	525.0	1.0	0.960	0.395	22.4	1.038	40.4	0.826	0.063	0.003	2.6	0.063	1.5	0.063	0.003	2.4	0.063
-88.0	525.0	1.0	0.931	0.381	22.2	1.006	40.2	0.800	0.062	0.002	1.8	0.062	1.4	0.062	0.002	1.6	0.062
-89.0	525.0	1.0	0.903	0.366	22.1	0.974	39.9	0.775	0.061	0.001	1.1	0.061	1.4	0.061	0.001	0.8	0.061
-90.0	525.0	1.0	0.876	0.353	21.9	0.944	39.8	0.752	0.060	0.001	0.8	0.060	1.4	0.060	-0.000	-0.0	0.060
-91.0	525.0	1.0	0.850	0.340	21.8	0.914	39.5	0.729	0.059	0.001	0.5	0.059	1.3	0.059	-0.001	-0.8	0.059
-92.0	525.0	1.0	0.826	0.328	21.7	0.888	39.3	0.707	0.058	0.002	1.7	0.058	1.3	0.058	-0.002	-1.6	0.058
-93.0	525.0	1.0	0.802	0.316	21.6	0.862	39.1	0.685	0.057	0.002	2.4	0.057	1.3	0.057	-0.002	-2.3	0.057
-94.0	525.0	1.0	0.779	0.305	21.4	0.837	38.9	0.666	0.055	0.003	3.1	0.056	1.3	0.055	-0.003	-3.1	0.056
-95.0	525.0	1.0	0.757	0.294	21.2	0.812	38.6	0.647	0.054	0.004	3.8	0.055	1.2	0.054	-0.004	-3.8	0.055
-96.0	525.0	1.0	0.736	0.284	21.1	0.789	38.4	0.628	0.053	0.005	4.5	0.054	1.2	0.053	-0.005	-4.5	0.054
-97.0	525.0	1.0	0.716	0.274	21.0	0.767	38.2	0.610	0.052	0.005	5.2	0.053	1.2	0.052	-0.005	-5.1	0.053
-98.0	525.0	1.0	0.697	0.265	20.8	0.745	37.9	0.593	0.052	0.005	5.9	0.053	1.2	0.052	-0.005	-5.8	0.053
-99.0	525.0	1.0	0.678	0.256	20.7	0.723	37.7	0.577	0.051	0.006	6.5	0.051	1.1	0.051	-0.006	-6.5	0.051
-100.0	525.0	1.0	0.660	0.248	20.6	0.702	37.4	0.561	0.050	0.006	7.2	0.051	1.1	0.050	-0.006	-7.2	0.051
-101.0	525.0	1.0	0.628	0.241	21.0	0.673	38.4	0.535	0.047	0.005	4.4	0.048	1.1	0.047	-0.005	-4.4	0.048
-102.0	525.0	1.0	0.611	0.233	20.9	0.654	38.2	0.521	0.046	0.006	7.0	0.047	1.1	0.046	-0.006	-7.0	0.047
-103.0	525.0	1.0	0.595	0.226	20.8	0.636	38.0	0.506	0.046	0.006	7.6	0.046	1.1	0.046	-0.006	-7.6	0.046
-104.0	525.0	1.0	0.579	0.219	20.7	0.619	37.7	0.493	0.045	0.006	8.2	0.045	1.0	0.045	-0.006	-8.2	0.045
-105.0	525.0	1.0	0.564	0.212	20.6	0.602	37.5	0.480	0.044	0.007	8.8	0.044	1.0	0.044	-0.007	-8.8	0.044
-106.0	525.0	1.0	0.550	0.205	20.5	0.587	37.3	0.467	0.043	0.007	9.4	0.044	1.0	0.043	-0.007	-9.4	0.044
-107.0	525.0	1.0	0.536	0.199	20.4	0.573	37.1	0.455	0.042	0.007	9.9	0.043	1.0	0.042	-0.007	-9.9	0.043
-108.0	525.0	1.0	0.522	0.193	20.2	0.557	36.8	0.443	0.042	0.008	10.5	0.042	1.0	0.042	-0.008	-10.5	0.042
-109.0	525.0	1.0	0.509	0.187	20.1	0.543	36.6	0.432	0.041	0.008	11.0	0.042	0.9	0.041	-0.008	-11.0	0.042
-110.0	525.0	1.0	0.497	0.181	20.0	0.529	36.4	0.421	0.040	0.008	11.5	0.041	0.9	0.040	-0.008	-11.5	0.041
-111.0	525.0	1.0	0.485	0.176	19.9	0.516	36.2	0.410	0.039	0.008	12.1	0.040	0.9	0.039	-0.008	-12.1	0.040
-112.0	525.0	1.0	0.473	0.171	19.8	0.503	36.0	0.399	0.039	0.009	12.6	0.040	0.9	0.039	-0.009	-12.6	0.040
-113.0	525.0	1.0	0.462	0.166	19.7	0.490	35.7	0.390	0.038	0.009	13.1	0.039	0.9	0.038	-0.009	-13.1	0.039
-114.0	525.0	1.0	0.451	0.161	19.6	0.478	35.5	0.381	0.037	0.009	13.6	0.039	0.9	0.037	-0.009	-13.6	0.039
-115.0	525.0	1.0	0.440	0.156	19.6	0.467	35.3	0.372	0.037	0.009	14.1	0.038	0.8	0.037	-0.009	-14.1	0.038
-116.0	525.0	1.0	0.430	0.150	19.5	0.456	35.0	0.363	0.036	0.009	14.5	0.037	0.8	0.036	-0.009	-14.5	0.037
-117.0	525.0	1.0	0.420	0.145	19.4	0.446	34.8	0.354	0.035	0.010	14.9	0.037	0.8	0.035	-0.010	-14.9	0.037
-118.0	525.0	1.0	0.410	0.143	19.3	0.434	34.6	0.346	0.035	0.010	15.5	0.036	0.8	0.035	-0.010	-15.5	0.036
-119.0	525.0	1.0	0.401	0.140	19.2	0.424	34.4	0.338	0.034	0.010	16.0	0.036	0.8	0.034	-0.010	-16.0	0.036
-120.0	525.0	1.0	0.392	0.136	19.1	0.414	34.1	0.330	0.034	0.010	16.4	0.035	0.8	0.034	-0.010	-16.4	0.035
-121.0	525.0	1.0	0.383	0.132	19.0	0.405	33.9	0.322	0.033	0.010	16.8	0.035	0.8	0.033	-0.010	-16.8	0.035
-122.0	525.0	1.0	0.374	0.128	18.9	0.396	33.6	0.315	0.033	0.010	17.2	0.034	0.7	0.033	-0.010	-17.2	0.034
-123.0	525.0	1.0	0.366	0.125	18.8	0.387	33.4	0.308	0.032	0.010	17.7	0.034	0.7	0.032	-0.010	-17.7	0.034
-124.0	525.0	1.0	0.358	0.122	18.8	0.378	33.2	0.301	0.031	0.010	18.1	0.033	0.7	0.031	-0.010	-18.1	0.033
-125.0	525.0	1.0	0.350	0.118	18.7	0.370	32.9	0.294	0.031	0.010	18.5	0.033	0.7	0.031	-0.010	-18.5	0.033
-126.0	525.0	1.0	0.343	0.115	18.6	0.362	32.7	0.287	0.030	0.010	18.9	0.032	0.7	0.030	-0.010	-18.9	0.032
-127.0	525.0	1.0	0.336	0.112	18.5	0.354	32.4	0.282	0.030	0.010	19.3	0.032	0.7	0.030	-0.010	-19.3	0.032
-128.0	525.0	1.0	0.328	0.110	18.4	0.346	32.2	0.276	0.029	0.011	19.7	0.031	0.7	0.029	-0.011	-19.7	0.031
-129.0	525.0	1.0	0.322	0.107	18.4	0.339	32.0	0.270	0.029	0.011	20.1	0.031	0.7	0.029	-0.011	-20.1	0.031
-130.0	525.0	1.0	0.315	0.104	18.3	0.332	31.7	0.264	0.029	0.011	20.4	0.030	0.7	0.029	-0.011	-20.4	0.030
-131.0	525.0	1.0	0.308	0.101	18.2	0.325	31.5	0.258	0.028	0.011	20.8	0.030	0.6	0.028	-0.011	-20.8	0.030
-132.0	525.0	1.0	0.302	0.099	18.2	0.318	31.2	0.253	0.028	0.011	21.2	0.030	0.6	0.028	-0.011	-21.2	0.030
-133.0	525.0	1.0	0.296	0.096	18.1	0.311	31.0	0.247	0.027	0.011	21.6	0.029	0.6	0.027	-0.011	-21.6	0.029
-134.0	525.0	1.0	0.290	0.094	18.0	0.305	30.8	0.243	0.027	0.011	21.9	0.029	0.6	0.027	-0.011	-21.9	0.029
-135.0	525.0	1.0	0.284	0.092	17.9	0.299	30.5	0.238	0.026	0.011	22.2	0.028	0.6	0.026	-0.011	-22.2	0.028
-136.0	525.0	1.0	0.279	0.090	17.9	0.293	30.3	0.234	0.026	0.011	22.5	0.028	0.6	0.026	-0.011	-22.5	0.028
-137.0	525.0	1.0	0.273	0.088	17.8	0.287	30.1	0.228	0.026	0.011	22.9	0.028	0.6	0.026	-0.011	-22.9	0.028
-138.0	525.0	1.0	0.268	0.086	17.8	0.281	29.9	0.224	0.025	0.011	23.2	0.027	0.6	0.025	-0.011	-23.2	0.027
-139.0	525.0	1.0	0.263	0.084	17.7	0.276	29.6	0.219	0.025	0.011	23.6	0.027	0.6	0.025	-0.011	-23.6	0.027
-140.0	525.0	1.0	0.258	0.082	17.6	0.270	29.4	0.214	0.024	0.011	23.9	0.027	0.6	0.024	-0.011	-23.9	0.027
-141.0	525.0	1.0	0.253	0.080	17.6	0.265	29.1	0.211	0.024								

EMF-OHL-001	Electric & Magnetic Field Study Report Kintore Tealing 400kV		Applies to	
			Distribution	Transmission ✓
Revision: 1.00	Classification: Public	Issue Date: July 25		

Appendix E Arcadis Complex EMF Assessment Report

SSEN KINTORE TEALING PROJECT

Electric and Magnetic Fields in Overhead Line Duck-Under
Scenarios

6096/134/R/HN/03

AUGUST 2025



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Electric and Magnetic Fields in Overhead line Duck-Under Scenarios

This report dated 01 August 2025 has been prepared for Scottish and Southern Energy Networks/ SSEN Transmission plc (the "Client") in accordance with the terms and conditions between the Client and **Arcadis Consulting (UK) Limited** ("Arcadis") for the purposes specified in the Appointment. For avoidance of doubt, no other person(s) may use or rely upon this report or its contents, and Arcadis accepts no responsibility for any such use or reliance thereon by any other third party.

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APPENDIX A

ASTI 400 kV OHL Tower (Information Only)

ASTI 400 kV OHL Phase and Earth Wire

Duck-under Parameters and Phasing

APPENDIX B

CDEGS (HIFREQ) Results – Craigiebuckler to Tarland 132 kV OHL

Executive Summary

Scottish and Southern Electricity Networks/ SSEN Transmission plc ("SSEN") is proposing to construct and operate approximately 105.2 kilometres (km) of new double circuit 400 kilovolts (kV) overhead transmission line (OHL) between Kintore and Tealing.

In July 2022, National Grid ESO (as of 1 October 2024 now known as the National Energy System Operator (NESO)) published the Pathway to 2030 Holistic Network Design (Pathway to 2023 HND), setting out the electricity transmission network infrastructure required to enable the forecasted growth in renewable electricity across Great Britain, in light of the UK and Scottish Government's 2030 offshore wind allocations of 50 gigawatt (GW) and 11 GW (through the Crown Estate and ScotWind leasing rounds) which are the main driver for these upgrades.

The proposed 400 kV overhead line (OHL) will consist of steel lattice towers using a new tower series known as the ASTI SSE400 or AS4 for short. These towers are expected to average 57 m in height across the routes. The conductor system is proposed to be 3 x 700 mm² AAAC Araucaria with 500 mm bundle spacing. The circuit is designed to function up to 90°C while maintaining a minimum ground clearance of 9 m under normal conditions. Although it is capable of operating at to 90°C, it is not currently intended to be used at this maximum rating.

This report details the EMF assessment in OHL duck-under scenarios (see Section 4). In the context of OHL, a duck-under describes a configuration where one transmission line passes beneath another, typically to prevent routing conflicts or ensure adequate clearances in constrained spaces. The primary objective of this report is to provide an EMF assessment for the general public exposure at a height of 1 m above ground at the crossing of the proposed Kintore Tealing and other SSEN overhead lines. This report details the input data, EMF limits, and EMF calculations conducted using the CDEGS software package, alongside a risk assessment based on industry guideline.

Main Results

Arcadis carried out an EMF assessment of the proposed 400 kV OHL duck under scenario with the existing Craigiebuckler - Tarland 132 kV OHL using CDEGS (HIFREQ). The calculation profile was placed at the OHL duck-under 1 m above ground. The power flow on both circuit was considered in same direction. The study acknowledges the limitation in accurately modelling insulator end fittings and conductor assembly hardware in HIFREQ; however, this does not impact EMF calculation at ground level itself.

To ensure public exposure remains within safe limits, set exposure thresholds at 9 kV/m for electric fields and 360 µT for magnetic fields were used.

The calculation considers that the duck-under configuration for the 132 kV OHL is sagged to maintain statutory clearance to ground of 6.7 m which is considered conservative for the purpose of this assessment. Due to limitations within the CDEGS software package all towers are modelled on a uniform plane. The model however considers the lowest point between the conductor and ground and therefore can be considered conservative.

The EMF was assessed using CDEGS (HIFREQ), with all calculated values for the Craigiebuckler - Tarland 132 kV OHL duck-under scenario remaining within the safe threshold. The corresponding graphs are shown in Appendix B.

Recommendations

It is advisable for SSEN to review all input data and assumptions outlined in the report during the detailed design stage to ensure compliance with public EMF exposure limits.

1. Introduction

Scottish and Southern Electricity Networks/ SSEN Transmission plc (“SSEN”) is proposing to build a number of projects including new high-voltage electricity 400 kV transmission lines, 400 kV Substations and HVDC (high voltage direct current) link to deliver the UK Government’s 50 GW offshore wind by 2030 target. This has been set out as part of the Pathway to 2030 Holistic Network Design. Figure 1 illustrates the SSEN Pathway to 2030 projects.

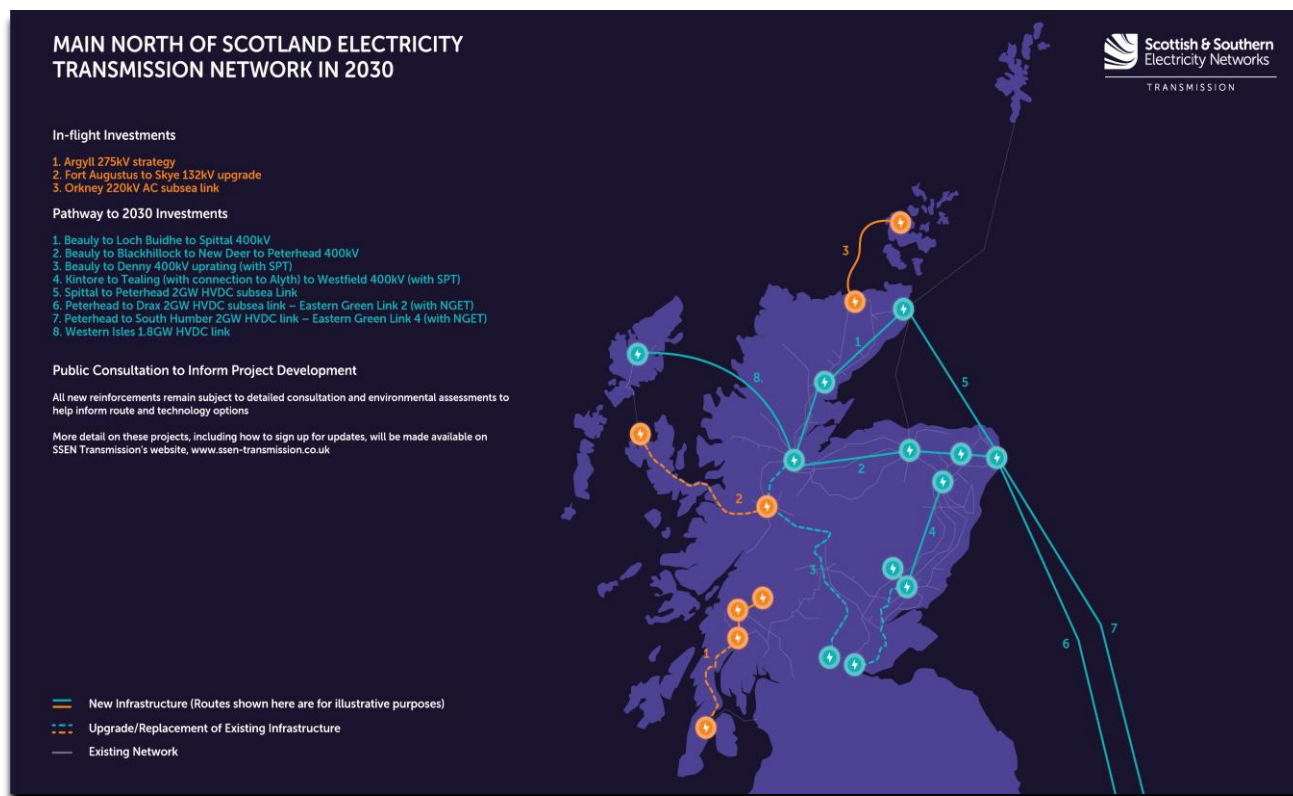


Figure 1. SSEN Pathway to 2030 Transmission Network

The Kintore to Tealing 400 kV overhead line (OHL) will consist of steel lattice towers using a new tower series known as the ASTI SSE400 or AS4 for short. These towers are expected to average 57 m in height across the routes. The conductor system is proposed to be 3x700 mm² AAAC Araucaria with 500 mm bundle spacing. The circuit is designed to function up to 90°C while maintaining a minimum ground clearance of 9 m under normal conditions. Although it is capable of operating at 90°C, it is not currently intended to be used at this maximum rating.

Arcadis Consulting (UK) Ltd (“Arcadis”) has been commissioned by SSEN to conduct an electric and magnetic fields (EMFs) assessment for the ASTI 400 kV OHL tower. Arcadis completed a report summarising the EMF calculations for AS4 tower^[1].

This report details the EMF assessment in OHL duck-under scenarios (see Section 4). In the context of OHL, a duck-under describes a configuration where one transmission line passes beneath another, typically to prevent routing conflicts or ensure adequate clearances in constrained spaces. The primary objective of this report is to provide an EMF assessment for the general public exposure at a height of 1 m above ground at the crossing of the proposed Kintore Tealing and other SSEN existing overhead lines. This report details the input data, EMF limits, and EMF calculations conducted using the CDEGS software package, alongside a risk assessment based on industry guideline. Sections 2 of the report remain unchanged from previous Arcadis report 6096/134/R/HN/01B^[1].

^[1] Arcadis Report 6096/134/R/HN/01B- SSE ASTI Project - 400 kV Overhead Line Tower Electric and Magnetic Fields, 18th February 2025
6096/134/R/HN/03C– 01/08/2025

2. Electric & Magnetic Field (EMF) Risks

The electromagnetic field (EMF) from power lines consist of electric field and magnetic field. The electric fields are produced by voltage. Electric fields are measured in volts per metre (v/m). Magnetic fields are produced by current, which is the flow of electricity. Generally, the higher the current, the higher the magnetic field. Magnetic fields are measured in microtesla (μT).

Alternating magnetic fields induces electric fields which will produce currents in a conductive medium. The human body is conductive and hence alternative magnetic fields will induce very weak voltages and currents in the human body. If these voltages and currents are high enough, it is possible to result in physiological effects on excitable tissues of the body, mainly nerve and muscle cells. Similar, direct exposure of alternating electric fields can induce very weak voltages and currents in the human body. Again, if these voltages and currents are high enough, it is possible to result in physiological effects on excitable tissues of the body, mainly nerve and muscle cells.

An active implantable medical device (AIMD) is any medical device which is intended to be totally or partially introduced, surgically or medically, into the human body, and which is intended to remain after the procedure. The commonest are pacemakers and defibrillators (together described as "implanted heart devices"). The electronic medical implants use electrical component in their construction. Under certain circumstances some implants may be susceptible to interference from electromagnetic field. This situation could lead to improper function of medical implants e.g.; a heart pacemaker disturbance can pose a health & safety threat. It should be noted that the Medicines and Healthcare products Regulatory Agency (MHRA) are aware of no instance of a patient having their implanted heart device interfered with by a high-voltage power line^[2].

The two internationally recognised exposure guidelines are established by the Institute of Electrical and Electronics Engineers (IEEE)^[3] and International Commission on Non-Ionising Radiation Protection (ICNIRP) and^[4].

2.1 How EMF Strengths Decrease with Distance

EMF decreases with distance from the source. Generally, at a distance from the source d , the fields will decrease as follows^[5]:

- Single-phase current – $1/d$,
- Single circuit or double circuit un-transposed – $1/d^2$, and
- Double circuit transposed (assuming symmetrical geometry) or coil – $1/d^3$.

Figure 2 shows this rate of decrease from different sources. In practice, factors such as unequal currents, zero sequence currents, tapered towers, geometrical deviations on the structure, and very close proximity to sources will result in rates of decrease which are less than the above. Furthermore, magnetic field profiles are typically shown horizontally along the ground (at one metre above ground), perpendicular to the conductor and typically at midspan where the conductors are closest to the ground.

^[2] <https://www.emfs.info/>

^[3] IEEE (2019) Standard for Safety Levels with Respect to Human Exposure to Electric, Magnetic, and Electromagnetic Fields, 0 Hz to 300 GHz. IEEE Std C95.1, New York

^[4] International Commission on Non-ionizing Radiation Protection (2010): Guidelines for limiting exposure to time-varying electric and magnetic fields (1 Hz to 100 kHz). Health Phys 99 (6), pp.818- 836. Erratum in Health Phys 100 (1), p.112 (2011). <https://www.icnirp.org/cms/upload/publications/ICNIRPLFgdl.pdf> and International Commission on Non-ionizing Radiation Protection (1998): Guidelines for Limiting Exposure to Time-Varying Electric, Magnetic Fields and Electromagnetic Fields (up to 300 GHz). Health Phys 74 (4), pp.494-522. <https://www.icnirp.org/cms/upload/publications/ICNIRPemfgdl.pdf>

^[5] CIGRE TB 806, Responsible management of electric and magnetic fields (EMF) – 2020.

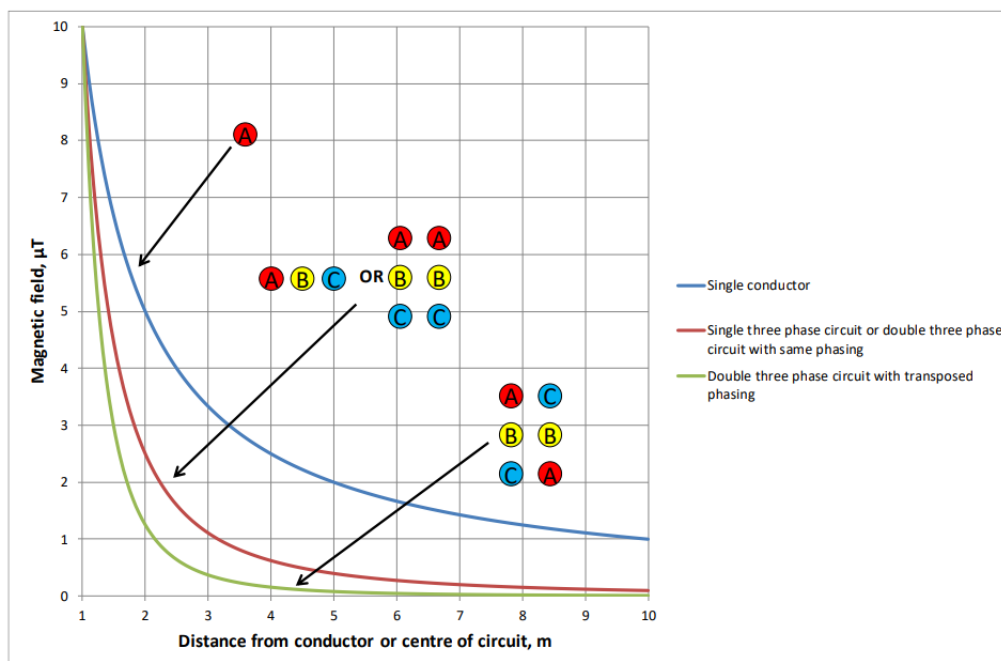


Figure 2: General Rate of Decrease of Magnetic Fields from Different Sources

2.2 EMF Limits

The EMF limits within the regulations^[6], are the exposure limits values (ELVs), and there are two levels: the Sensory ELVs and Health ELVs. The Sensory ELVs can be exceeded if a range of conditions are met, but the health ELVs must not be exceeded. For occupational exposure the first level of exposure limits for the unperturbed fields are the Sensory Action Levels which are:

- Magnetic field: 1 mT or 1000 μ T (18 mT for exposure only to limbs)
- Electric field: 10 kV/m

The regulations allow for the sensory effects ELVs to be exceeded under the following conditions: i) They are only exceeded temporarily. ii) Hazardous spark discharges and contact currents in excess of 1 mA are prevented through the provision of information and training and the use of suitable technical and personal protection measures. iii) Adequate information is provided to the employee on the possibility of sensory effects related to time varying magnetic fields, including retinal phosphenes. iv) Where any of those sensory effects are reported to the employer, the risk assessment is updated where necessary. Providing the above conditions are complied with, the Regulations allow exposure up to a High Action Levels (which ensure the health ELV are not exceeded), which are:

- Magnetic field: 6 mT or 6000 μ T (18 mT for exposure only to limbs)
- Electric field: 20 kV/m

To ensure public exposure remains within safe limits, general public exposures in the UK should adhere to the ICNIRP 1998 guidelines, as outlined in the voluntary Code of Practice^[7]. In practical terms, this means:

- An electric field of 9 kV/m.
- A magnetic field of 360 μ T.

^[6] The Control of Electromagnetic Fields at Work Regulations 2016, see <https://www.legislation.gov.uk/ukxi/2016/588/contents>

^[7] Power Lines: Demonstrating compliance with EMF public exposure guidelines – A voluntary Code of Practice, published by DECC in February 2011.

3. Computation Software

The EMF was calculated using **HIFREQ (Electromagnetic Fields Analysis) module of the SES CDEGS software suite**. HIFREQ is an optimal computation tool for tackling complex electromagnetic problems involving any system of conductors, which can be comprised of various materials and assembled in various configurations, and which may include metallic plates, coaxial or multi-core cables, GIS/GIL, transformers, and assorted lumped components (e.g. resistors, inductors, and capacitors, etc.). HIFREQ is the only computation module that can provide accurate solutions to transient and steady state problems in the frequency range of zero to hundreds of megahertz, for the analysis of buried and aboveground conductors. It computes electric and magnetic fields in the air and soil, as well as conductor and soil potentials, and the current distribution in the soil and in the conductors.

More information on HIFREQ module <https://sestech.com/en/Product/Module/HIFREQ>

Limitations: This study acknowledges the limitation in accurately modelling insulator end fittings and conductor assembly hardware in CDEGS. Accurate modelling can be attained by applying 3D electric field design and analysis software featuring Boundary Element Method (BEM) technology.

Electric fields near the surface of a conductor are very sensitive to the shape of the conductor. HIFREQ can be used to compute electric fields by modelling the OHL tower and phase conductors, however, the conductors are represented as wire filaments and the exact shape of a conductor (for example the steel members of a tower), and insulators cannot be modelled. It is important to note that electric fields computed with HIFREQ at points located far away (i.e., several conductor radii away) from the conductors should nonetheless be accurate.

4. OHL Duck-Under Scenarios

The proposed Kintore to Tealing OHL involves the construction of approximately 105.2 km of new 400 kV double circuit OHL between the existing Kintore Substation and new substation sites proposed at Fetteresso Forest (Hurlie 400 kV substation) and Tealing (Emmock 400 kV substation).

The existing Craigiebuckler to Tarland 132 kV OHL requires modification to achieve the required crossing arrangement to ensure safe operation of the 132 kV and 400 kV OHL. The works comprise constructing two new L4m SF60 (low profile) support structures and two new L4m DT support structures in a diamond formation. The new support structures will be strung with a single conductor on each phase, one circuit will be on the northern part of the diamond, and the other circuit will be on the southern part of the diamond.

The EMF assessment was carried out at the following location. The circuit data for new 400 kV and crossing arrangement is shown in Section 5 and 6.



Figure 3: Craigiebuckler to Tarland 132 kV OHL Crossing

5. Data for CDEGS Model

This section details the input data for the proposed Kintore to Tealing 400 kV circuits that was used to develop a computer model to calculate EMF as requested by SSEN.

5.1 Soil Resistivity

The soil resistivity along the OHL route was considered 500 Ωm . The magnitude was chosen based on the Arcadis engineering experience within SSEN network area. The above soil model will be used in all future subsequent analysis to represent the soil conditions.

5.2 Conductor Data

The Kintore to Tealing 400 kV OHL route will consist of steel lattice towers using a new tower series known as the ASTI SSE400 or AS4 for short. A 400 kV tower drawing is detailed within the Appendix A of this report. For each crossing the tower type, span length and sag was designed in a PLSCAD model and information shared by SSEN^[8]. The conductor system is proposed to be 3 x 700 mm² AAAC Araucaria with 500 mm bundle spacing. The phase and earth wire data sheets are attached in Appendix A.

At OHL duck-under scenarios, the existing OHL phase and earth wire data for the 132kV Craigiebuckler to Tarland OHL was based on the information attached in Appendix A of this report.

5.3 OHL Voltage Levels and Load Current

The steady state coupling in this report considers the proposed Kintore to Tealing 400 kV OHLs operating at maximum pre fault continuous winter rating of 5000 A and maximum 400 kV voltage.

At OHL duck-under scenarios, the duck under OHL rating was based on the information attached in Appendix A of this report. At the crossing location, the ground clearance of the oversailing ASTI 400 kV overhead lines was modelled using a conservative approach, bounded between a minimum clearance of 9 meters and the conductor sag profile derived from PLS-CADD simulations. The sag of the duck under OHL was modelled such that the phase conductor was approaching statutory clearance 6.7 m for 132 kV given in the Electricity Safety, Quality and Continuity Regulations 2002 (see <https://www.legislation.gov.uk/uksi/2002/2665/contents>).

The report does not consider fault conditions. As per CIGRE guidelines, in extreme cases, lightning and electrical faults can create very brief, large, fault currents in equipment and conductors/cables, and consequently elevated magnetic fields in the vicinity. Fault current events are of very short duration (typically a few cycles), rare (typically a few times per year or less) and have a low probability of coincidence with someone being in very close proximity at the time. This is a somewhat similar scenario to lightning strikes. ICNIRP 2010 does not provide specific guidance on fault currents. IEEE^[3] states that the averaging time for assessing exposures is 200 ms or ten cycles. Faults currents that exceed ten cycles are typically on low-voltage distribution systems or remote from the protection. In these cases, the current is typically lower. In any case where such faults occur the electricity system is designed to immediately isolate the fault and thereby eliminate any exposure. Therefore, electrical networks are compliant with the general principle that when a danger is identified it is eliminated as soon as possible, and all reasonable attempts are made to avoid its occurrence.

^[8] Email from SSEN, "RE: Special Arrangement Models - SF60s for EMFs" 20th February 2025.

5.4 OHL Phasing

Similar to the phase and earth wire, the phase arrangement of the OHL on a double circuit tower can impact EMF. SSEN have provided data on the proposed phasing for both the existing and proposed OHL which is shown within Appendix A. The Kintore Tealing OHL will have optimal phasing with a “centre points symmetrical” phase arrangement, as illustrated in Figure 4. This is the phasing arrangement used in the analysis. The existing OHL phasing has been modelled as per the information provided in Appendix A.

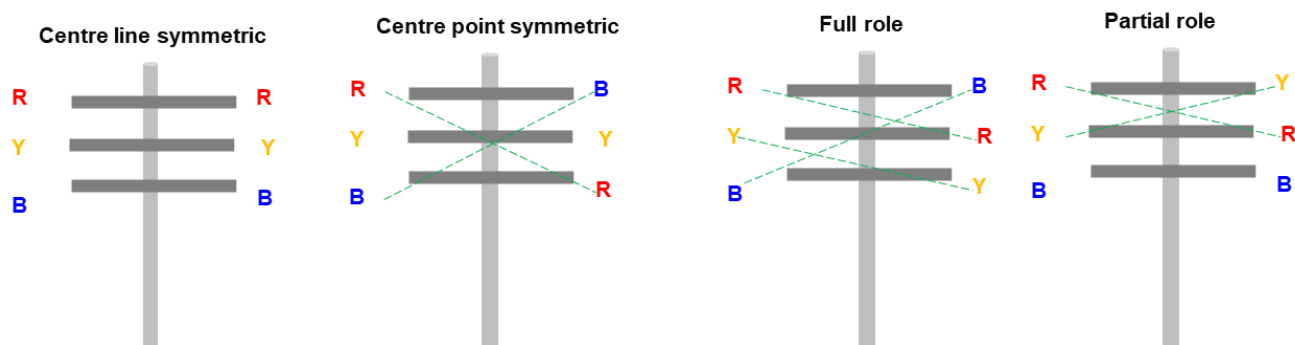


Figure 4: Possible Phase Arrangements -Double Circuit OHL

6. EMF Calculations

This section details the calculations and interpretations of EMF using HIFREQ along the CDEGS model at the proposed crossing. The OHL tower, phase, and earth wires were modelled using the data, in Section 4. Two spans were modelled, and calculation profile were placed at OHL duck-under 1 m above ground. The power flow on both circuit was considered in same direction. As stated before, this study acknowledges the limitation in accurately modelling insulator end fittings and conductor assembly hardware in HIFREQ. The insulators were omitted, and conductors were modelled at respective locations at the tower crossarm, it should be noted however that as the conductor is sagged to achieve 9m clearance to ground the insulator length has negligible impact.

According to the CDEGS model of the 132kV Craigiebuckler to Tarland OHL crossing, the maximum electric and magnetic field values are presented below, with the corresponding CDEGS plot provided in Appendix B.

- An electric field 8.44 kV < safe threshold of 9 kV/m
- A magnetic field 98.81 μT < safe threshold 360 μT

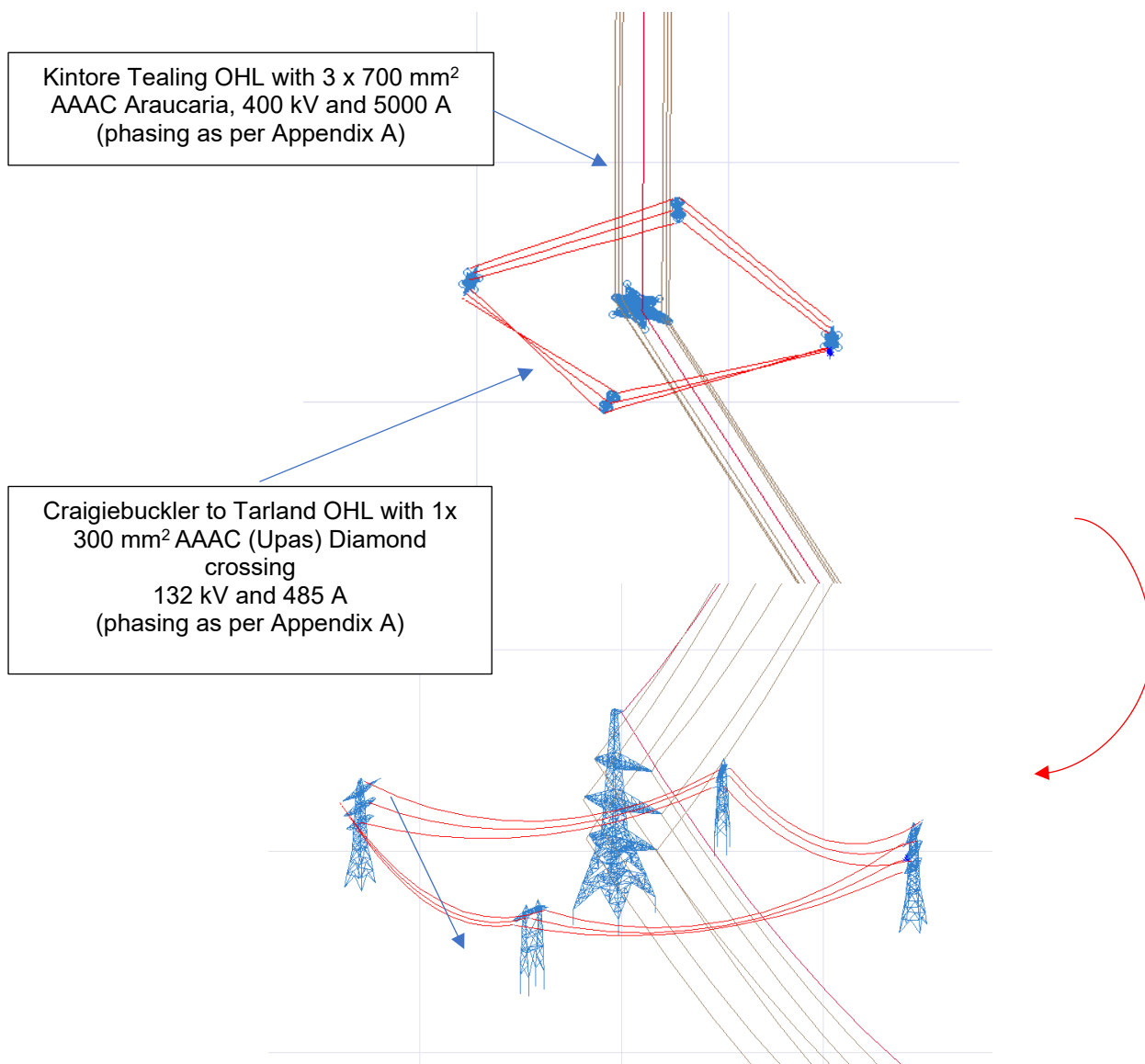


Figure 5: 132 kV Craigiebuckler to Tarland OHL Crossing

7. Conclusions

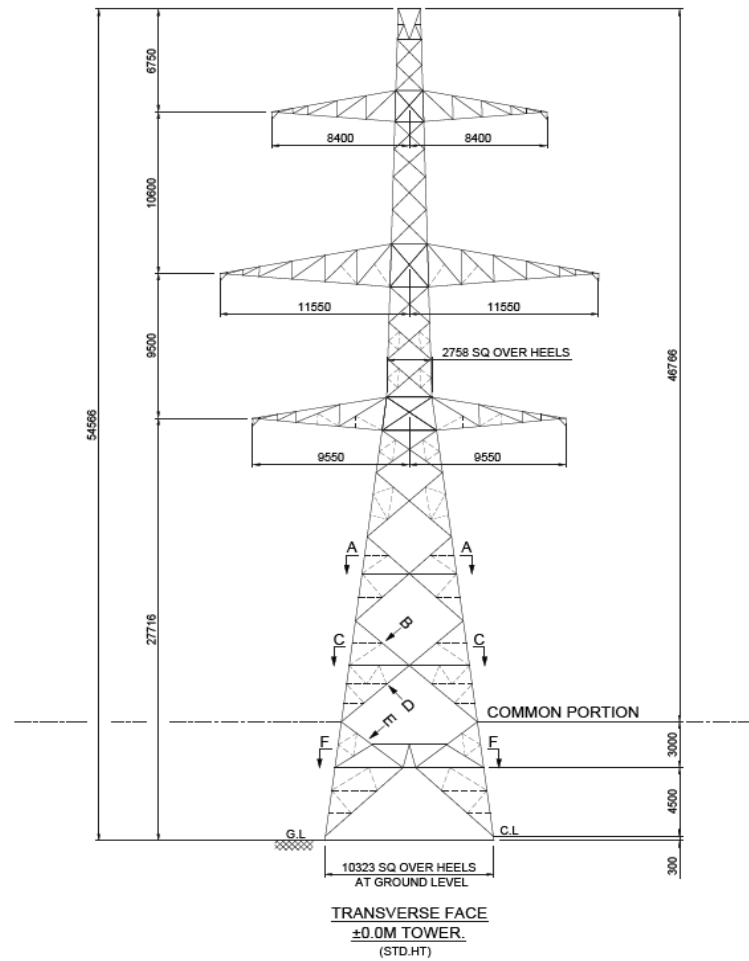
- a) Arcadis carried out an EMF assessment of the proposed Kintore Tealing 400kV OHL duck under scenario with existing SSEN Craigiebuckler to Tarland 132 kV OHL using CDEGS (HIFREQ). The calculation profile was placed at the OHL duck-under 1 m above ground. The power flow on both circuit was considered in same direction. The study acknowledges the limitation in accurately modelling insulator end fittings and conductor assembly hardware in HIFREQ however this does not impact EMF calculation at ground level itself.
- b) To ensure public exposure remains within safe limits, set exposure thresholds at 9 kV/m for electric fields and 360 μ T for magnetic fields were used.
- c) The EMF was assessed using CDEGS (HIFREQ), with all calculated values for the Craigiebuckler to Tarland 132 kV OHL duck-under scenario remaining within the safe threshold. The corresponding graphs are shown in Appendix B.

8. Recommendations

- a) It is advisable for SSEN to review all input data and assumptions outlined in the report during the detailed design stage to ensure compliance with public EMF exposure limits.

Appendix A

ASTI 400 kV OHL Tower (Information Only)



ASTI 400 kV OHL Phase and Earth Wire

data sheet

LF AAAC Araucaria EHC


LAMIFIL


Version 1, 23-02-2008

Conductor	AAAC 820mm ²
Code name	LF AAAC Araucaria EHC

Mechanical specifications	Metric (SI)		Imperial	
Nominal aluminium equivalent area	mm ²	761	in ²	1,179
Nominal cross sectional area of aluminium alloy	mm ²	821,1	in ²	1,273
Number, diameter and type of central wire	#, mm	1 4,14 R Alloy	#, in	1 0,163 R Alloy
Number, (eq.) diameter and type of wire in layer	#, mm	6 4,14 R Alloy	#, in	6 0,163 R Alloy
Number, (eq.) diameter and type of wire in layer	#, mm	12 4,14 R Alloy	#, in	12 0,163 R Alloy
Number, (eq.) diameter and type of wire in layer	#, mm	18 4,14 R Alloy	#, in	18 0,163 R Alloy
Number, (eq.) diameter and type of wire in layer	#, mm	24 4,14 R Alloy	#, in	24 0,163 R Alloy
Diameter tolerance of aluminium wires (Al or Alloy)	mm	± 0,03	in	± 0,001
Lay ratio of inner layer(s)		10-16		10-16
Lay ratio of outer layer		10-14		10-14
Overall diameter	mm	37,26	in	1,467
Rated tensile strength of conductor (RTS)	kN	242,2	kibf	54,5
Nominal mass per unit length - total	kg/km	2350,5	lb/kft	1579,5
Nominal mass per unit length - total bare	kg/km	2271,5	lb/kft	1526,4
Nominal mass per unit length - grease	kg/km	79,0	lb/kft	53,1
Coefficient of linear expansion below thermal kneepoint	/ K	0,00002300	/ °F	0,00001278
Modulus of elasticity below thermal kneepoint	GPa	56,6	Msi	8,20
Geometric mean radius	mm	14,5	ft	0,0476

Electrical specifications	Metric (SI)		Imperial	
Nominal DC resistance at 20 °C (tolerance ± 2%)	Ohm/km	0,0381	Ohm/mile	0,0612
Temperature coefficient		0,00403		0,00403
Frequency	Hz	50	Hz	60
Nominal AC resistance at 20 °C (tolerance ± 2%)	Ohm/km	0,0401	Ohm/mile	0,0659
Nominal AC resistance at 25 °C (tolerance ± 2%)	Ohm/km	0,0408	Ohm/mile	0,0671
Nominal AC resistance at 50 °C (tolerance ± 2%)	Ohm/km	0,0445	Ohm/mile	0,0729
Nominal AC resistance at 75 °C (tolerance ± 2%)	Ohm/km	0,0482	Ohm/mile	0,0787
Nominal AC resistance at 100 °C (tolerance ± 2%)	Ohm/km	0,0519	Ohm/mile	0,0846
Maximum allowable continuous operating temperature (surface)	°C	90	°F	194
Inductive reactance: X _a (conductor part)	Ohm/km	0,1914	Ohm/mile	0,3696
Shunt capacitive reactance: X _a (conductor part)	MOhm/km	0,1204	MOhm/mile	0,1003

Individual wires	Metric (SI)		Imperial	
Maximum resistivity of aluminium alloy at 20 °C, minimum IACS	nOhm, %	30,50 57%	nOhmft, %	100,07 57%
Minimum tensile strength, aluminium alloy wire	MPa	295	psi	42786
Minimum elongation for aluminium alloy wire.	%	3,5	%	3,5

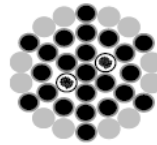
Standard applied for conductor manufacturer: TS 3.4.2 - Issue 5 - juni 2004

Page 1


08.04.2024, Ja
TK 14988-10 Rev. 00

ASLH-V(2S)bbb 96 SMF (AL3/A20SA 109/209)
Optical Ground Wire (OPGW)

according to IEC 60794-4-10



- Stranding direction of outer layer: right hand (Z-stranding)
- Greasing acc. to EN 50182 A.2 / Grease acc. to EN 50326, type A
- Entire conductor greased except outer layer
- Wires acc. to EN 50183 / EN 61232
- Maximum fibre capacity per steel tube: 48 x 250µm Ø / 66 x 200µm Ø
- Fibres coloured acc. to colour code 048 F TIA-598-D
- Fibres acc. to G.652.D
- Tube marking: #1: none #2: **|| 2 2 ||**

Configuration

Center	1 A20SA - Wire	3,50 mm
Layer 1	4 A20SA - Wires	3,40 mm
	+ 2 Stainless Steel Tubes with 48 SMF	3,00 / 3,40 mm
Layer 2	12 A20SA - Wires	3,40 mm
Layer 3	12 AL3 - Wires	3,40 mm
	6 A20SA - Wires	3,40 mm

Mechanical Data

Cable Diameter	23,9 mm
Cable Weight	1798 kg/km
Supporting Cross Section	318,3 mm ²
Rated Tensile Strength (RTS)	278,6 kN
Modulus of Elasticity	126,1 kN/mm ²
Thermal Elongation Coefficient	14,5 · 10 ⁻⁶ /K
Permissible Maximum Working Stress (50% RTS)	437,7 N/mm ² (139,3kN)
Recommended Everyday Stress (20% RTS)	175,1 N/mm ² (55,7kN)
Ultimate Exceptional Stress (80% RTS)	700,3 N/mm ² (222,9kN)

Electrical Data

DC Resistance (20°C)	0,176 Ω/km
Conductivity	30,8% IACS
Short Time Current (1,0s; 20-200°C)	25,8 kA
Short Time Current (0,5s; 20-200°C)	36,5 kA
Short Time Current Capacity It (20-200°C)	665,4 kA²s

Application

Maximum Permissible Installation Force	83,6 kN
Minimum Bending Radius	static 299 mm
	dynamic 359 mm
Normal Delivery Length	3000 m
Temperature Range	Installation -10 to +50°C
	Transportation and Operation -40 to +85°C

All Sizes and Values are Nominal Values. The latest edition of referenced documents applies.
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Duck-under Parameters and Phasing

LT455 – TKUP

Special Arrangement 1

Conductor type:

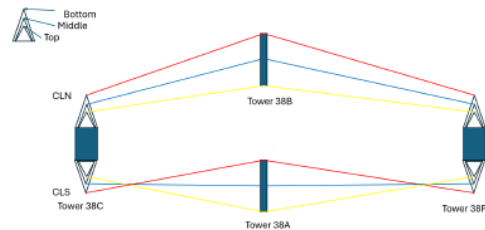
- Existing conductor: 1x Lynx
- New conductor (for diamond only): 1 x AAAC Upas

Circuit rating:

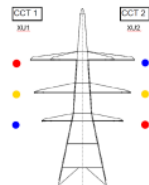
- Voltage: 132kV
- For Lynx @ 50°C: Winter Pre Fault =485A

Circuit Thermal Overload Ratings for 132kV, 1 x 175 mm ² Lynx ACSR						
O/H Circuit ID – CLN (Foggieton (T)-Tarland)						
Rated Temperature: 50°C						
ALL RATINGS ARE PER CIRCUIT	Winter Amps	Winter MVA	Spring / Autumn Amps	Spring / Autumn MVA	Summer Amps	Summer MVA
Pre-Fault Continuous	485	111	450	103	390	89
Post-Fault Continuous	580	132	540	123	465	106

Phasing: CLN/CLS



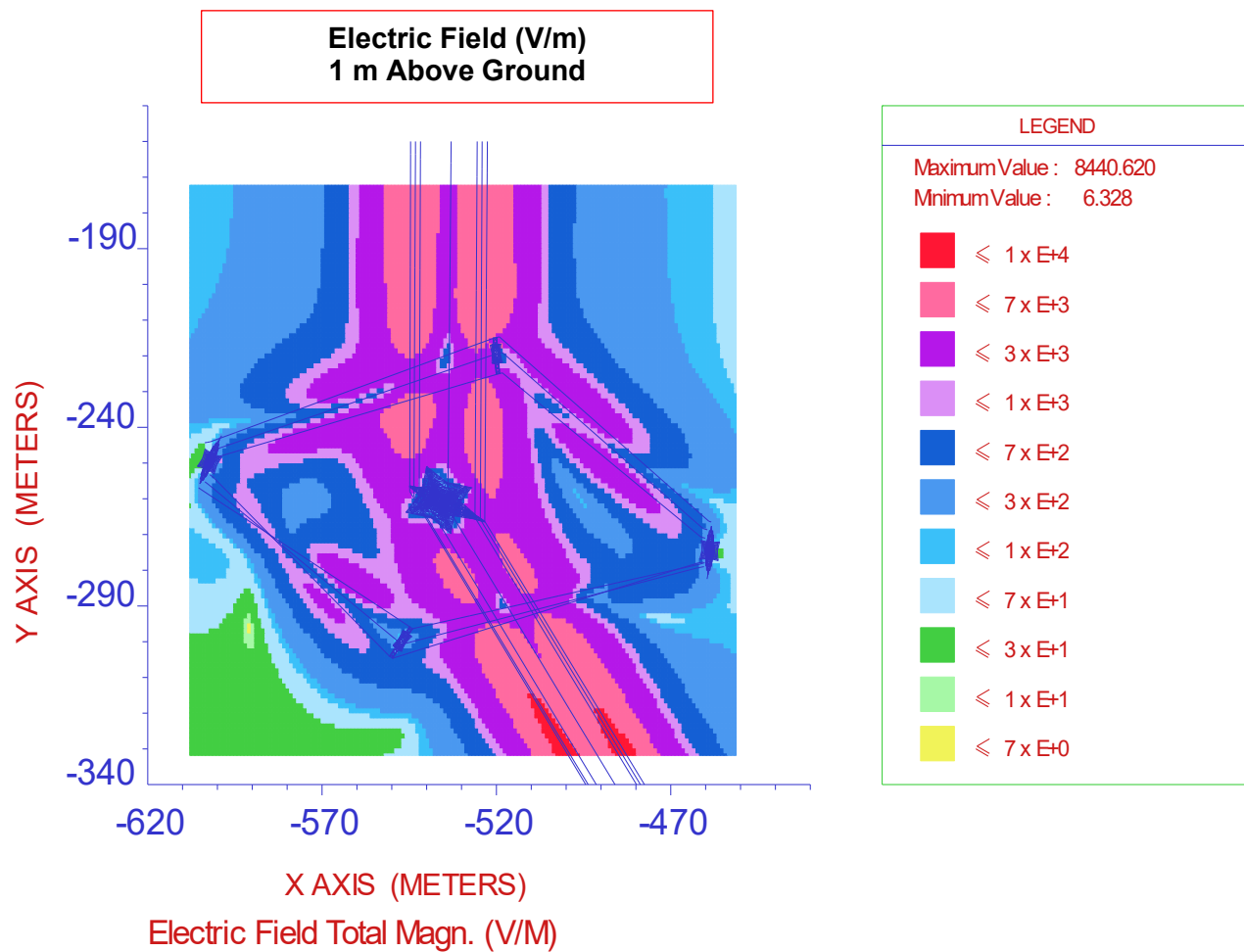
ASTI Phasing:

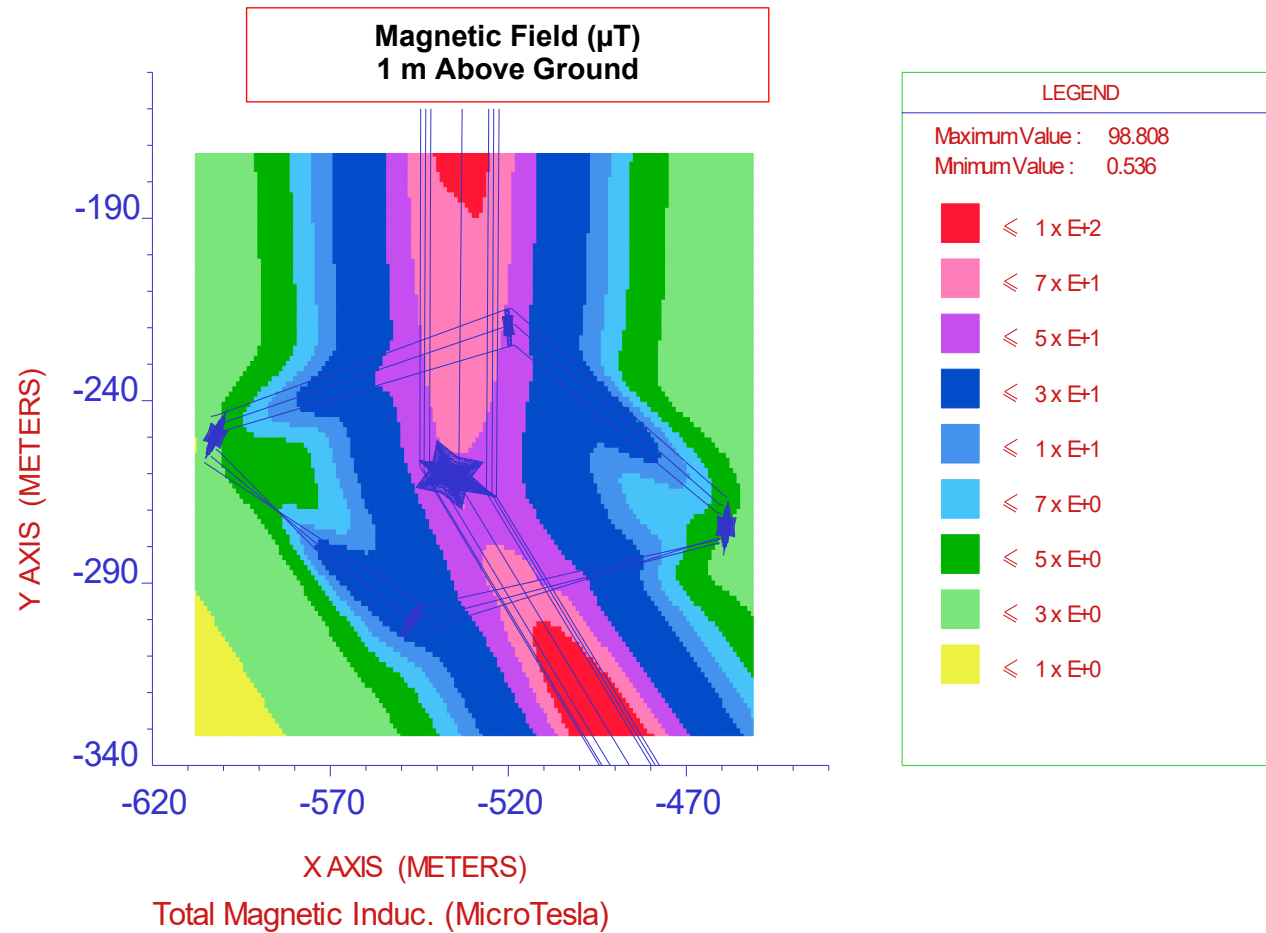


Appendix B

CDEGS (HIFREQ) Results – Craigiebuckler to Tarland 132 kV OHL

Craigiebuckler to Tarland 132 kV Crossing





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